

## 1500 Watt MOSORB

### GENERAL DATA APPLICABLE TO ALL SERIES IN THIS GROUP

## Zener Transient Voltage Suppressors Unidirectional and Bidirectional

Mosorb devices are designed to protect voltage sensitive components from high voltage, high energy transients. They have excellent clamping capability, high surge capability, low zener impedance and fast response time. These devices are Motorola's exclusive, cost-effective, highly reliable Surmetic axial leaded package and are ideally-suited for use in communication systems, numerical controls, process controls, medical equipment, business machines, power supplies and many other industrial/consumer applications, to protect CMOS, MOS and Bipolar integrated circuits.

#### Specification Features:

- Standard Voltage Range — 6.2 to 250 V
- Peak Power — 1500 Watts @ 1 ms
- Maximum Clamp Voltage @ Peak Pulse Current
- Low Leakage < 5  $\mu$ A Above 10 V
- UL Recognition
- Response Time is Typically < 1 ns

#### Mechanical Characteristics:

**CASE:** Void-free, transfer-molded, thermosetting plastic

**FINISH:** All external surfaces are corrosion resistant and leads are readily solderable

**POLARITY:** Cathode indicated by polarity band. When operated in zener mode, will be positive with respect to anode

**MOUNTING POSITION:** Any

**WAFER FAB LOCATION:** Phoenix, Arizona

**ASSEMBLY/TEST LOCATION:** Guadalajara, Mexico

**1N6267A  
SERIES  
1500 WATT  
PEAK POWER**

**MOSORB  
ZENER OVERVOLTAGE  
TRANSIENT  
SUPPRESSORS  
6.2-250 VOLTS  
1500 WATT PEAK POWER  
5 WATTS STEADY STATE**



**CASE 41A  
PLASTIC**

#### MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Peak Power Dissipation (1) @ $T_L \leq 25^\circ\text{C}$	$P_{PK}$	1500	Watts
Steady State Power Dissipation @ $T_L \leq 75^\circ\text{C}$ , Lead Length = 3/8" Derated above $T_L = 75^\circ\text{C}$	$P_D$	5	Watts
		50	mW/ $^\circ\text{C}$
Forward Surge Current (2) @ $T_A = 25^\circ\text{C}$	$I_{FSM}$	200	Amps
Operating and Storage Temperature Range	$T_J, T_{stg}$	- 65 to +175	$^\circ\text{C}$

Lead temperature not less than 1/16" from the case for 10 seconds: 230 $^\circ\text{C}$

NOTES: 1. Nonrepetitive current pulse per Figure 5 and derated above  $T_A = 25^\circ\text{C}$  per Figure 2.

2. 1/2 sine wave (or equivalent square wave), PW = 8.3 ms, duty cycle = 4 pulses per minute maximum.

Devices listed in bold, italic are Motorola preferred devices.

**\*ELECTRICAL CHARACTERISTICS** ( $T_A = 25^\circ\text{C}$  unless otherwise noted)  $V_F\# = 3.5\text{ V Max}$ ,  $I_F^{**} = 100\text{ A}$

