

# DATA SHEET

## **TEA1064B**

Low voltage versatile telephone transmission circuit with dialler interface and transmit level dynamic limiting

Product specification  
File under Integrated Circuits, IC03A

March 1994

## Low voltage versatile telephone transmission circuit with dialler interface and transmit level dynamic limiting

TEA1064B

### FEATURES

- Low DC line voltage; operates down to 1.8 V (excluding polarity guard)
- Voltage regulator with low voltage drop and adjustable static resistance
- DC line voltage adjustment facility
- Provides a supply for external circuits
- Dynamic limiting (speech-controlled) in transmit direction prevents distortion of line signal and sidetone
- Symmetrical high-impedance inputs (64 k $\Omega$ ) for dynamic, magnetic or piezo-electric microphones
- Asymmetrical high-impedance input (32 k $\Omega$ ) for electret microphones
- DTMF signal input
- Confidence tone in the earpiece during DTMF dialling
- Mute input for disabling speech during pulse or DTMF dialling
- Power-down input for improved performance during pulse dial or register recall (flash)
- Receiving amplifier for dynamic, magnetic or piezo-electric earpieces

- Large amplification setting ranges on microphone and earpiece amplifiers
- Line loss compensation (line current dependent) for microphone and earpiece amplifiers (not used for DTMF amplifier)
- Gain control curve adaptable to exchange supply
- Automatic disabling of the DTMF amplifier in extremely-low voltage conditions
- Microphone MUTE function available with switch
- MUTE, POWER-DOWN and DTMF input reference (pin V<sub>EE2</sub>) can be connected either to V<sub>EE1</sub> or SLPE.

### GENERAL DESCRIPTION

The TEA1064B is a bipolar integrated circuit that performs all the speech and line interface functions required in fully electronic telephone sets. It performs electronic switching between dialling and speech. The IC operates at line voltages down to 1.8 V DC (with reduced performance) to facilitate the use of more telephone sets connected in parallel. The transmit signal on the line is dynamically limited (speech-controlled) to prevent distortion at high transmit levels of both the sending signal and the sidetone.

### ORDERING INFORMATION

EXTENDED TYPE NUMBER	PACKAGE			
	PINS	PIN POSITION	MATERIAL	CODE
TEA1064B	20	DIL	plastic	SOT146 <sup>(1)</sup>
TEA1064BT	20	mini-pack	plastic	SO20; SOT163A <sup>(2)</sup>

### Notes

1. SOT146-1; 1998 Jun 18.
2. SOT163-1; 1998 Jun 18.

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**QUICK REFERENCE DATA**

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
$I_{line}$	line current operating range	note 1	11	–	140	mA
	normal operation with reduced performance		2	–	11	mA
$I_{CC}$	internal supply current	$V_{CC} = 2.8\text{ V}$	–	1.3	1.6	mA
	power-down input LOW power-down input HIGH		–	60	82	$\mu\text{A}$
$G_v$	voltage gain range		44	–	52	dB
	microphone amplifier receiving amplifier		20	–	45	dB
$G_v$	line loss compensation ranges		5.7	6.1	6.5	dB
$V_{exch}$	gain control		36	–	60	V
$R_{exch}$	exchange supply voltage exchange feeding bridge resistance		400	–	1000	$\Omega$
$V_{LN(p-p)}$	maximum output voltage swing on LN (peak-to-peak value)	$R_{16} = 392\ \Omega$ ; $I_{line} = 15\text{ mA}$	3.55	3.80	4.05	V
		$I_p = 1.4\text{ mA}$ $I_p = 2.7\text{ mA}$	3.25	3.50	3.75	V
$V_p$	supply for peripherals	$I_{line} = 15\text{ mA}$	2.5	2.7	–	V
		$I_p = 1.4\text{ mA}$	2.9	3.1	–	V
		$I_p = 2.7\text{ mA}$ ; $R_{REG-SLPE} = 20\text{ k}\Omega$				
$V_{LN}$	DC line voltage	$I_{line} = 15\text{ mA}$ without $R_{REG-SLPE}$	3.25	3.5	3.75	V
		$R_{REG-SLPE} = 20\text{ k}\Omega$	4.05	4.4	4.75	V
$T_{amb}$	operating ambient temperature range		–25	–	+75	$^{\circ}\text{C}$

**Note**

- For the TEA1064BT the maximum line current depends on the heat dissipating qualities of the mounted device.

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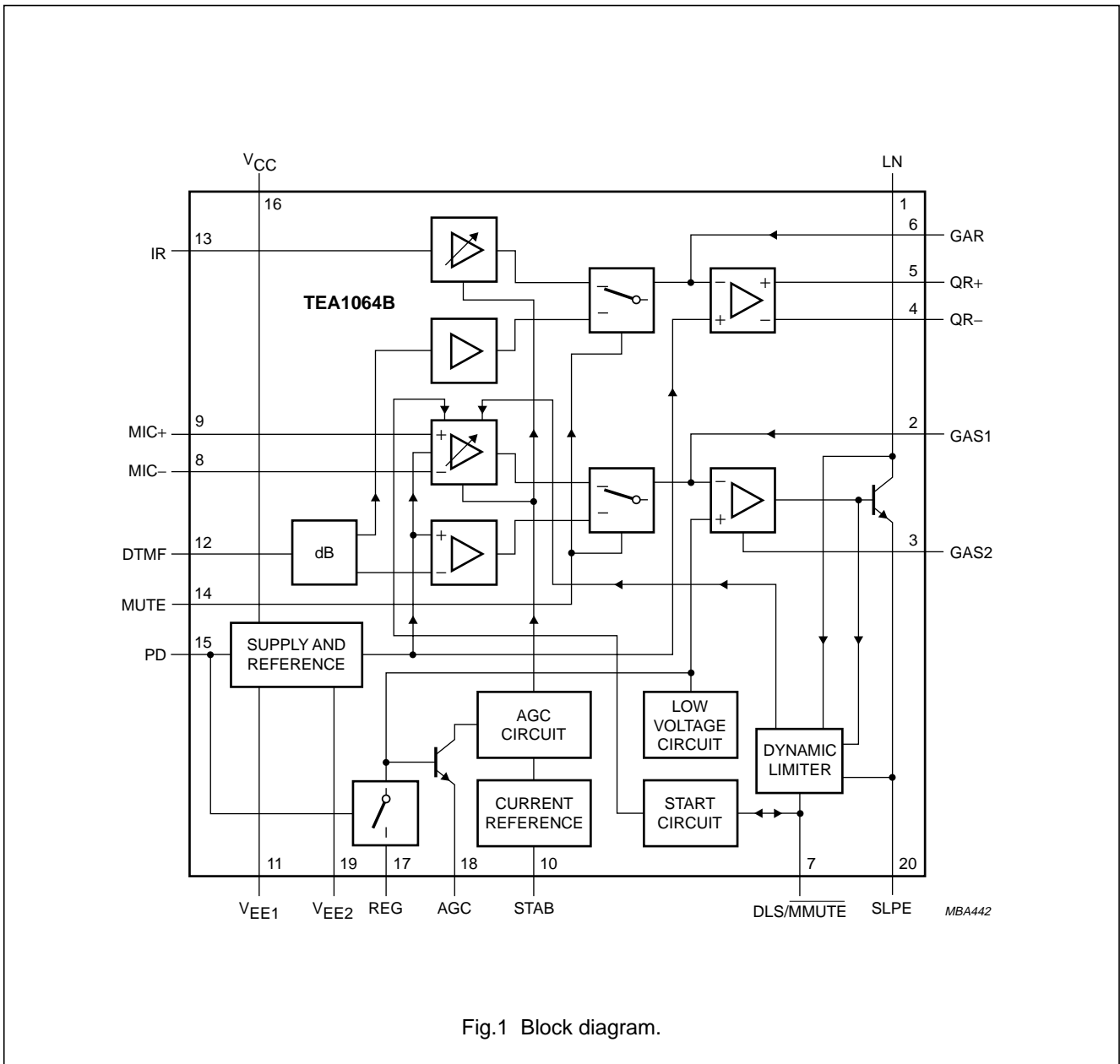


Fig.1 Block diagram.

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PINNING

SYMBOL	PIN	DESCRIPTION
LN	1	positive line terminal
GAS1	2	gain adjustment; transmitting amplifier
GAS2	3	gain adjustment; transmitting amplifier
QR-	4	inverting output; receiving amplifier
QR+	5	non-inverting output; receiving amplifier
GAR	6	gain adjustment; receiving amplifier
DLS/MMUTE	7	decoupling for transmit amplifier dynamic and microphone MUTE input
MIC-	8	inverting microphone input
MIC+	9	non-inverting microphone input
STAB	10	current stabilizer
V <sub>EE1</sub>	11	negative line terminal
DTMF	12	dual-tone multi-frequency input
IR	13	receiving amplifier input
MUTE	14	mute input
PD	15	power-down input
V <sub>CC</sub>	16	internal supply decoupling
REG	17	voltage regulator decoupling
AGC	18	automatic gain control input
V <sub>EE2</sub>	19	reference for POWER-DOWN (PD), MUTE and DTMF
SLPE	20	slope adjustment for DC curve/reference for peripheral circuits

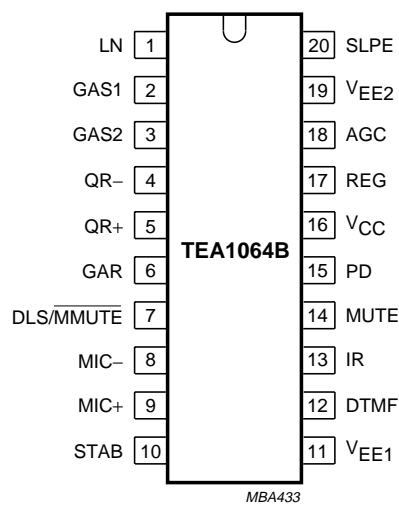


Fig.2 Pin configuration.

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## FUNCTIONAL DESCRIPTION

### Supplies $V_{CC}$ , $V_{EE2}$ , LN, SLPE, REG and STAB (Figs 3 and 5)

Power for the TEA1064B and its peripheral circuits is usually obtained from the telephone line. The IC develops its own supply voltage at  $V_{CC}$  and regulates its voltage drop. The internal supply requires a decoupling capacitor between  $V_{CC}$  and  $V_{EE1}$ . The internal current stabilizer is set by a 3.6 k $\Omega$  resistor between STAB and  $V_{EE1}$ .

The DC current flowing into the set is determined by the exchange supply voltage  $V_{exch}$ , the feeding bridge resistance  $R_{exch}$ , the subscriber line DC resistance  $R_{line}$  and the DC voltage (including polarity guard) on the subscriber set (see Fig.3).

The internal voltage regulator generates a temperature-compensated reference voltage that is available between LN and SLPE ( $V_{ref} = V_{LN-SLPE} = 3.23$  V typ.). This internal voltage regulator requires decoupling by a capacitor between REG and  $V_{EE1}$  (C3).

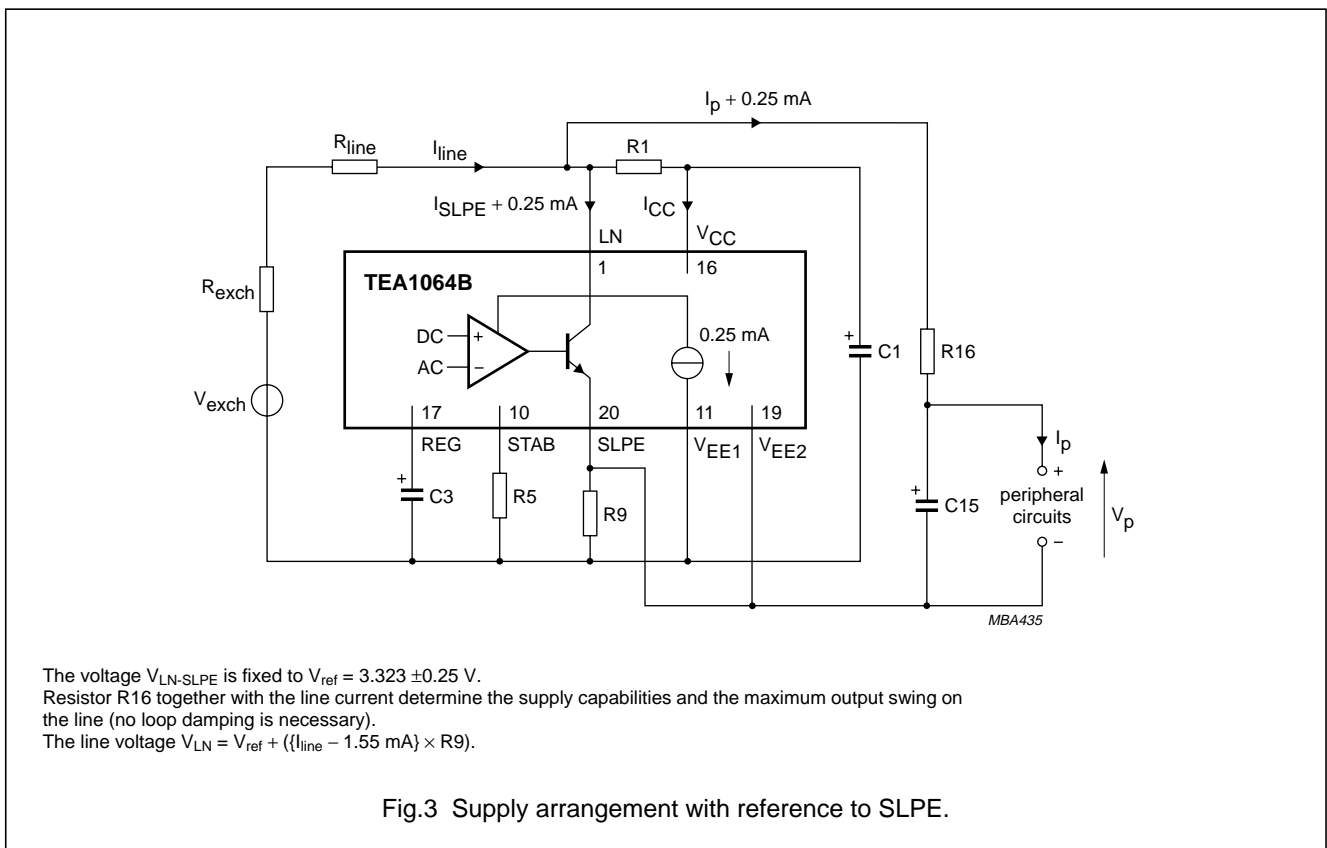
The configuration shown in Fig.3, gives a stabilized voltage across pins LN and SLPE which, applied via the low-pass filter R16, C15, provides a supply to the peripherals that is independent of the line current and depends only on the peripheral supply current.

