## KH600

## 1GHz, Differential Input/Output Amplifier

## Features

- DC - 1 GHz bandwidth
- Fixed $14 \mathrm{~dB}(5 \mathrm{~V} / \mathrm{V})$ gain
- $100 \Omega$ (differential) inputs and outputs
- -74/-64dBc 2nd/3rd HD at 50MHz
- 45 mA output current
- $9 \mathrm{~V}_{\mathrm{pp}}$ into $100 \Omega$ differential load
- 13,000V/us slew rate
- Optional supply current and offset voltage adjustment


## Applications

- ATE systems
- High-end instrumentation
- High bandwidth output amplifier
- Differential buffer
- Line driver


## General Description

The KH600 is the first amplifier to combine differential input and output with a bandwidth of $\mathrm{DC}-1 \mathrm{GHz}$ at $2 \mathrm{~V}_{\text {pp }}$. The inputs and outputs are $100 \Omega$ differential ( $50 \Omega$ single ended). The KH600 operates from $\pm 5 \mathrm{~V}$ supplies and offers a fixed gain of $14 \mathrm{~dB}(5 \mathrm{~V} / \mathrm{V})$.

The KH600 also offers optional supply current, differential output offset voltage, and common mode offset voltage adjustments.

The KH600 is constructed using Fairchild's in-house thin film resistor/bipolar transistor technology. The KH600 is available in a 12 -pin TO8 package.



## KH600 Electrical Characteristics

$$
\begin{array}{r}
\left(\mathrm{G}=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega \text { (differential), } \mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C},\right. \\
\left.+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{S}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{S}}=-5 \mathrm{~V} \text {; unless noted }\right)
\end{array}
$$

| Parameters | Conditions | TYP | Min \& Max | UNITS | NOTES |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Case Temperature |  | $+25^{\circ} \mathrm{C}$ | $+25^{\circ} \mathrm{C}$ |  |  |
| Frequency Domain Response <br> -3dB bandwidth <br> peaking <br> full power bandwidth linear phase deviation gain <br> input return loss (single-ended $50 \Omega$ ) <br> output return loss (single-ended $50 \Omega$ ) | $\mathrm{V}_{\mathrm{O}}=2 \mathrm{~V}_{\mathrm{pp}}$ <br> DC to 250 MHz <br> DC to 500 MHz <br> $\mathrm{V}_{\mathrm{O}}=8 \mathrm{~V}_{\mathrm{pp}}$ <br> DC to 500 MHz <br> 1 MHz <br> DC <br> DC $=250 \mathrm{MHz}$ <br> $D C=500 \mathrm{MHz}$ <br> $D C=500 \mathrm{MHz}$ | $\begin{gathered} 1000 \\ 0.2 \\ 0.5 \\ 350 \\ 3 \\ 14 \\ 14.3 \\ 22 \\ 14 \\ 27 \end{gathered}$ | $\pm 0.1$ | MHz dB dB MHz deg dB dB dB dB dB | 1 |
| Time Domain Response rise and fall time <br> overload recovery slew rate | 2V step <br> 8 V step $\mathrm{V}_{\mathrm{in}}=4 \mathrm{~V}_{\mathrm{pp}}$ <br> 8 V step | $\begin{gathered} 350 \\ 1 \\ 900 \\ 13,000 \end{gathered}$ |  | $\begin{gathered} \mathrm{ps} \\ \mathrm{~ns} \\ \mathrm{ps} \\ \mathrm{~V} / \mu \mathrm{s} \end{gathered}$ |  |
| Distortion and Noise Response 2nd harmonic distortion <br> 3rd harmonic distortion <br> input referred noise noise figure | $5 \mathrm{~V}_{\mathrm{pp}}, 50 \mathrm{MHz}$ <br> $2 \mathrm{~V}_{\mathrm{pp}}, 50 \mathrm{MHz}$ <br> $1 \mathrm{~V}_{\mathrm{pp}}, 200 \mathrm{MHz}$ <br> $5 \mathrm{~V}_{\mathrm{pp}}, 50 \mathrm{MHz}$ <br> $2 \mathrm{~V}_{\mathrm{pp}}, 50 \mathrm{MHz}$ <br> $1 \mathrm{Vpp}, 200 \mathrm{MHz}$ <br> $>1 \mathrm{MHz}$ | $\begin{gathered} 61 \\ 74 \\ 65 \\ 46 \\ 64 \\ 70 \\ 1.35 \\ 6.5 \end{gathered}$ | 61 57 | dBc dBc dBc dBc dBc dBc $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ dB | 1 <br> 1 |
| DC Performance <br> output offset voltage <br> average drift <br> power supply rejection ratio ( $\pm \mathrm{V}_{\mathrm{s}}$ ) <br> supply current | I/O's terminated into $50 \Omega$ to GND <br> DC <br> $\pm \mathrm{V}_{\mathrm{s}}$ pins <br> $\pm \mathrm{V}_{\mathrm{b}}$ pins ( $+\mathrm{V}_{\mathrm{b} 1}$ shorted to $+\mathrm{V}_{\mathrm{b} 2}$ ) | $\begin{gathered} -18 \\ 200 \\ 55 \\ 67 \\ 22 \end{gathered}$ | $\begin{aligned} & \pm 60 \\ & \\ & 70 \\ & 24 \end{aligned}$ | mV <br> $\mu \mathrm{V} /{ }^{\circ} \mathrm{C}$ <br> dB <br> mA <br> mA | 1 1 |
| Output Characteristics output voltage swing output current | differential | $\begin{gathered} 9 \\ \pm 45 \end{gathered}$ |  | $\begin{aligned} & \mathrm{V}_{\mathrm{pp}} \\ & \mathrm{~mA} \end{aligned}$ |  |
| Recommended Operating Conditions total supply voltage $-V_{b}$ <br> $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ <br> input voltage (relative to gain) | $\left(+V_{s}\right.$ to $\left.-V_{s}\right)$ | $\begin{gathered} 4 \text { to } 12 \\ 0 \text { to }-12 \\ 0 \text { to } 12 \\ \pm 2 \end{gathered}$ |  | V V V V |  |