The value of R16 and the level of the DC voltage  $V_{LN-SLPE}$  determine the supply capabilities. In the basic application  $R16 = 392 \Omega$  and  $C15 = 220 \mu F$ . The worst-case peripheral supply current as a function of supply voltage is shown in Fig.4.

To increase the supply capabilities, the value of R16 can be decreased or the DC voltage  $V_{LN-SLPE}$  can be increased by using  $R_{VA(REG-SLPE)}$ .

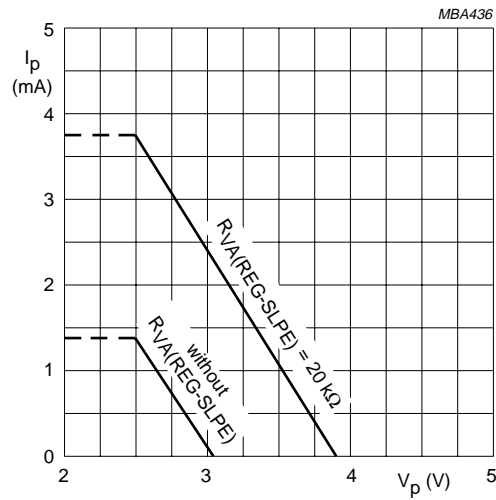
### Note

The TEA1064B application is the same as is used for TEA1060/TEA1061, TEA1067 and TEA1068 integrated circuits.



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$I_{line} = 15 \text{ mA}$ ;  $R_{16} = 392 \Omega$ ; valid for MUTE = 0 and 1.  
Line current has very little influence.

Fig.4 Maximum supply current with respect to Fig.3 for peripherals ( $I_p$ ) as a function of the peripheral supply voltage ( $V_p$ ).

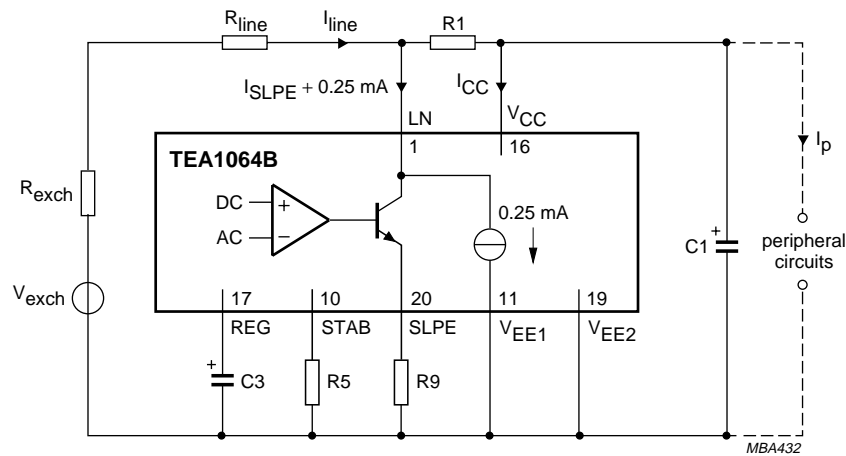
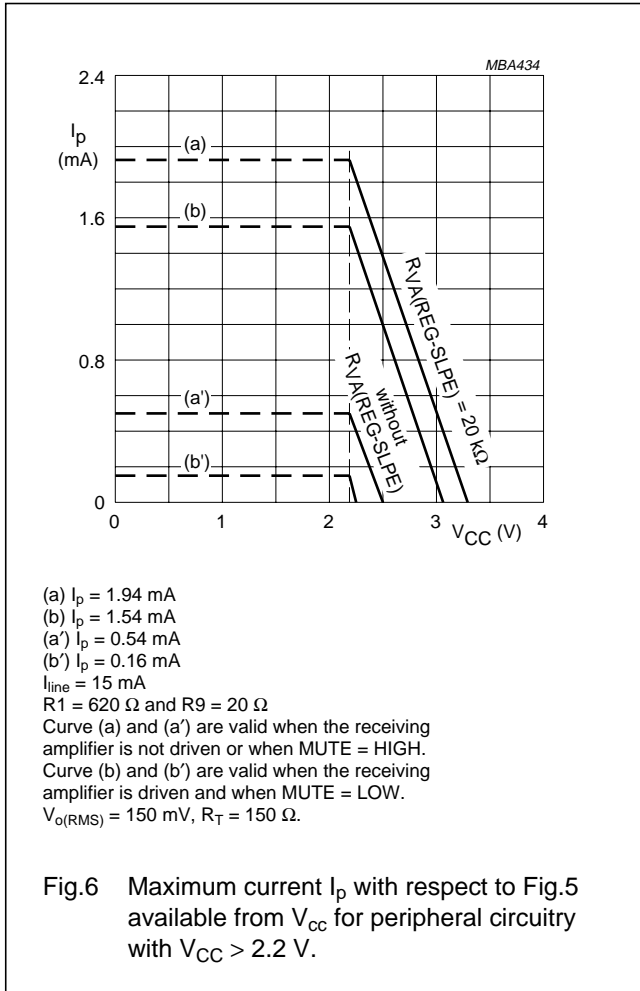


Fig.5 Supply arrangement with reference to  $V_{EE1}$ .

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The maximum AC output swing on the line at low currents is influenced by R16 (limited by current) and the maximum output swing on the line at high currents is influenced by DC voltage  $V_{LN-SLPE}$  (limited by voltage). In both these situations, the internal dynamic limiter in the sending channel prevents distortion when the microphone is overdriven. The maximum AC output swing on LN is shown in Fig.7; practical values for R16 are from 200  $\Omega$  to 600  $\Omega$  and this influences both maximum output swing at low line currents and the supply capabilities.

When the SLPE pin is the reference for peripheral circuits, inputs MUTE, PD and DTMF must be referenced to SLPE. This is achieved by connecting pin  $V_{EE2}$  to pin SLPE;  $V_{EE2}$  being the reference of MUTE, PD and DTMF input stages.

Active microphones can be supplied between  $V_{CC}$  and  $V_{EE1}$  as shown in Fig.5. Low power circuits that provide MUTE, PD and DTMF inputs to the TEA1064B can also be powered from  $V_{CC}$  (see Fig.6 for the supply capability of

$V_{CC}$ ). MUTE, PD and DTMF are then referenced to  $V_{EE1}$  and the pin  $V_{EE2}$  must therefore be connected to  $V_{EE1}$ .

If the line current  $I_{line}$  exceeds  $I_{CC} + 0.25\text{ mA}$ , the voltage converter shunts the excess current to SLPE via LN; where  $I_{CC} \approx 1.3\text{ mA}$ , the value required by the IC for normal operation.

The DC line voltage on LN is:

- $V_{LN} = V_{LN-SLPE} + (I_{SLPE} \times R_9)$
- $V_{LN} = V_{ref} + \{(I_{line} - I_{CC} - 0.25 \times 10^{-3}\text{ A}) \times R_9\}$

in which:

- $V_{ref} = 3.23\text{ V} \pm 0.25\text{ V}$  is the internal reference voltage between LN and SLPE; its value can be adjusted by external resistor  $R_{VA}$ .
- $R_9 =$  external resistor between SLPE and  $V_{EE1}$  (20  $\Omega$  in basic operation).

With  $R_9 = 20\ \Omega$ , this results in:

- $V_{LN} = 3.3 \pm 0.25\text{ V}$  at  $I_{line} = 15\text{ mA}$
- $V_{LN} = 4.1 \pm 0.3\text{ V}$  at  $I_{line} = 15\text{ mA}$ ,  $R_{VA(REG-SLPE)} = 33\text{ k}\Omega$
- $V_{LN} = 4.4 \pm 0.35\text{ V}$  at  $I_{line} = 15\text{ mA}$ ,  $R_{VA(REG-SLPE)} = 20\text{ k}\Omega$

The preferred value for  $R_9$  is 20  $\Omega$ . Changing  $R_9$  influences microphone gain, DTMF gain, the gain control characteristics, sidetone and the DC characteristics (especially the low voltage characteristics).

In normal conditions,  $I_{SLPE} \gg (I_{CC} + 0.25\text{ mA})$  and the static behaviour is equivalent to a voltage regulator diode with an internal resistance of  $R_9$ . In the audio frequency range the dynamic impedance is determined mainly by  $R_1$ . The equivalent impedance of the circuit in audio frequency range is shown in Fig.8.

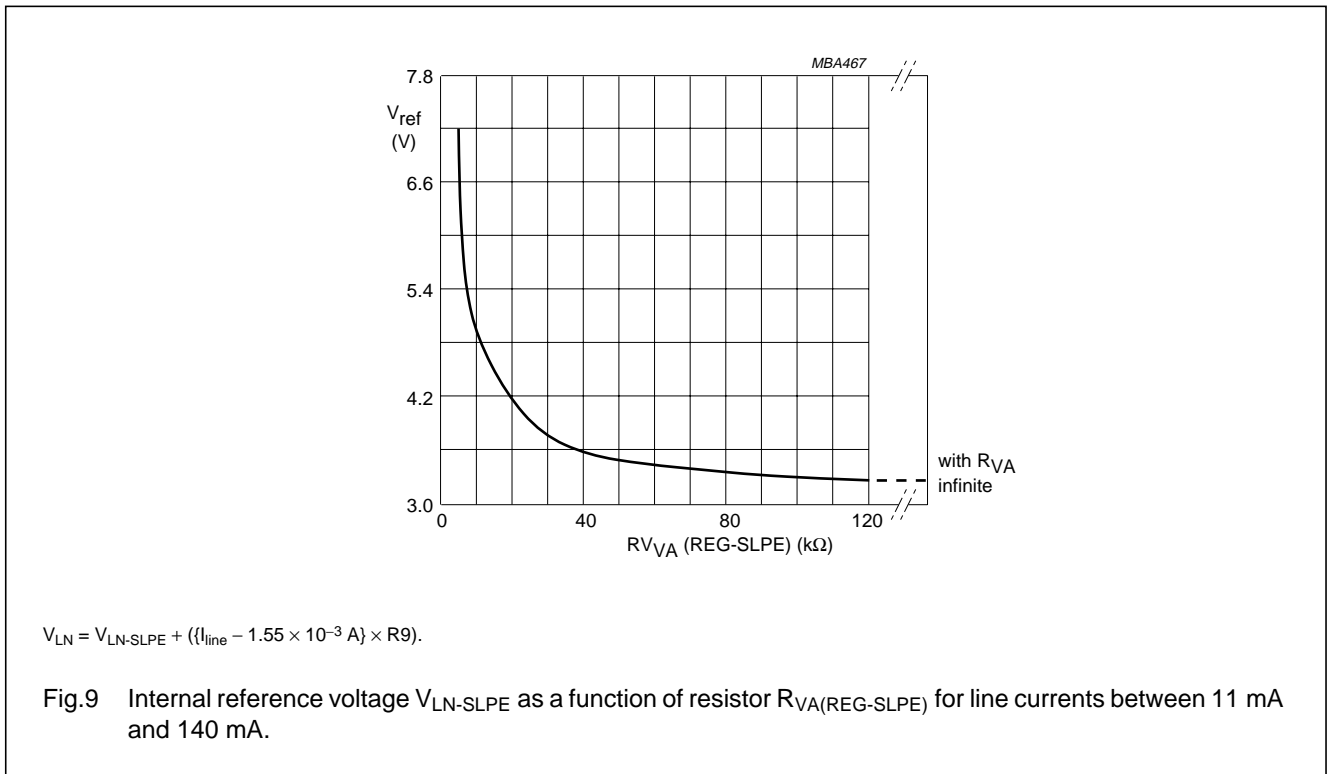
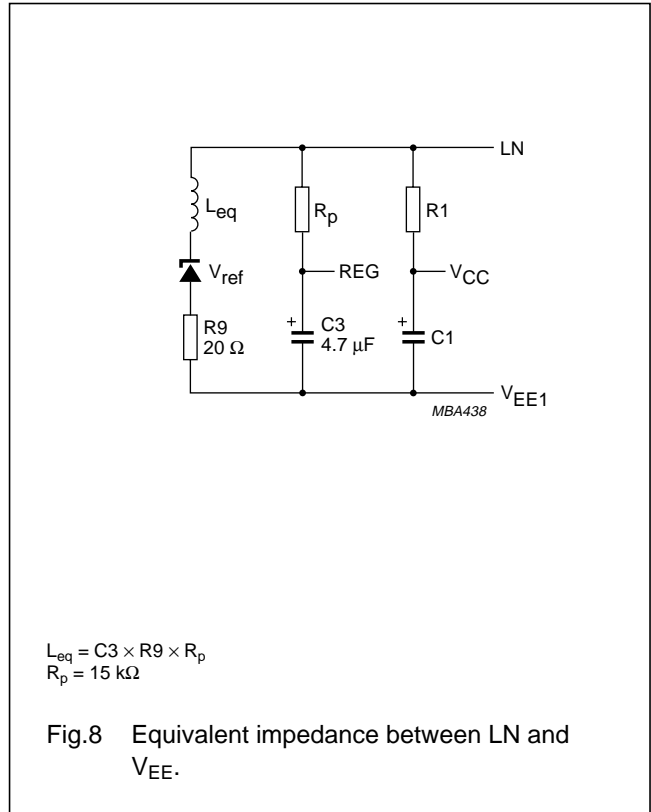
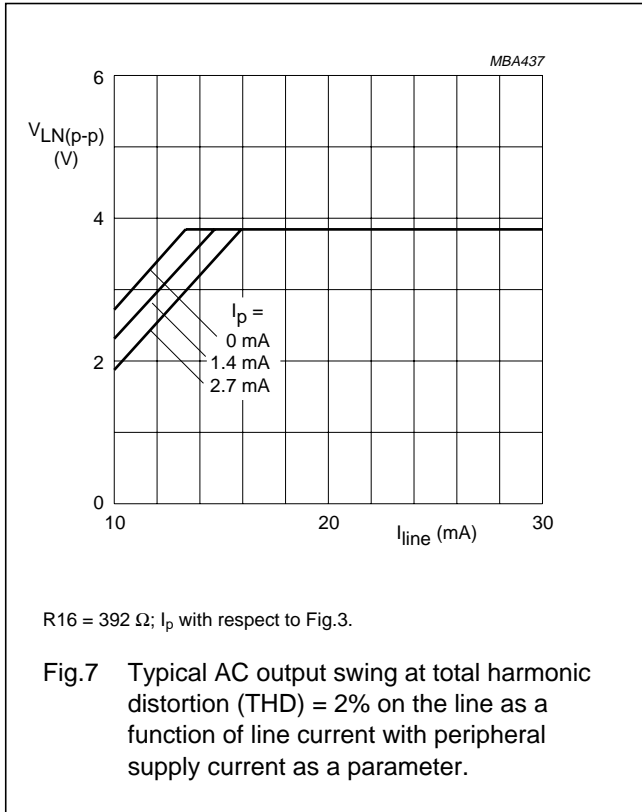
The internal reference voltage  $V_{LN-SLPE}$  can be increased by external resistor  $R_{VA(REG-SLPE)}$  connected between REG and SLPE. The voltage  $V_{LN-SLPE}$  is shown as a function of  $R_{VA(REG-SLPE)}$  in Fig.9. Changing the reference voltage influences the output swing of both sending and receiving amplifiers.

At line currents below 8 mA (typ.), the DC voltage dropped across the circuit is adjusted to a lower level automatically (approximately 1.8 V at 2 mA). This gives the possibility of operating more telephone sets in parallel with DC line voltages (excluding polarity guard) down to an absolute minimum of 1.8 V. At line currents below 8 mA (typ.), the circuit has limited sending and receiving levels.



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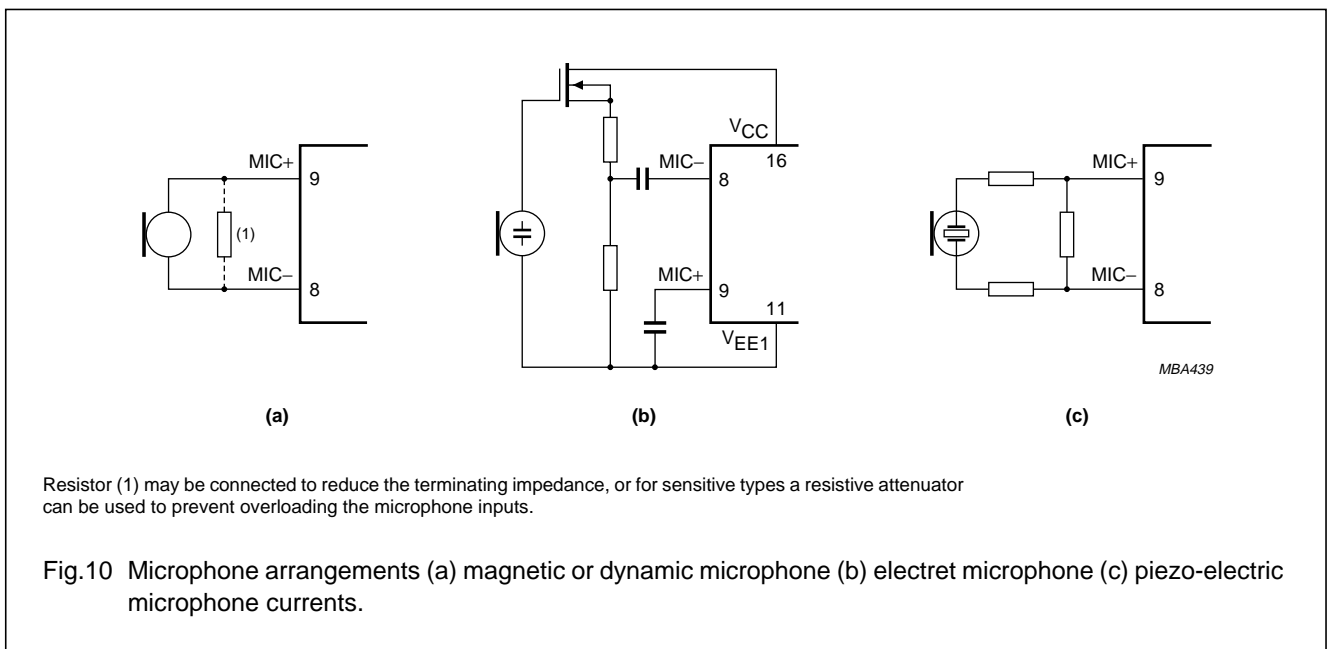
## TEA1064B

### Microphone inputs MIC+ and MIC- and gain pins GAS1 and GAS2

The TEA1064B has symmetrical microphone inputs, its input impedance is 64 kΩ (2 x 32 kΩ) and its voltage amplification is typically 52 dB with R7 = 68 kΩ. Either dynamic, magnetic or piezo-electric microphones can be used, or an electret microphone with a built-in FET buffer. Arrangements for the microphone types are shown in Fig.10.

The gain of the microphone amplifier is proportional to external resistor R7 connected between GAS1 and GAS2 and with this it can be adjusted between 44 dB and 52 dB to suit the sensitivity of the transducer.

An external 100 pF capacitor (C6) is required between GAS1 and SLPE to ensure stability. A larger value of C6 may be chosen to obtain a first-order low-pass filter with a cut-off frequency corresponding to the time constant R7 x C6.



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## Dynamic limiter (microphone) pin $\overline{\text{DLS/MMUTE}}$

A low level at the  $\overline{\text{DLS/MMUTE}}$  pin inhibits the microphone inputs MIC+ and MIC- but has no influence on the receiving and DTMF amplifiers.

Removing the low level at the  $\overline{\text{DLS/MMUTE}}$  pin provides the normal function of the microphone amplifier after a short time determined by the capacitor connected to  $\overline{\text{DLS/MMUTE}}$  pin. The microphone mute function can be realised by a simple switch as shown in Fig.11.

To prevent distortion of the transmitted signal, the gain of the sending amplifier is reduced rapidly when peaks of the signal on the line exceed an internally-determined threshold. The time in which gain reduction is effected (attack time) is very short. The circuit stays in the gain-reduced condition until the peaks of the sending signal remain below the threshold level. The sending gain then returns to normal after a time determined by the capacitor connected to  $\overline{\text{DLS/MMUTE}}$  (release time).

The internal threshold adapts automatically to the DC voltage setting of the circuit ( $V_{\text{LN-SLPE}}$ ). This means that the maximum output swing on the line will be higher if the DC voltage dropped across the circuit is increased. Fig.12 shows the maximum possible output swing on the line as a function of the DC voltage drop ( $V_{\text{LN-SLPE}}$ ) with  $I_{\text{line}} - I_p$  as a parameter.

The internal threshold level is lowered automatically if the DC current in the transmit output stage is insufficient. This prevents distortion of the sending signal in applications using parallel-connected telephones or telephones operating over long lines, for example.

Dynamic limiting also considerably improves sidetone performance in over-drive conditions (less distortion; limited sidetone level).

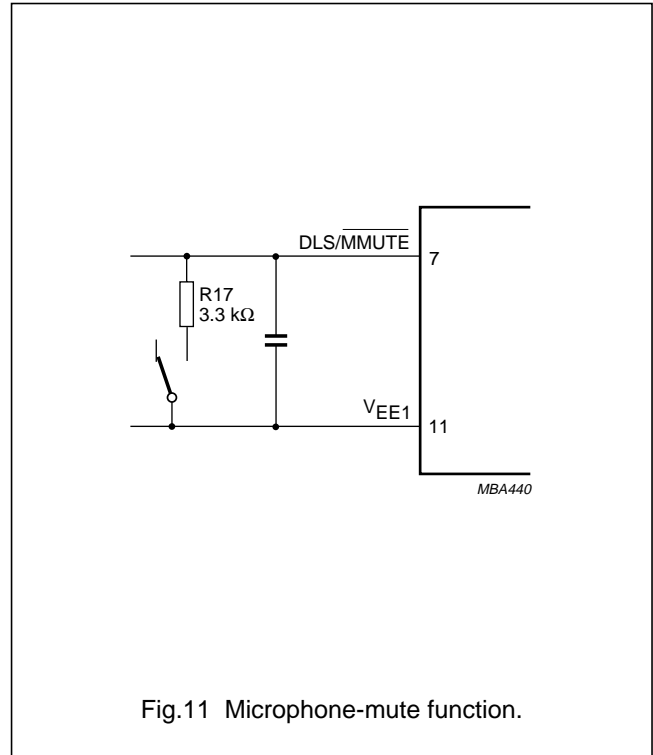
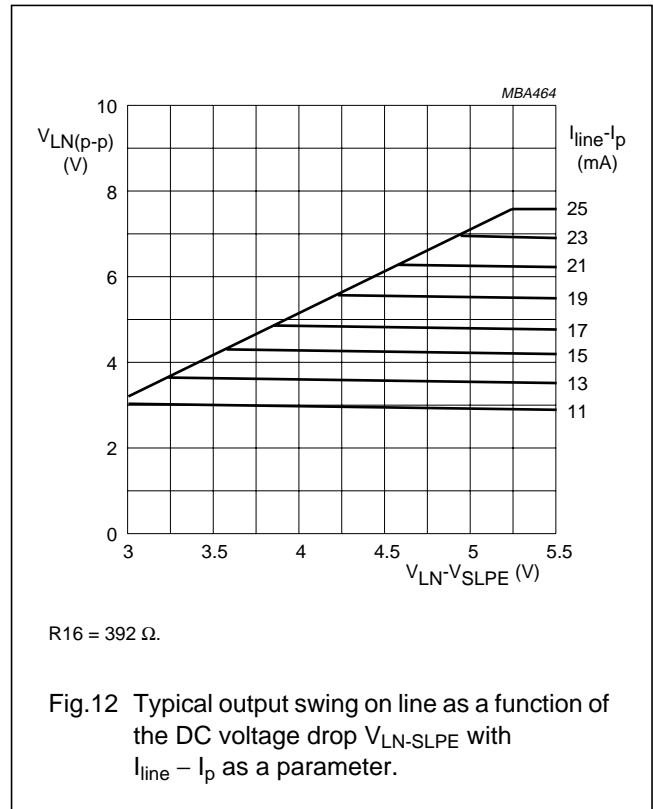


Fig.11 Microphone-mute function.



R16 = 392 Ω.

Fig.12 Typical output swing on line as a function of the DC voltage drop  $V_{\text{LN-SLPE}}$  with  $I_{\text{line}} - I_p$  as a parameter.