$\mathrm{Min} / \mathrm{max}$ ratings are based on product characterization and simulation. Individual parameters are tested as noted. Outgoing quality levels are determined from tested parameters.

## NOTES:

1) $100 \%$ tested at $25^{\circ} \mathrm{C}$.

## Absolute Maximum Ratings

total supply voltage
maximum junction temperature
storage temperature range lead temperature ( 10 sec )

## KH600 Package

$$
\begin{array}{r}
15 \mathrm{~V} \\
+150^{\circ} \mathrm{C} \\
-65^{\circ} \mathrm{C} \text { to }+150^{\circ} \mathrm{C} \\
+300^{\circ} \mathrm{C}
\end{array}
$$



NOTE: Case is grounded.

## KH600 Performance Characteristics





( $G=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C}$,
$+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{s}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{s}}=-5 \mathrm{~V}$; unless noted)





## KH600 Performance <br> Characteristics



2nd Harmonic Distortion vs. Vo


Single Tone Intercept Point


( $\mathrm{G}=+5 \mathrm{~V} / \mathrm{V}\left(14 \mathrm{~dB}\right.$ ), $\mathrm{R}_{\mathrm{L}}=100 \Omega$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C}$, $+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{s}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{s}}=-5 \mathrm{~V}$; unless noted)


3rd Harmonic Distortion vs. $\mathrm{V}_{\mathbf{o}}$

-1dB Compression



## KH600 Performance Characteristics



Low Frequency Gain vs. Temperature

( $G=+5 \mathrm{~V} / \mathrm{V}(14 \mathrm{~dB}), \mathrm{R}_{\mathrm{L}}=100 \Omega$ (differential), $\mathrm{T}_{\mathrm{a}}=+25^{\circ} \mathrm{C}$,
$+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{s}}=+5 \mathrm{~V},-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{s}}=-5 \mathrm{~V}$; unless noted)