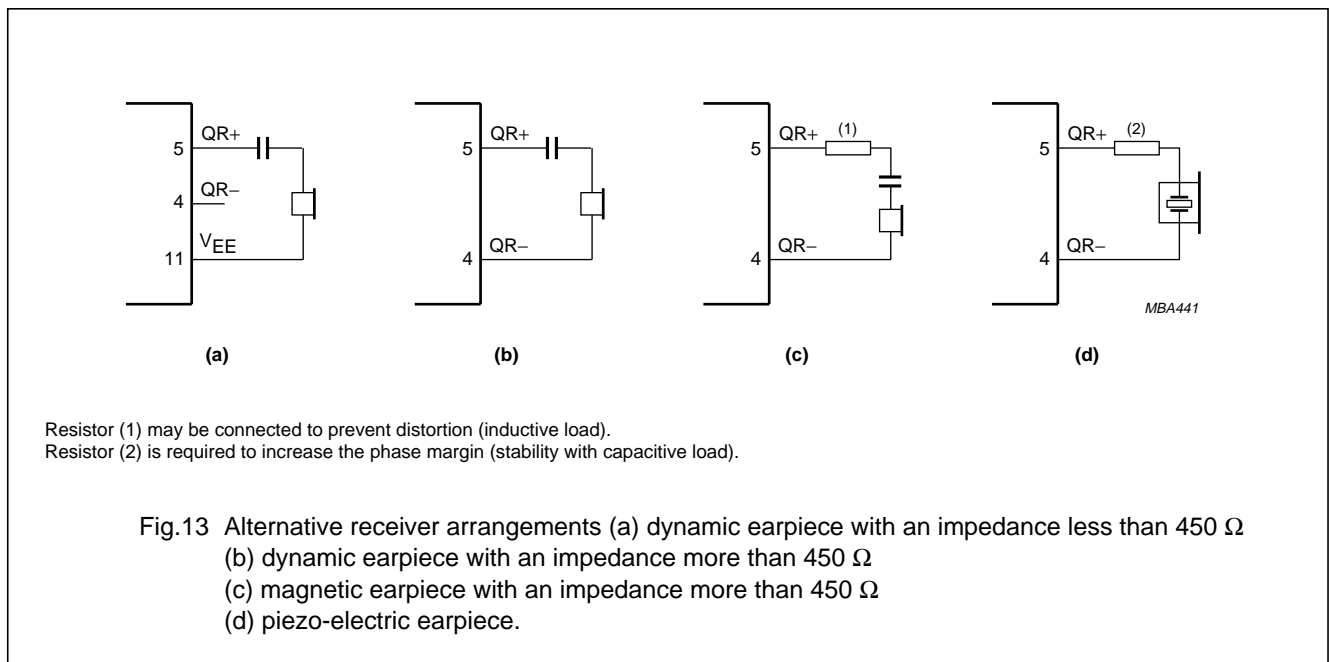
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### Receiving amplifier IR, QR+, QR- and GAR

The receiving amplifier has one input IR and two complimentary outputs, QR+ (non-inverting) and QR- (inverting). These outputs may be used for single-ended or differential drive, depending on the type and sensitivity of the earpiece used (see Fig.13). Gain from IR to QR+ is typically 31 dB with  $R_4 = 100\text{ k}\Omega$ , sufficient for

low-impedance magnetic or dynamic earpieces which are suitable for single-ended drive. By using both outputs (differential drive) the gain is increased by 6 dB. Differential drive can be used when the earpiece impedance exceeds  $450\ \Omega$  as with high-impedance dynamic, magnetic or piezo-electric earpieces.



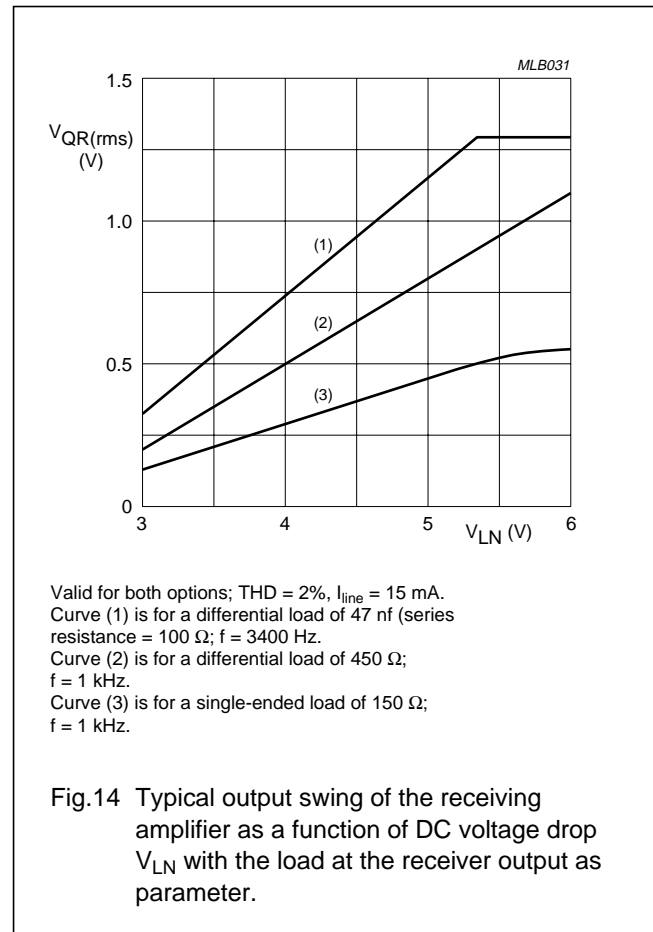
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The output voltage of the receiving amplifier is specified for continuous-wave drive. Fig. 14 shows the maximum output swing of the receiving amplifier as a function of the DC voltage drop ( $V_{LN}$ ). The maximum output voltage will be higher under speech conditions, where the ratio of the peak to the RMS value is higher.

The gain of the receiving amplifier can be adjusted to suit the sensitivity of the transducer used. The adjustment range is between 20 dB and 39 dB with single-ended drive and between 26 dB and 45 dB with differential drive. The gain is proportional to the external resistor R4 connected between GAR and QR+. The overall gain between LN and QR+ can be found by subtracting the attenuation of the anti-sidetone network (32 dB) from the amplifier gain.

Two external capacitors ( $C4 = 100$  pF and  $C7 = 10 \times C4 = 1$  nF) ensure stability. A larger value may be chosen to obtain a first-order low-pass filter. The cut-off frequency corresponds with time constant  $R4 \times C4$ . The relationship  $C7 = 10 \times C4$  must be maintained.



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### Automatic gain control input AGC

Automatic compensation of line loss is obtained by connecting a resistor (R6) between AGC and  $V_{EE1}$ .

This automatic gain control varies the gain of the microphone amplifier and receiving amplifier in accordance with the DC line current. The control range is 6.1 dB; this corresponds to a 5 km line of 0.5 dB diameter copper twisted-pair cable (DC resistance = 176  $\Omega$ /km, average attenuation = 1.2 dB/km). The DTMF gain is not affected by this feature.

The value of R6 must be chosen with reference to the exchange supply voltage and its feeding bridge resistance (see Fig.15 and Table 1). Different values of R6 give the same line current ratios at the start and the end of the control range. If automatic line-loss compensation is not required the AGC pin can be left open-circuit, the amplifiers then provide their maximum gain.

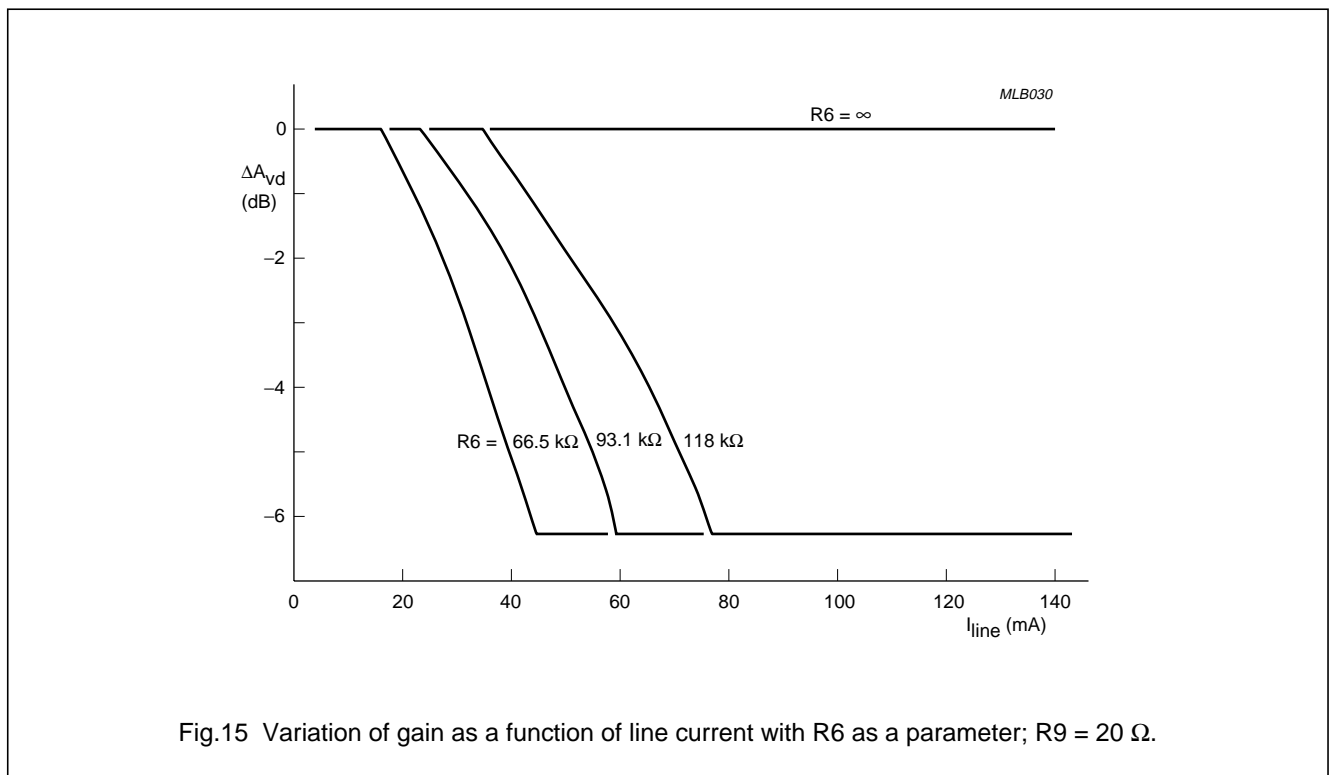


Fig.15 Variation of gain as a function of line current with R6 as a parameter; R9 = 20  $\Omega$ .

**Table 1** Values of R6 giving optimum line-loss compensation at various values of exchange supply voltage ( $V_{exch}$ ) and exchange feeding bridge resistance ( $R_{exch}$ ); R9 = 20  $\Omega$

		$R_{exch}$ ( $\Omega$ )			
		400	600	800	1000
		$R6$ (k $\Omega$ )			
$V_{exch}$ (V)	35	84.5	66.5	x	x
	48	118	93.1	77.8	66.5
	60	x	x	97.6	84.5

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### V<sub>EE2</sub> input

V<sub>EE2</sub> is the reference for MUTE, POWER-DOWN and DTMF inputs. These signals are referenced to V<sub>EE1</sub> when generated by peripherals powered between V<sub>CC</sub> and V<sub>EE1</sub>, but they can also be referenced to SLPE when peripherals are powered as shown in Fig.3. In the first instance (reference to V<sub>EE1</sub>), V<sub>EE2</sub> has to be connected to V<sub>EE1</sub>. In the second instance (reference to SLPE), V<sub>EE2</sub> has to be connected to SLPE.

### MUTE input (see notes 1 and 2)

MUTE = HIGH enables the DTMF input and inhibits the microphone and receiving amplifier inputs.

MUTE = LOW or open-circuit disables the DTMF input and enables the microphone and receiving amplifier inputs.

Switching MUTE gives negligible clicks at the telephone outputs and on the line.

### Dual-tone multi-frequency input DTMF (see note 1)

When the DTMF input is enabled, dialling tones may be sent on the line. The voltage gain between DTMF-V<sub>EE2</sub> and LN-V<sub>EE1</sub> is typically 26.5 dB less than the gain of the microphone amplifier and varies with R7 in the same way as the gain of the microphone amplifier. This means that the tone level at the DTMF input has to be adjusted after setting the gain of the microphone amplifier.

With R7 = 68 kΩ the gain is typically 25.5 dB.

The signalling tones can be heard in the earpiece at a low level (confidence tone).

### Power-down input PD (see notes 1. and 2.)

During pulse dialling or register recall (timed loop break) the telephone line is interrupted; as a consequence it provides no supply for the transmission circuit connected to V<sub>CC</sub> or for the peripherals between V<sub>LN</sub> and SLPE.

These supply gaps are bridged by the charges in the capacitors C1 and C15. The requirements on these capacitors are eased by an applied HIGH level to the PD input during the time of the loop break. This reduces the internal supply current I<sub>CC1</sub> from 1.3 mA (typ.) to 60 μA (typ.) and switches off the voltage regulator to prevent discharge via LN to V<sub>CC2</sub>.

A HIGH level at PD also internally disconnects the capacitor at REG so that the voltage stabilizer has no switch-on delay after line interruptions. This minimizes the contribution of the IC to the current waveform during pulse dialling or register recall.