## Pin Description

| Pin \#'s | Name | Function |
| :---: | :---: | :--- |
| 6,10 | $+\mathrm{V}_{\mathrm{s}}$ | Positive supply voltage |
| 8 | $-\mathrm{V}_{\mathrm{s}}$ | Negative supply voltage |
| 11 | $+\mathrm{V}_{\mathrm{b} 1}$ | Positive bias voltage for OUT1 |
| 5 | $+\mathrm{V}_{\mathrm{b} 2}$ | Positive bias voltage for OUT2 |
| 2 | $-\mathrm{V}_{\mathrm{b}}$ | Negative bias voltage for OUT1 and OUT2 |
| 1 | IN1 | Input 1, +IN |
| 3 | IN2 | Input 2, -IN |
| 9 | OUT1 | Output 1, +OUT |
| 7 | OUT2 | Output 2, -OUT |
| 4,12 | GND | Input termination ground and case |

## General Description

## Standard Operation:

$$
\begin{aligned}
& +V_{b 1}=+V_{b 2}=+V_{s}=+5 \mathrm{~V} ; \\
& -V_{b}=-V_{s}=-5 \mathrm{~V}
\end{aligned}
$$

The KH600 is a 1 GHz differential input/output amplifier constructed using Fairchild's in-house thin film resistor/ bipolar transistor technology. A differential signal on the inputs of the KH600 will generate a differential signal at the outputs. If a single ended input signal is applied to IN1 and a fixed voltage to IN2, the KH600 will produce both a differential and common-mode output signal. To achieve the maximum dynamic range, center the inputs halfway between $+\mathrm{V}_{\mathrm{s}}$ and $-\mathrm{V}_{\mathrm{s}}$.

The KH600 includes $50 \Omega$ resistors from each input to ground, resulting in a differential input impedance of $100 \Omega$. Each KH600 output has a $50 \Omega$ resistance, synthesized by feedback, providing a $100 \Omega$ differential output impedance.

The KH600 has 3 bias voltage pins that can be used to:
Adjust the supply current

- Trim the differential output offset voltage
- Adjust the common mode output offset voltage over a $\pm 3 \mathrm{~V}$ range
If these adjustments are not required, short $+\mathrm{V}_{\mathrm{b} 1}$ and $+V_{b 2}$ to $+V_{s}$ and $-V_{b}$ to $-V_{s}$ as shown in Figure 1. Throughout this data sheet, this configuration ( $+\mathrm{V}_{\mathrm{b} 1}=$ $+\mathrm{V}_{\mathrm{b} 2}=+\mathrm{V}_{\mathrm{s}}=+5 \mathrm{~V}$ and $-\mathrm{V}_{\mathrm{b}}=-\mathrm{V}_{\mathrm{s}}=-5 \mathrm{~V}$ ) is referred to as the Standard Operating Condition. All of the plots in the Typical Performance section and the specifications in the Electrical Characteristics table utilize the basic circuit configuration shown in Figure 1, unless otherwise indicated.

Figure 2 illustrates the optional circuit configuration, utilizing the bias voltage pins. Further discussions regarding these optional adjustments are provided later in this document.


Figure 1: Basic Circuit Configuration


Figure 2: Optional Circuit Configuration (including optional supply current and offset adjust)

## Gain

Differential Gain for the KH600 is defined as (OUT1-OUT2)/(IN1-IN2). Applying identical (same phase) signals to both inputs and measuring one output will provide the Common Mode Gain. Figure 3 shows the differential and common mode gains of the KH600. Figure 4 illustrates the response of the KH600 outputs when one input is driven and the other is terminated into $50 \Omega$.


Figure 3: Differential and Common Mode Gain


Figure 4: Gain with Single-Ended Input Applied to IN1

## Supply Current

The KH600 draws supply current from the $2 \mathrm{~V}_{\mathrm{s}}$ pins as well as the $3 \mathrm{~V}_{\mathrm{b}}$ pins. Under Standard Conditions, the total supply current is typically 89 mA . Changing the voltages on the bias voltage pins will change their respective supply currents as shown in Figures 5 and 6.


Figure 5: $\mathrm{V}_{\mathrm{b}}$ Supply Currents vs $+\mathrm{V}_{\mathrm{b} 1}$
Changing the voltage on the $+\mathrm{V}_{\mathrm{b} 1}$ pin will alter the supply current for $+\mathrm{V}_{\mathrm{b} 1}$ only, $+\mathrm{V}_{\mathrm{b} 2}$ and $-\mathrm{V}_{\mathrm{b}}$ stay constant at typically 11 mA and 22 mA respectively. See Figure 5 . The same principle applies for $+\mathrm{V}_{\mathrm{b} 2}$. And Figure 6 illustrates the effect of changing $-\mathrm{V}_{\mathrm{b}}$.


Figure 6: $\mathrm{V}_{\mathrm{b}}$ Supply Currents vs $-\mathrm{V}_{\mathrm{b}}$

## Power Dissipation

The KH600 runs at "constant" power, which may be calculated by (Total $\left.\mathrm{I}_{\mathrm{s}}\right)\left(\mathrm{V}_{\mathrm{s}}-\left(-\mathrm{V}_{\mathrm{s}}\right)\right.$ ). Under standard operating conditions, the power is 890 mW . The power dissipated in the package is completely constant, independent of signal level. In other words, the KH600 runs class A.

## Power Supply Rejection Ratio (PSRR)

The KH600 has 5 supply pins, $+\mathrm{V}_{\mathrm{s}^{\prime}}-\mathrm{V}_{\mathrm{s}^{\prime}}+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$, and $-\mathrm{V}_{\mathrm{b}}$. All of these sources must be considered when measuring the PSRR. Figure 7 shows the response of $+\mathrm{V}_{\mathrm{s}}$ and $-\mathrm{V}_{\mathrm{s}^{\prime}}$ looking at OUT2. $+\mathrm{V}_{\mathrm{s}}$ and $-\mathrm{V}_{\mathrm{s}}$ have the same effect on OUT1.


Figure 7: $\pm \mathrm{V}_{\mathrm{s}}$ PSRR
Figure 8 shows the response of OUT1 and OUT2 when $+\mathrm{V}_{\mathrm{b} 1}$ changes. The PSRR of the $\mathrm{V}_{\mathrm{b}}$ pins is "bad", which means that they have a large effect on the response of the KH600 when their voltages are changed. This is the desired effect of the bias voltage pins. As Figure 8 indicates, changing $+\mathrm{V}_{\mathrm{b} 1}$ has a greater effect on OUT1 than it does on OUT2. Changing $+\mathrm{V}_{\mathrm{b} 1}$ has a direct effect on OUT1. Changing $+\mathrm{V}_{\mathrm{b} 2}$ has a direct effect on OUT2. See the Trimming Differential Output Offset Voltage section for more details.


Figure 8: $+\mathrm{V}_{\mathrm{b}}$ PSRR

## Single-to-Differential Operation

The KH600 is specifically designed for differential-todifferential operation. However, the KH600 can be used in a single-to-differential configuration with some performance degradation. The unused input should be terminated into $50 \Omega$. When driven single-ended, there will be a slight imbalance in the differential output voltages, see Figure 4. This imbalance is approximately 2.88 dB . To compensate for this imbalance, attenuate the higher gain output. (If the signal is applied to IN1, attenuate OUT1.)

## Unused Inputs and/or Outputs

For optimal performance, terminate any unused inputs and/or outputs with $50 \Omega$.

## Adjusting Supply Current

The KH600 operates class A, so maximum output current is directly proportional to supply current. Adjusting the voltages on $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ in opposition to $-\mathrm{V}_{\mathrm{b}}$ controls supply current. The default supply current of the KH600 has been optimized for best bandwidth and distortion performance. The main reason for adjusting supply current is to either reduce power or increase maximum output current. Adjusting the supply current will not significantly improve bandwidth or distortion and may actually degrade them.