When the power-down facility is not required, the PD pin can be left open-circuit or connected to V<sub>EE2</sub>.

### Sidetone suppression

Suppression of the transmitted signal in the earpiece is obtained by the anti-sidetone network comprising R1//Z<sub>line</sub>, R2, R3, R8, R9 and Z<sub>bal</sub> (see Fig.16). Maximum compensation is obtained when the following conditions are fulfilled:

$$(a) \quad R9 \times R2 = R1 \times (R3 + \{R8/Z_{bal}\})$$

$$(b) \quad (Z_{bal}/\{Z_{bal} + R8\}) = (Z_{line}/\{Z_{line} + R1\})$$

If fixed values are chosen for R1, R2, R3 and R9, then condition (a) is always fulfilled provided  $|R8/Z_{bal}| \ll R3$

To obtain optimum sidetone suppression, condition (b) has to be fulfilled, resulting in:

$$Z_{bal} = (R8/R1) \times Z_{line} = k \times Z_{line}$$

Where k is a scale factor;  $k = (R8/R1)$ .

The scale factor k (value of R8) is chosen to meet the following criteria:

- compatibility with a standard capacitor from the E6 or E12 range for Z<sub>bal</sub>
- $|Z_{bal}/R8| \ll R3$  to fulfil condition (a) and thus ensure correct anti-sidetone bridge operation
- $|Z_{bal} + R8| \gg R9$  to avoid influencing the transmit gain

In practise Z<sub>line</sub> varies considerably with the line length and line type. Therefore the value chosen for Z<sub>bal</sub> should be for an average line length giving satisfactory sidetone suppression with short and long lines. The suppression also depends on the accuracy of the match between Z<sub>bal</sub> and the impedance of the average line.

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**EXAMPLE**

The line impedance for which optimum suppression is to be obtained can be represented by  $210 \Omega + (1265 \Omega // 140 \text{ nF})$ . This represents a 5 km line of 0.5 mm diameter copper twisted-pair cable matched with  $600 \Omega (176 \Omega/\text{km}; 38 \text{ nF}/\text{km})$ .

With  $k = 0.64$  this results in :  $R_8 = 390 \Omega$ ;  
 $Z_{bal} = 130 \Omega + (820 \Omega // 220 \text{ nF})$ .

The anti-sidetone network for the TEA1060 family shown in Fig.16 attenuates the signal received from the line by 32 dB before it enters the receiving amplifier. The attenuation is almost constant over the whole audio-frequency range.

Alternatively a conventional Wheatstone bridge can be used as an anti-sidetone circuit (see Fig.17). Both bridge types can be used with either resistive or complex set impedances. (More information on the balancing of anti-sidetone bridges can be obtained in our publication "Versatile speech transmission ICs for electronic telephone sets", order number 9398 341 10011).

**Notes**

1. The reference level used for the MUTE, DTMF and PD inputs is  $V_{EE2}$ .
2. A LOW level for any of these pins is defined by connection to  $V_{EE2}$ , a HIGH level is defined as a voltage greater than  $V_{EE2} + 1.5 \text{ V}$  and smaller than  $V_{CC} + 0.4 \text{ V}$ .

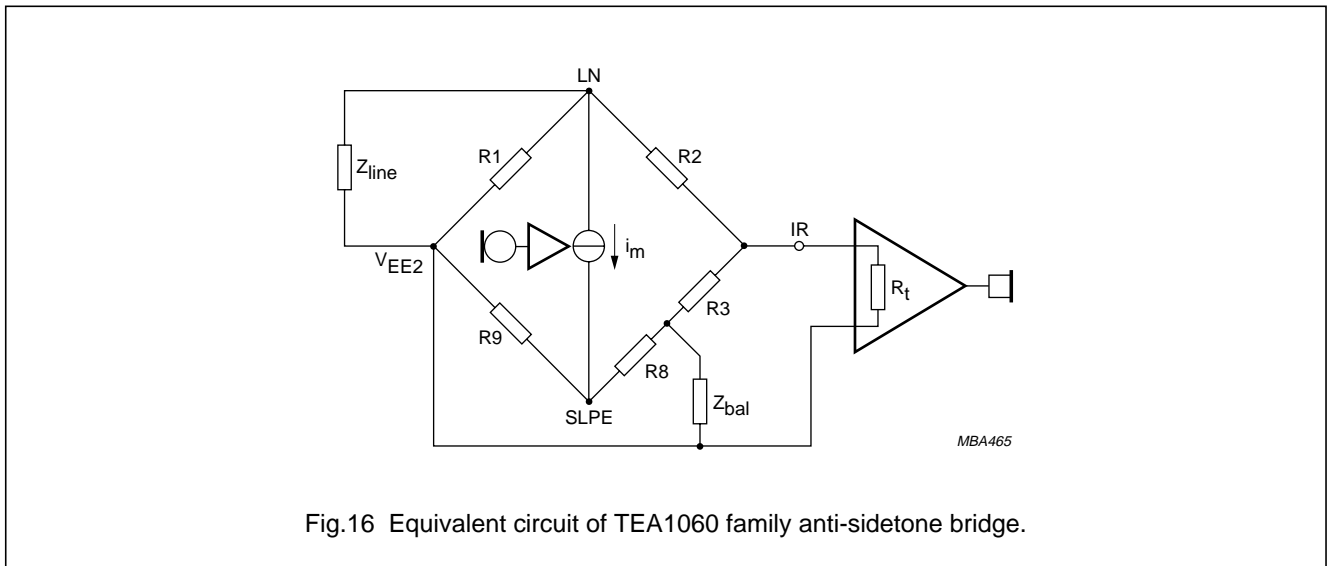


Fig.16 Equivalent circuit of TEA1060 family anti-sidetone bridge.

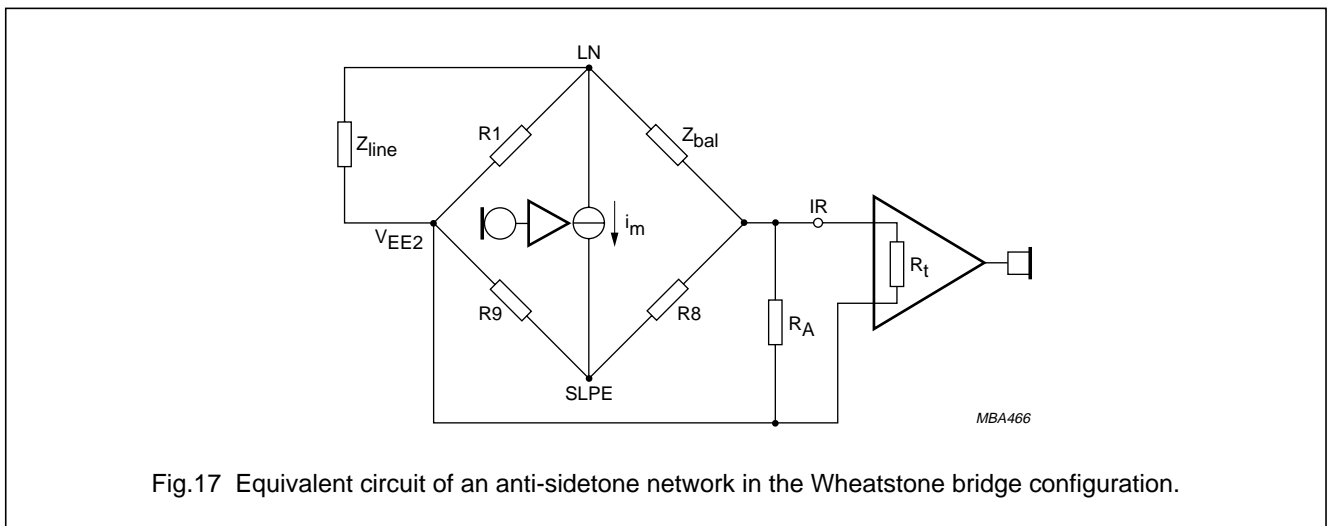


Fig.17 Equivalent circuit of an anti-sidetone network in the Wheatstone bridge configuration.



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## LIMITING VALUES

In accordance with the Absolute Maximum System (IEC134).

SYMBOL	PARAMETER	CONDITIONS	MIN.	MAX.	UNIT
$V_{LN}$	positive line voltage continuous		–	12	V
$V_{LN}$	repetitive line voltage during switch-on line interruption		–	13.2	V
$V_{LN}$	repetitive peak line voltage one 1 ms pulse per 5 s	R9 = 20 $\Omega$ ; R10 = 13 $\Omega$ ; see Fig.22	–	28	V
$I_{LN}$	line current	R9 = 20 $\Omega$			
	TEA1064B	note 1	–	140	mA
	TEA1064BT	note 1	–	140	mA
$V_i$	input voltage on pins other than LN		$V_{EE1}-0.7$	$V_{CC}+0.7$	V
$P_{tot}$	total power dissipation	R9 = 20 $\Omega$ ; note 2			
	TEA1064B		–	717	mW
	TEA1064BT		–	555	mW
$T_{amb}$	operating ambient temperature		–25	+75	$^{\circ}\text{C}$
$T_{stg}$	storage temperature		–40	+125	$^{\circ}\text{C}$
$T_j$	junction temperature		–	+125	$^{\circ}\text{C}$

### Notes

1. Mostly dependent on the maximum required  $T_{amb}$  and on the voltage between LN and SLPE. See Figs 18 and 19 to determine the current as a function of the required voltage and the temperature.
2. Calculated for the maximum ambient temperature specified  $T_{amb} = 75\text{ }^{\circ}\text{C}$  and a maximum junction temperature of  $125\text{ }^{\circ}\text{C}$ .

## THERMAL RESISTANCE

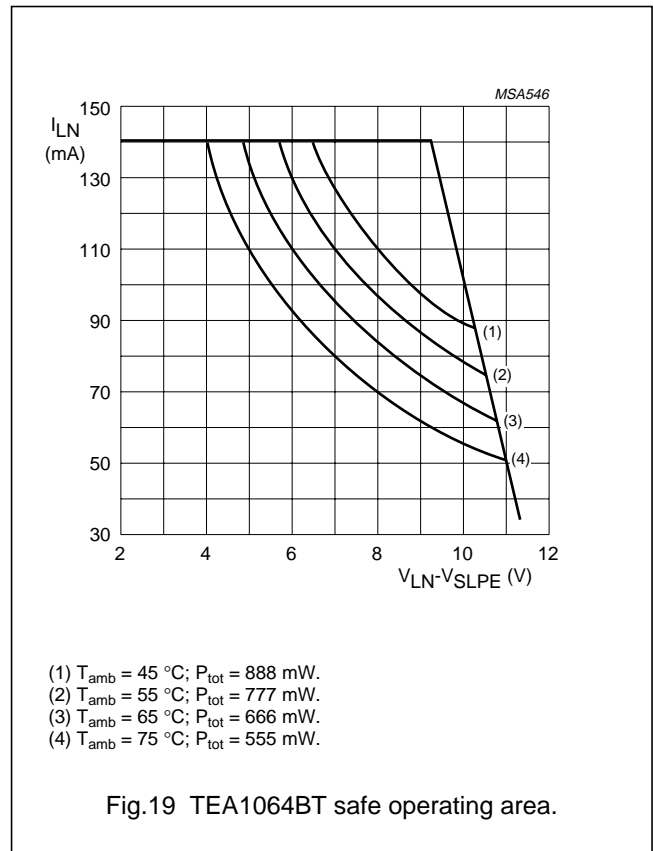
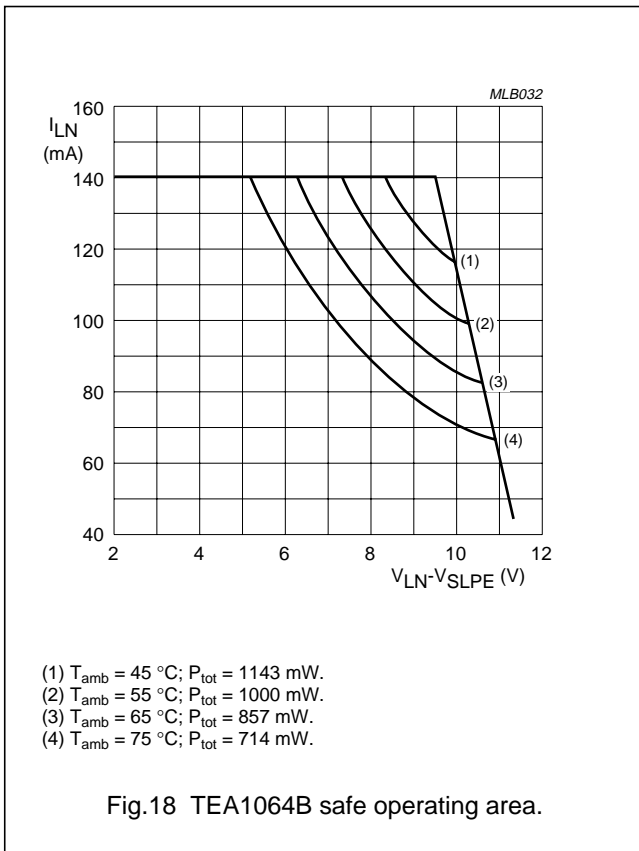
SYMBOL	PARAMETER	THERMAL RESISTANCE
$R_{th\ j-a}$	from junction to ambient in free air	
	SOT146	70 K/W
	SOT163A (note 1)	90 K/W

### Note

1. Mounted on glass epoxy board  $41 \times 19 \times 1.5\text{ mm}$ .

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TEA1064B



# Low voltage versatile telephone transmission circuit with dialler interface and transmit level dynamic limiting

TEA1064B

**CHARACTERISTICS**

$I_{line} = 11$  to  $140$  mA;  $V_{EE1} = 0$  V;  $f = 800$  Hz;  $T_{amb} = 25$  °C;  $R_L = 600$   $\Omega$ ; tested in the circuits of Fig.20 or Fig.21;  $V_{EE2}$  connected to SLPE; unless otherwise specified.

SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
<b>Supplies LN and V<sub>CC</sub> (pins 1 and 16)</b>						
$V_{LN}$	DC line voltage: voltage drop between LN and $V_{EE1}$	MIC <sup>-</sup> , MIC <sup>+</sup> inputs open-circuit; without $R_{VA}$ $I_{line} = 2$ mA $I_{line} = 4$ mA $I_{line} = 7$ mA $I_{line} = 11$ mA $I_{line} = 15$ mA $I_{line} = 100$ mA $I_{line} = 140$ mA	– – – – 3.25 – –	1.8 2.2 3.2 3.4 3.5 5.25 6.1	– – – – 3.75 6.05 7.0	V V V V V V V
$\Delta V_{LN}/\Delta T$	variation with temperature	$I_{line} = 15$ mA	–3	–1	+1	mV/K
$V_{LN}$	voltage drop over circuit with $R_{VA}$ connected between REG and SLPE	$R_{VA} = 33$ k $\Omega$ $R_{VA} = 20$ k $\Omega$	3.8 4.05	4.1 4.4	4.4 4.75	V V
$I_{CC}$	internal supply current into pin 16	$V_{CC} = 2.8$ V PD = LOW PD = HIGH	– –	1.3 60	1.6 82	mA $\mu$ A
$V_{CC}$	supply voltage available for peripheral circuitry $V_{EE2}$ connected to $V_{EE1}$	$I_{line} = 15$ mA; MUTE = HIGH; see Fig.5 $I_p = 0.54$ mA $I_p = 0$ mA	2.2 2.5	2.4 2.7	– –	V V
$V_p$	supply voltage available for peripheral circuitry	$I_{line} = 15$ mA $I_p = 1.4$ mA $I_p = 2.7$ mA; $R_{REG-SLPE} = 20$ k $\Omega$	2.5 2.9	2.7 3.1	– –	V V
<b>Microphone inputs MIC<sup>-</sup> and MIC<sup>+</sup> (pins 8 and 9)</b>						
$Z_i$	input impedance differential single-ended		51 25.5	64 32.0	77 38.5	k $\Omega$ k $\Omega$
CMRR	common mode rejection ratio		–	82	–	dB
$G_v$	voltage gain (see Fig.20)	$I_{line} = 15$ mA; $R_7 = 68$ k $\Omega$	51	52	53	dB
$\Delta G_v f$	variation of $G_v$ with frequency referred to 0.8 kHz	$f = 300$ and 3400 Hz	–0.5	$\pm 0.1$	+0.5	dB

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SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
$\Delta G_V T$	variation of $G_V$ with temperature referred to 25 °C	without R6; $I_{line} = 50 \text{ mA}$ ; $T_{amb} = -25 \text{ to } +75 \text{ °C}$	–	$\pm 0.2$	–	dB
<b>DTMF input (pin 12)</b>						
$Z_i$	input impedance		16.8	20.7	24.6	k $\Omega$
$G_V$	voltage gain (see Fig.20)	$I_{line} = 15 \text{ mA}$ ; $R7 = 68 \text{ k}\Omega$	24.5	25.5	26.5	dB
$\Delta G_V f$	variation of $G_V$ with frequency referred to 0.8 kHz	$f = 300 \text{ and } 3400 \text{ Hz}$ $f = 697 \text{ and } 1633 \text{ Hz}$	–0.5 –0.2	$\pm 0.01$ $\pm 0.05$	+0.5 +0.2	dB dB
$\Delta G_V T$	variation of $G_V$ with temperature referred to 25 °C	$I_{line} = 50 \text{ mA}$ ; $T_{amb} = -25 \text{ to } +75 \text{ °C}$	–	$\pm 0.2$	0.5	dB
<b>Gain adjustment inputs GAS1 and GAS2 (pins 2 and 3)</b>						
$\Delta G_V$	transmitting amplifier gain adjustment range		–8	–	+0	dB
<b>Sending amplifier output LN (pin 1)</b>						
DYNAMIC LIMITER						
$V_{LN(p-p)}$	output voltage swing (peak-to-peak value)	$I_{line} = 15 \text{ mA}$ ; $R7 = 68 \text{ k}\Omega$ ; $V_{i(RMS)} = 3.6 \text{ mV}$	3.4	3.8	4.2	V
THD	total harmonic distortion	$V_i = 3.6 \text{ mV } +10 \text{ dB}$ $V_i = 3.6 \text{ mV } +15 \text{ dB}$	– –	1.5 2.8	– –	% %
$V_{LN(p-p)}$	output voltage swing (peak-to-peak value)	$V_i = 3.6 \text{ mV } +10 \text{ dB}$ $I_p = 1.4 \text{ mA}$ $I_p = 2.7 \text{ mA}$ $I_p = 0 \text{ mA}; I_{line} = 7 \text{ mA}$ $I_p = 0 \text{ mA}; I_{line} = 4 \text{ mA}$	3.55 3.25 – –	3.8 3.5 1.8 0.9	4.05 3.75 – –	V V V V
$t_{att}$	dynamic behaviour of limiter attack time $V_{mic}$ jumps from 2 mV to 40 mV	$C16 = 470 \text{ nF}$	–	1.5	5.0	ms
$t_{rel}$	release time $V_{mic}$ jumps from 40 mV to 2 mV		50	150	–	ms
$V_{no(RMS)}$	noise output voltage (RMS value)	$I_{line} = 15 \text{ mA}$ ; $R7 = 68 \text{ k}\Omega$ ; 200 $\Omega$ between MIC– and MIC+; psophometrically weighted (P53 curve)	–	–72	–	dBmp

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SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
<b>Receiving amplifier input IR (pin 13)</b>						
$Z_i$	input impedance		17	21	25	$k\Omega$
<b>Receiving amplifier outputs QR- and QR+ (pins 4 and 5)</b>						
$Z_o$	output impedance	single-ended	–	4	–	$\Omega$
$G_v$	voltage gain (see Fig.21)	$I_{line} = 15 \text{ mA};$ $R_4 = 100 \text{ k}\Omega$				
	single-ended	$R_T = 300 \Omega$	30	31	32	dB
	differential	$R_T = 600 \Omega$	36	37	38	dB
$\Delta G_{vf}$	variation of $G_v$ with frequency referred to 0.8 kHz	$f = 300$ and $3400 \text{ Hz}$	–0.5	–0.2	0	dB
$\Delta G_{vT}$	variation of $G_v$ with temperature referred to $25 \text{ }^\circ\text{C}$	without $R_6$ ; $I_{line} = 50 \text{ mA};$ $T_{amb} = -25$ to $+75 \text{ }^\circ\text{C}$	–	$\pm 0.2$	–	dB
$V_{o(RMS)}$	output voltage (RMS value)	TDA = 2%; sinewave drive; $R_4 = 100 \text{ k}\Omega$ ; $I_{line} = 15 \text{ mA}$				
	single-ended	$R_T = 150 \Omega$	–	0.2	–	V
	differential	$R_T = 450 \Omega$	–	0.37	–	V
	differential	$C_T = 47 \text{ nF};$ $R_s = 100 \Omega$ ; $f = 3400 \text{ Hz}$	–	0.52	–	V
$V_{o(RMS)}$	output voltage (RMS value)	$I_p = 0 \text{ mA};$ TDA = 10%; sinewave drive; $R_4 = 100 \text{ k}\Omega$ ; $R_T = 150 \Omega$				
		$I_{line} = 4 \text{ mA}$ $I_{line} = 7 \text{ mA}$	–	20	–	mV
			–	160	–	mV
$V_{no(RMS)}$	noise output voltage (RMS value)	$I_{line} = 15 \text{ mA};$ $R_4 = 100 \text{ k}\Omega$ ; psophometrically weighted (P53 curve); pin IR open-circuit				
	single-ended	$R_T = 300 \Omega$	–	45	–	$\mu\text{V}$
	differential	$R_T = 600 \Omega$	–	90	–	$\mu\text{V}$
$V_{no(RMS)}$	noise output voltage (RMS value)	see Fig.21; S1 in position 2; $200 \Omega$ between MIC- and MIC+; single-ended; $R_T = 300 \Omega$				
		$R_7 = 68 \text{ k}\Omega$	–	100	–	$\mu\text{V}$
		$R_7 = 24.9 \text{ k}\Omega$	–	65	–	$\mu\text{V}$

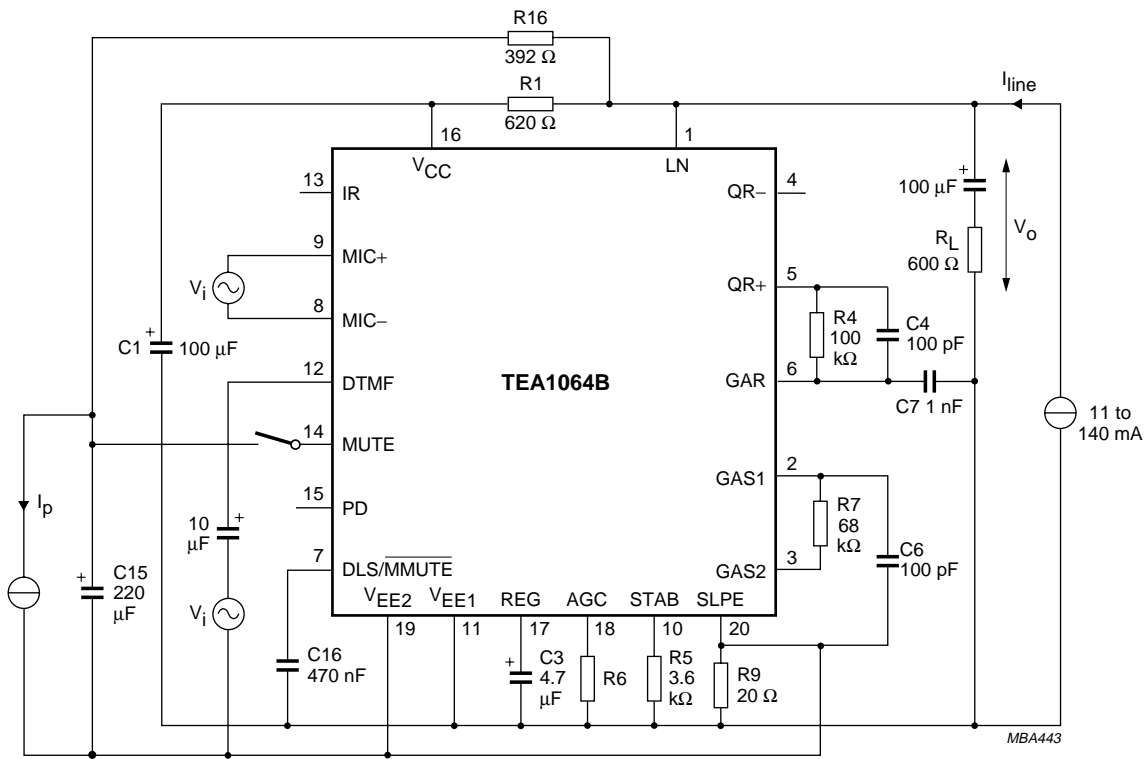
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SYMBOL	PARAMETER	CONDITIONS	MIN.	TYP.	MAX.	UNIT
<b>Gain adjustment input GAR (pin 6)</b>						
$\Delta G_v$	receiving amplifier gain adjustment range		-11	-	+8	dB
<b>MUTE input (pin 14)</b>						
$V_{IH}$	HIGH level input voltage		$1.5 + V_{EE2}$	-	$V_{CC} + 0.4$	V
$V_{IL}$	LOW level input voltage		0	-	$0.3 + V_{EE2}$	V
$I_{mute}$	input current		-	11	20	$\mu A$
$\Delta G_v$	change of microphone amplifier gain at mute on	MUTE = HIGH	-	-100	-	dB
$G_v$	voltage gain from input DTMF-SLPE to QR+ output with mute on	MUTE = HIGH; single-ended load; $R_L = 300 \Omega$	-	-18	-	dB
<b>Power-down input PD (pin 15)</b>						
$V_{IH}$	HIGH level input voltage		$1.5 + V_{EE2}$	-	$V_{CC1} + 0.4$	V
$V_{IL}$	LOW level input voltage		0	-	$0.3 + V_{EE2}$	V
$I_{PD}$	input current		-	5	10	$\mu A$
<b>Automatic gain control input AGC (pin 18)</b>						
$G_v$	controlling the gain from IR (pin 13) to QR+, QR- (pins 4, 5) and the gain from MIC+, MIC- (pins 8, 9) to LN (pin 1) gain control range with respect to $I_{line} = 15 \text{ mA}$	$R6 = 93.1 \text{ k}\Omega$ (between pins 18 and 11)  $I_{line} = 75 \text{ mA}$	-5.7	-6.1	-6.5	dB
$I_{line}$	highest line current for maximum gain		-	24	-	mA
$I_{line}$	lowest line current for minimum gain		-	61	-	mA
$\Delta G_v$	change of gain between $I_{line} = 15$ and $35 \text{ mA}$		-0.9	-1.4	-1.9	dB
<b>Microphone mute input DLS/MMUTE (pin 7)</b>						
$V_{IL}$	LOW level input voltage		$V_{EE1}$	-	$V_{EE1} + 0.3$	V
$I_{IL}$	input current at LOW level input voltage		-85	-60	-35	$\mu A$
$t_{rel}$	release time after a LOW level on pin 7	$C16 = 470 \text{ nF}$	-	30	-	ms
$\Delta G_v$	change of microphone amplifier gain at LOW level input voltage on pin 7		-	-100	-	dB

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For measuring gain from MIC+ and MIC- the MUTE input should be LOW or open-circuit.  
For measuring the DTMF input, the MUTE input should be HIGH.  
Inputs not being tested should be open-circuit.