To adjust the supply current, apply voltages of equal magnitude, but opposite polarity, to the bias voltage pins. For example, setting $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ to +5 VDC and $-\mathrm{V}_{\mathrm{b}}$ to -5VDC (as shown in Figure 2) results in the standard supply current condition. Setting $+\mathrm{V}_{\mathrm{b} 1},+\mathrm{V}_{\mathrm{b} 2}$ to +5.5 V and $-\mathrm{V}_{\mathrm{b}}$ to -5.5 V results in an approximate $10 \%$ increase in supply current. Figure 9 shows the how the total supply current of the KH600 is effected by changes in the bias voltages $\left(\mathrm{V}_{\mathrm{b}}=+\mathrm{V}_{\mathrm{b} 1}=+\mathrm{V}_{\mathrm{b} 2}=\left|-\mathrm{V}_{\mathrm{b}}\right|\right)$.


Figure 9: Total Supply Current vs. $\mathrm{V}_{\mathrm{b}}$
Supply current is relatively independent of the voltages on $+V_{s}$ and $-V_{s}$ as shown in Figure 10.


Figure 10: Total Supply Current vs. $\mathrm{V}_{\mathrm{s}}$


Figure 11: -3dB Bandwidth vs. $I_{s}$


Figure 12: Harmonic Distortion vs. Total $\mathrm{I}_{\mathrm{s}}$


Figure 13: Harmonic Distortion vs. Total $\mathrm{I}_{\mathrm{s}}$

## Trimming Differential Output Offset Voltage

Vary $+\mathrm{V}_{\mathrm{b} 1}$ and $+\mathrm{V}_{\mathrm{b} 2}$ to adjust differential offset voltage. $+\mathrm{V}_{\mathrm{b} 1}$ controls OUT1 and $+\mathrm{V}_{\mathrm{b} 2}$ controls OUT2. The output voltage moves in a direction opposite to the direction of the bias voltage. Figure 14 shows the resulting voltage change at OUT1 and OUT2 when the voltage on $+\mathrm{V}_{\mathrm{b} 1}$ is changed. Figure 15 shows the resulting voltage change at OUT1 and OUT2 when the voltage on $+\mathrm{V}_{\mathrm{b} 2}$ is changed. OUT1 and OUT2 change at the same rate when $-\mathrm{V}_{\mathrm{b}}$ is changed, as shown in Figure 16. Therefore, changing the voltage on $-\mathrm{V}_{\mathrm{b}}$ has no effect on differential output offset voltage.


Figure 14: Output vs. $+\mathrm{V}_{\mathrm{b} 1}$


Figure 15: Output vs. $+\mathrm{V}_{\mathrm{b} 2}$


Figure 16: Output vs. $-\mathrm{V}_{\mathrm{b}}$

## Adjusting Common Mode Output Offset Voltage

Short $+\mathrm{V}_{\mathrm{b} 1}$ to $+\mathrm{V}_{\mathrm{b} 2}$ and vary $+\mathrm{V}_{\mathrm{b}}$ and $-\mathrm{V}_{\mathrm{b}}$ to adjust common mode output offset voltage. The recommended values for achieving a given output offset are shown in Figure 17. These values were chosen to give the best distortion performance. The exact values are not crucial.


Figure 17: $\mathrm{V}_{\mathrm{b}}$ vs. Common Mode Voltage

For common mode voltages of 0 to -3.5 V swap the $\mathrm{V}_{\mathrm{b}}$ 's and change the polarity. See the example below.

| Desired Common <br> Mode Voltage | $+\mathbf{V}_{\mathbf{b} 1}$ and $+\mathrm{V}_{\mathbf{b} 2}(\mathrm{~V})$ | $-\mathrm{V}_{\mathbf{b}}(\mathrm{V})$ |
| :---: | :---: | :---: |
| 2 Volts | 2 | -8 |
| -2 Volts | 8 | -2 |



Figure 18: $2 \mathrm{~V}_{\mathrm{pp}} \mathrm{HD}$ vs. Common Mode Voltage


Figure 19: $\mathbf{5} \mathrm{V}_{\mathrm{pp}} \mathrm{HD}$ vs. Common Mode Voltage


Figure 20: Resulting $I_{s}$ and $-I_{s}$
Figures 18 and 19 illustrate how the common mode voltage effects harmonic distortion. Figure 20 show the resulting $\mathrm{I}_{\mathrm{s}}$ and $-\mathrm{I}_{\mathrm{s}}$ supply currents.