Fig.20 Test circuit for defining voltage gain of MIC-, MIC+ and DTMF inputs; voltage gain ( $G_V$ ) is defined as  $20\log |V_o/V_i|$ .

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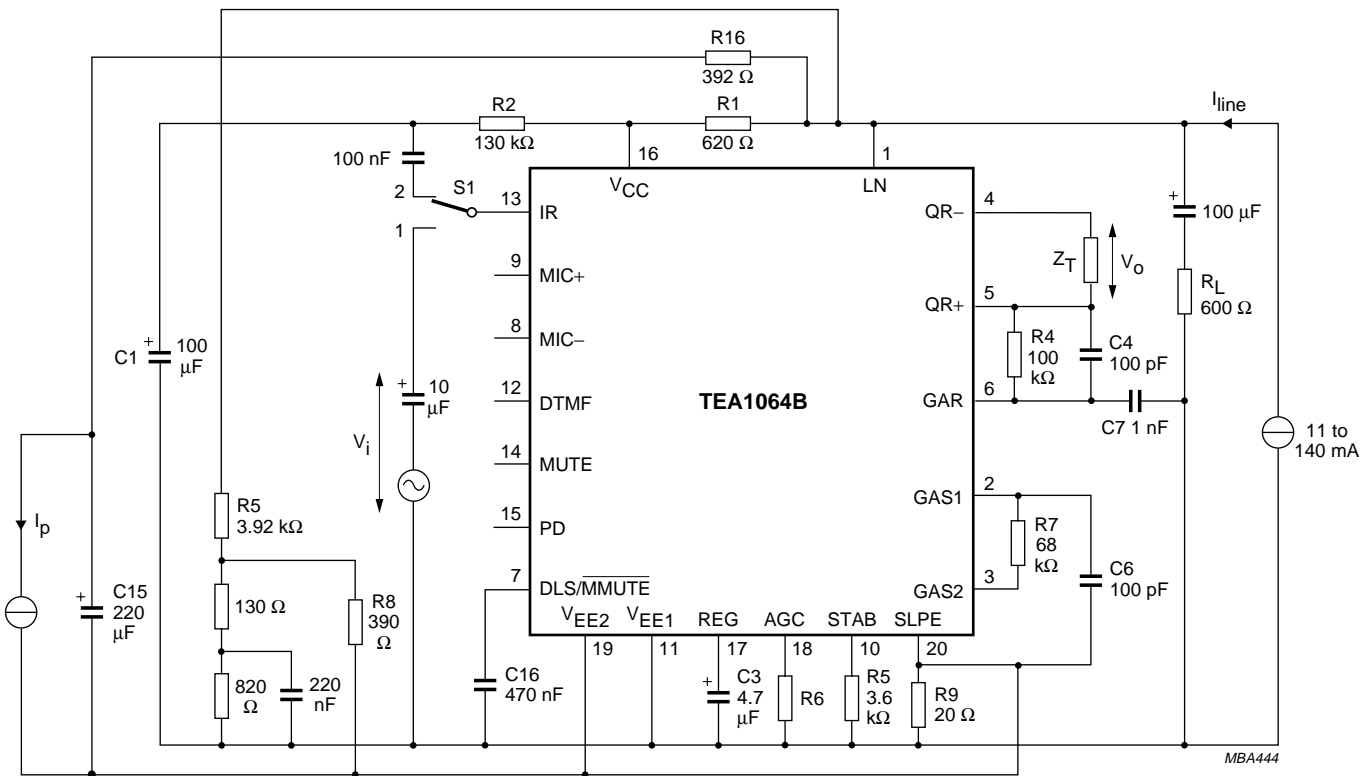


Fig.21 Test circuit for defining voltage gain of the receiving amplifier; voltage gain ( $G_v$ ) is defined as  $20 \log |V_o/V_i|$  (with S1 in position 1).

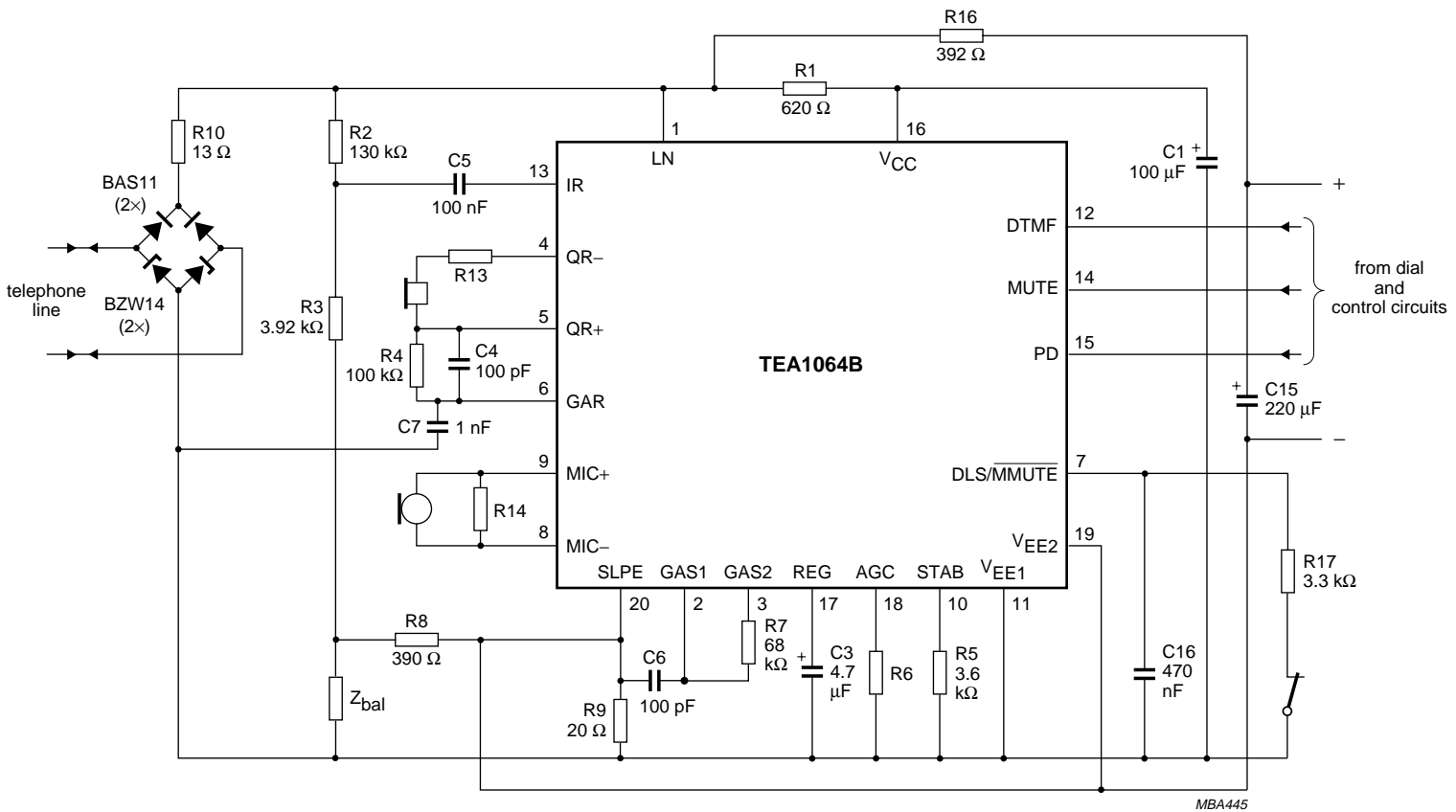


## Low voltage versatile telephone transmission circuit with dialler interface and transmit level dynamic limiting

### TEA1064B

#### APPLICATION INFORMATION

The basic application circuit is shown in Fig.22 and a typical application is shown in Fig.23.

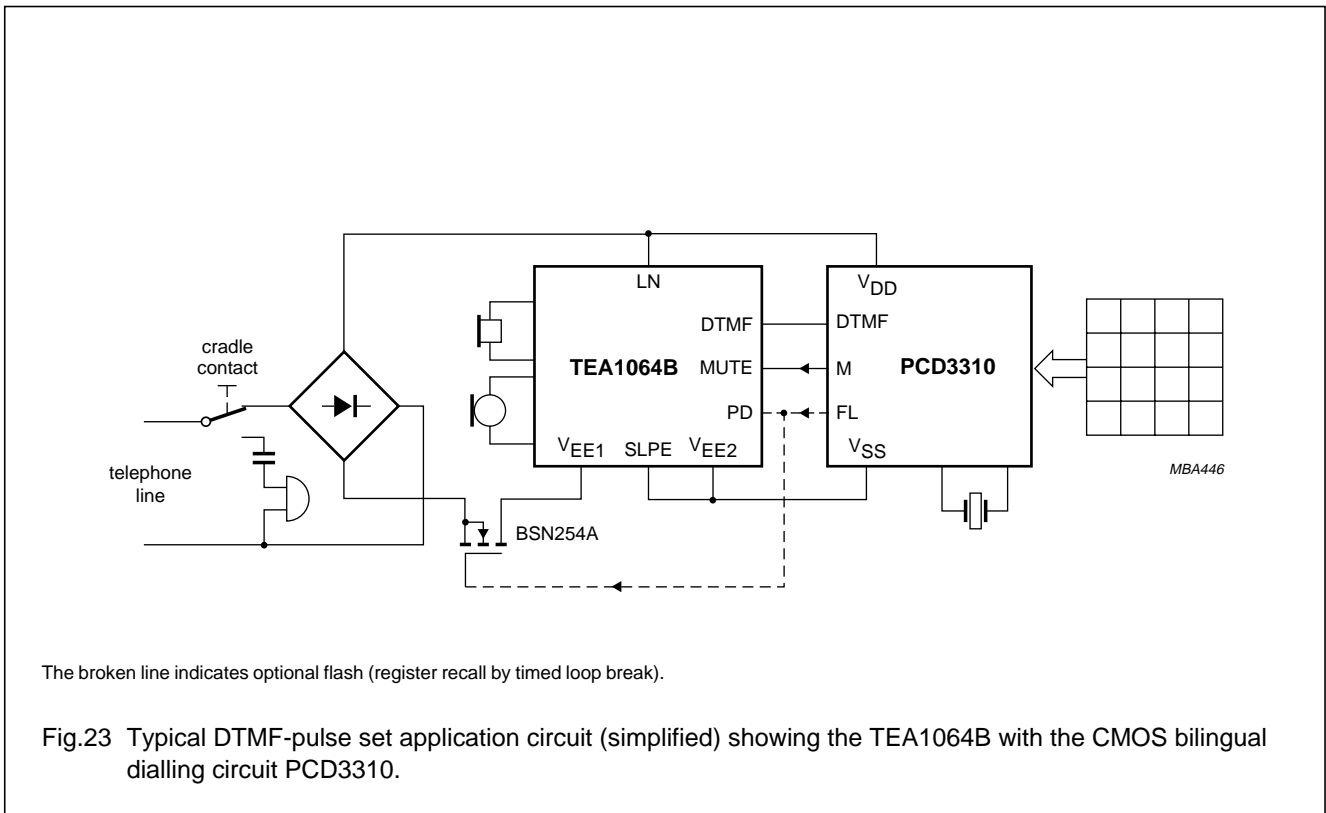


The diode bridge and R10 limit the current into, and the voltage across, the circuit during line transients. A different protection arrangement is required for pulse dialling or register recall.

Fig.22 Basic application of TEA1064B with SLPE as supply reference for peripherals, shown here with piezo-electric earpiece and DTMF dialling.