Pay close attention to your peak-to-peak output voltage requirement. As you change the common mode voltage, you may need to increase or shift $\pm \mathrm{V}_{\mathrm{s}}$ in order to achieve your output requirements. A 2 V margin is recommended. For example, if your output requirement is $5 \mathrm{~V}_{\mathrm{pp}}$ and you will be changing the common mode from 1 V to 3 V set $\mathrm{V}_{\mathrm{s}}=+7.5$ and $-\mathrm{V}_{\mathrm{s}}$ to -3.5 V . This example calls for a supply voltage of greater than 10 V . This will not effect supply current because as Figure 10 indicates, changing $\pm \mathrm{V}_{\mathrm{s}}$ has no effect on supply current.

## Layout Considerations

General layout and supply bypassing play major roles in high frequency performance. Fairchild has evaluation boards to use as a guide for high frequency layout and as aid in device testing and characterization. Follow the steps below as a basis for high frequency layout:

## ■ Include all recommended $6.8 \mu \mathrm{~F}$ and $0.01 \mu \mathrm{~F}$ bypass capacitors

■ Place the $6.8 \mu \mathrm{~F}$ capacitors within 0.75 inches of the power pin
■ Place the $0.01 \mathrm{\mu F}$ capacitors within 0.1 inches of the power pin

- Remove the ground plane under and around the part, especially near the input and output pins to reduce parasitic capacitance
- Minimize all trace lengths to reduce series inductances
- A 10 pF to 50 pF bypass capacitor can be used between pins 5 and 6 and between pins 10 and 11 to reduce crosstalk from the positive supply
Refer to the evaluation board layouts shown in Figure 21 for more information.


## Evaluation Board Information

The following evaluation boards are available to aid in the testing and layout of this device:

| Evaluation <br> Board | Description | Products |
| :---: | :--- | :--- |
| KEB007 | Basic KH600 Eval Bd | KH600 |
| KEB009 | KH600 Eval Bd with offset and <br> I CC Adjust Option | KH600 |

Do not include capacitors C2, C3, C7, C11, and C12 that are shown on the KEBOO7 evaluation board. Evaluation board schematics and layouts are shown in Figure 21. Refer to the schematic shown in Figure 1 for the KEB007 board and Figure 2 for the KEB009 board.

## KH600 Evaluation Board Layout



Figure 21a: KEB007 (top side)


Figure 21c: KEB009 (top side)


Figure 21b: KEB007 (bottom side)


Figure 21d: KEB009 (bottom side)

## KH600 Package Dimensions



| TO-8 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| SYMBOL | INCHES |  | MILIMETERS |  |
|  | Minimun | Maximum | Minimum | Maximum |
| A | 0.142 | 0.181 | 3.61 | 4.60 |
| ¢b | 0.016 | 0.019 | 0.41 | 0.48 |
| $\phi \mathrm{D}$ | 0.595 | 0.605 | 15.11 | 15.37 |
| $\phi \mathrm{D}_{1}$ | 0.543 | 0.555 | 13.79 | 14.10 |
| e | 0.400 BSC |  | 10.16 BSC |  |
| $\mathrm{e}_{1}$ | 0.200 BSC |  | 5.08 BSC |  |
| $\mathrm{e}_{2}$ | 0.100 BSC |  | 2.54 BSC |  |
| F | 0.016 | 0.030 | 0.41 | 0.76 |
| k | 0.026 | 0.036 | 0.66 | 0.91 |
| $\mathrm{k}_{1}$ | 0.026 | 0.036 | 0.66 | 0.91 |
| L | 0.310 | 0.340 | 7.87 | 8.64 |
| $\alpha$ | $45^{\circ} \mathrm{BSC}$ |  | $45^{\circ} \mathrm{BSC}$ |  |

notes:
Seal: cap weld
Lead finish: gold per MIL-M-38510
Package composition:
Package: metal
Lid: Type A per MIL-M-38510

## Ordering Information

| Part No. | Temperature | Package | Eval. Board |
| :---: | :---: | :---: | :---: |
| KH600AI | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 12 -pin TO8 | KEB007, KEB009 |

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