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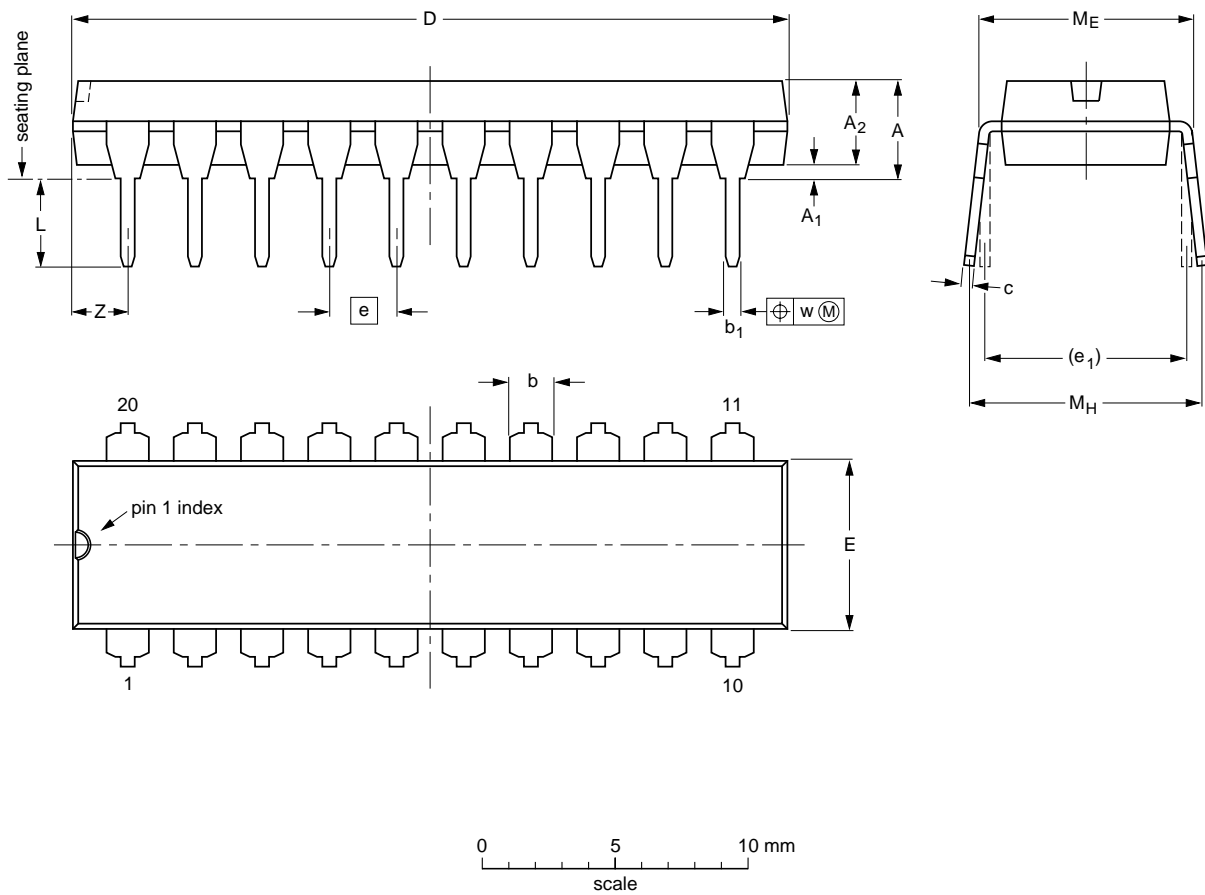
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PACKAGE OUTLINES

DIP20: plastic dual in-line package; 20 leads (300 mil)

SOT146-1



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

UNIT	A max.	A <sub>1</sub> min.	A <sub>2</sub> max.	b	b <sub>1</sub>	c	D <sup>(1)</sup>	E <sup>(1)</sup>	e	e <sub>1</sub>	L	M <sub>E</sub>	M <sub>H</sub>	w	Z <sup>(1)</sup> max.
mm	4.2	0.51	3.2	1.73 1.30	0.53 0.38	0.36 0.23	26.92 26.54	6.40 6.22	2.54	7.62	3.60 3.05	8.25 7.80	10.0 8.3	0.254	2.0
inches	0.17	0.020	0.13	0.068 0.051	0.021 0.015	0.014 0.009	1.060 1.045	0.25 0.24	0.10	0.30	0.14 0.12	0.32 0.31	0.39 0.33	0.01	0.078

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

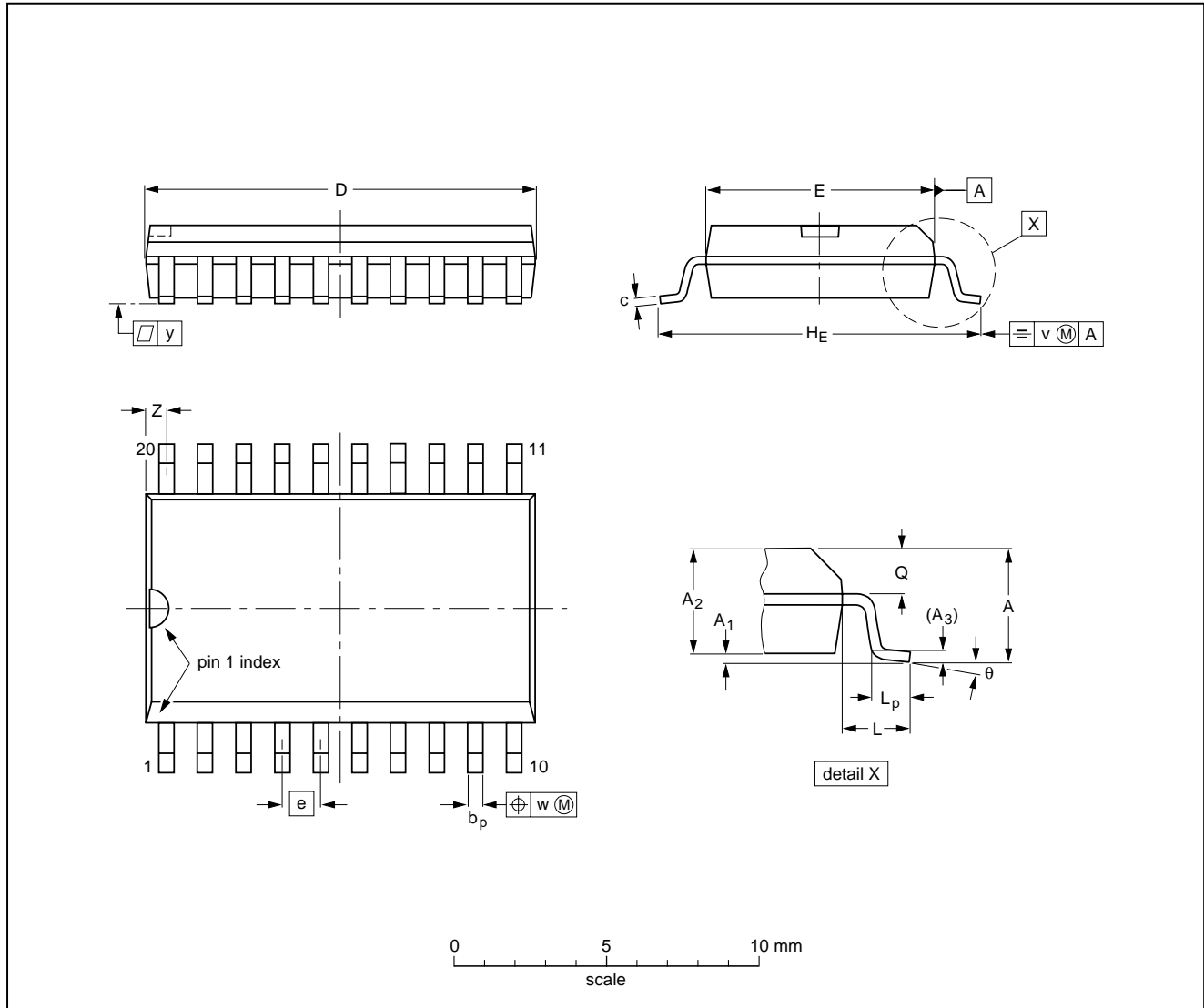
OUTLINE VERSION	REFERENCES				EUROPEAN PROJECTION	ISSUE DATE
	IEC	JEDEC	EIAJ			
SOT146-1			SC603			92-11-17 95-05-24

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SO20: plastic small outline package; 20 leads; body width 7.5 mm

SOT163-1



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

UNIT	A max.	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	b <sub>p</sub>	c	D <sup>(1)</sup>	E <sup>(1)</sup>	e	H <sub>E</sub>	L	L <sub>p</sub>	Q	v	w	y	Z <sup>(1)</sup>	θ
mm	2.65	0.30 0.10	2.45 2.25	0.25	0.49 0.36	0.32 0.23	13.0 12.6	7.6 7.4	1.27	10.65 10.00	1.4	1.1 0.4	1.1 1.0	0.25	0.25	0.1	0.9 0.4	8° 0°
inches	0.10	0.012 0.004	0.096 0.089	0.01	0.019 0.014	0.013 0.009	0.51 0.49	0.30 0.29	0.050	0.419 0.394	0.055	0.043 0.016	0.043 0.039	0.01	0.01	0.004	0.035 0.016	

Note

1. Plastic or metal protrusions of 0.15 mm maximum per side are not included.

OUTLINE VERSION	REFERENCES				EUROPEAN PROJECTION	ISSUE DATE
	IEC	JEDEC	EIAJ			
SOT163-1	075E04	MS-013AC				95-01-24 97-05-22

## Low voltage versatile telephone transmission circuit with dialler interface and transmit level dynamic limiting

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### SOLDERING

#### Introduction

There is no soldering method that is ideal for all IC packages. Wave soldering is often preferred when through-hole and surface mounted components are mixed on one printed-circuit board. However, wave soldering is not always suitable for surface mounted ICs, or for printed-circuits with high population densities. In these situations reflow soldering is often used.

This text gives a very brief insight to a complex technology. A more in-depth account of soldering ICs can be found in our *"Data Handbook IC26; Integrated Circuit Packages"* (order code 9398 652 90011).

#### DIP

##### SOLDERING BY DIPPING OR BY WAVE

The maximum permissible temperature of the solder is 260 °C; solder at this temperature must not be in contact with the joint for more than 5 seconds. The total contact time of successive solder waves must not exceed 5 seconds.

The device may be mounted up to the seating plane, but the temperature of the plastic body must not exceed the specified maximum storage temperature ( $T_{stg\ max}$ ). If the printed-circuit board has been pre-heated, forced cooling may be necessary immediately after soldering to keep the temperature within the permissible limit.

##### REPAIRING SOLDERED JOINTS

Apply a low voltage soldering iron (less than 24 V) to the lead(s) of the package, below the seating plane or not more than 2 mm above it. If the temperature of the soldering iron bit is less than 300 °C it may remain in contact for up to 10 seconds. If the bit temperature is between 300 and 400 °C, contact may be up to 5 seconds.

#### SO

##### REFLOW SOLDERING

Reflow soldering techniques are suitable for all SO packages.

Reflow soldering requires solder paste (a suspension of fine solder particles, flux and binding agent) to be applied to the printed-circuit board by screen printing, stencilling or pressure-syringe dispensing before package placement.

Several techniques exist for reflowing; for example, thermal conduction by heated belt. Dwell times vary between 50 and 300 seconds depending on heating method. Typical reflow temperatures range from 215 to 250 °C.

Preheating is necessary to dry the paste and evaporate the binding agent. Preheating duration: 45 minutes at 45 °C.

##### WAVE SOLDERING

Wave soldering techniques can be used for all SO packages if the following conditions are observed:

- A double-wave (a turbulent wave with high upward pressure followed by a smooth laminar wave) soldering technique should be used.
- The longitudinal axis of the package footprint must be parallel to the solder flow.
- The package footprint must incorporate solder thieves at the downstream end.

During placement and before soldering, the package must be fixed with a droplet of adhesive. The adhesive can be applied by screen printing, pin transfer or syringe dispensing. The package can be soldered after the adhesive is cured.

Maximum permissible solder temperature is 260 °C, and maximum duration of package immersion in solder is 10 seconds, if cooled to less than 150 °C within 6 seconds. Typical dwell time is 4 seconds at 250 °C.

A mildly-activated flux will eliminate the need for removal of corrosive residues in most applications.

##### REPAIRING SOLDERED JOINTS

Fix the component by first soldering two diagonally-opposite end leads. Use only a low voltage soldering iron (less than 24 V) applied to the flat part of the lead. Contact time must be limited to 10 seconds at up to 300 °C. When using a dedicated tool, all other leads can be soldered in one operation within 2 to 5 seconds between 270 and 320 °C.

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**DEFINITIONS**

<b>Data sheet status</b>	
Objective specification	This data sheet contains target or goal specifications for product development.
Preliminary specification	This data sheet contains preliminary data; supplementary data may be published later.
Product specification	This data sheet contains final product specifications.
<b>Limiting values</b>	
Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 134). Stress above one or more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation of the device at these or at any other conditions above those given in the Characteristics sections of the specification is not implied. Exposure to limiting values for extended periods may affect device reliability.	
<b>Application information</b>	
Where application information is given, it is advisory and does not form part of the specification.	

**LIFE SUPPORT APPLICATIONS**

These products are not designed for use in life support appliances, devices, or systems where malfunction of these products can reasonably be expected to result in personal injury. Philips customers using or selling these products for use in such applications do so at their own risk and agree to fully indemnify Philips for any damages resulting from such improper use or sale.

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**NOTES**

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