JEDEC Device	Device	Breakdown Voltage				Working Peak Reverse Voltage $V_{RWM}^{***}$ (Volts)	Maximum Reverse Leakage @ $V_{RWM}$ $I_R$ ( $\mu\text{A}$ )	Maximum Reverse Surge Current $I_{RSM}^\dagger$ (Amps)	Maximum Reverse Voltage @ $I_{RSM}$ (Clamping Voltage) $V_{RSM}$ (Volts)	Maximum Temperature Coefficient of $V_{BR}$ ( $\% / ^\circ\text{C}$ )
		$V_{BR}^{\dagger\dagger}$ Volts			@ $I_T$ (mA)					
		Min	Nom	Max						
<b>1N6267A</b>	1.5KE6.8A	<b>6.45</b>	<b>6.8</b>	<b>7.14</b>	<b>10</b>	<b>5.8</b>	<b>1000</b>	<b>143</b>	<b>10.5</b>	<b>0.057</b>
1N6268A	1.5KE7.5A	7.13	7.5	7.88	10	6.4	500	132	11.3	0.061
1N6269A	1.5KE8.2A	7.79	8.2	8.61	10	7.02	200	124	12.1	0.065
1N6270A	1.5KE9.1A	8.65	9.1	9.55	1	7.78	50	112	13.4	0.068
1N6271A	1.5KE10A	9.5	10	10.5	1	8.55	10	103	14.5	0.073
1N6272A	1.5KE11A	10.5	11	11.6	1	9.4	5	96	15.6	0.075
1N6273A	1.5KE12A	11.4	12	12.6	1	10.2	5	90	16.7	0.078
1N6274A	1.5KE13A	12.4	13	13.7	1	11.1	5	82	18.2	0.081
<b>1N6275A</b>	1.5KE15A	<b>14.3</b>	<b>15</b>	<b>15.8</b>	<b>1</b>	<b>12.8</b>	<b>5</b>	<b>71</b>	<b>21.2</b>	<b>0.084</b>
1N6276A	1.5KE16A	15.2	16	16.8	1	13.6	5	67	22.5	0.086
1N6277A	1.5KE18A	17.1	18	18.9	1	15.3	5	59.5	25.2	0.088
1N6278A	1.5KE20A	19	20	21	1	17.1	5	54	27.7	0.09
1N6279A	<b>1.5KE22A</b>	<b>20.9</b>	<b>22</b>	<b>23.1</b>	<b>1</b>	<b>18.8</b>	<b>5</b>	<b>49</b>	<b>30.6</b>	<b>0.092</b>
<b>1N6280A</b>	1.5KE24A	<b>22.8</b>	<b>24</b>	<b>25.2</b>	<b>1</b>	<b>20.5</b>	<b>5</b>	<b>45</b>	<b>33.2</b>	<b>0.094</b>
<b>1N6281A</b>	1.5KE27A	<b>25.7</b>	<b>27</b>	<b>28.4</b>	<b>1</b>	<b>23.1</b>	<b>5</b>	<b>40</b>	<b>37.5</b>	<b>0.096</b>
<b>1N6282A</b>	1.5KE30A	<b>28.5</b>	<b>30</b>	<b>31.5</b>	<b>1</b>	<b>25.6</b>	<b>5</b>	<b>36</b>	<b>41.4</b>	<b>0.097</b>
<b>1N6283A</b>	1.5KE33A	<b>31.4</b>	<b>33</b>	<b>34.7</b>	<b>1</b>	<b>28.2</b>	<b>5</b>	<b>33</b>	<b>45.7</b>	<b>0.098</b>
1N6284A	1.5KE36A	34.2	36	37.8	1	30.8	5	30	49.9	0.099
<b>1N6285A</b>	<b>1.5KE39A</b>	<b>37.1</b>	<b>39</b>	<b>41</b>	<b>1</b>	<b>33.3</b>	<b>5</b>	<b>28</b>	<b>53.9</b>	<b>0.1</b>
1N6286A	1.5KE43A	40.9	43	45.2	1	36.8	5	25.3	59.3	0.101
1N6287A	1.5KE47A	44.7	47	49.4	1	40.2	5	23.2	64.8	0.101
<b>1N6288A</b>	1.5KE51A	<b>48.5</b>	<b>51</b>	<b>53.6</b>	<b>1</b>	<b>43.6</b>	<b>5</b>	<b>21.4</b>	<b>70.1</b>	<b>0.102</b>
1N6289	<b>1.5KE56A</b>	<b>53.2</b>	<b>56</b>	<b>58.8</b>	<b>1</b>	<b>47.8</b>	<b>5</b>	<b>19.5</b>	<b>77</b>	<b>0.103</b>
1N6290A	1.5KE62A	58.9	62	65.1	1	53	5	17.7	85	0.104
1N6291A	1.5KE68A	64.6	68	71.4	1	58.1	5	16.3	92	0.104
1N6292A	1.5KE75A	71.3	75	78.8	1	64.1	5	14.6	103	0.105
1N6293A	1.5KE82A	77.9	82	86.1	1	70.1	5	13.3	113	0.105
1N6294A	1.5KE91A	86.5	91	95.5	1	77.8	5	12	125	0.106
1N6295A	1.5KE100A	95	100	105	1	85.5	5	11	137	0.106
1N6296A	1.5KE110A	105	110	116	1	94	5	9.9	152	0.107
1N6297A	1.5KE120A	114	120	126	1	102	5	9.1	165	0.107
1N6298A	1.5KE130A	124	130	137	1	111	5	8.4	179	0.107
1N6299A	1.5KE150A	143	150	158	1	128	5	7.2	207	0.108
1N6300A	1.5KE160A	152	160	168	1	136	5	6.8	219	0.108
1N6301A	1.5KE170A	162	170	179	1	145	5	6.4	234	0.108
1N6302A	1.5KE180A	171	180	189	1	154	5	6.1	246	0.108
1N6303A	1.5KE200A	190	200	210	1	171	5	5.5	274	0.108
	1.5KE220A	209	220	231	1	185	5	4.6	328	0.109
	1.5KE250A	237	250	263	1	214	5	5	344	0.109

\* Indicates JEDEC registered data.

\*\* 1/2 sine wave (or equivalent square wave), PW = 8.3 ms, duty cycle = 4 pulses per minute maximum.

\*\*\* A transient suppressor is normally selected according to the maximum reverse stand-off voltage ( $V_{RWM}$ ), which should be equal to or greater than the dc or continuous peak operating voltage level.

† Surge current waveform per Figure 5 and derate per Figure 2 of the General Data — 1500 W at the beginning of this group.

††  $V_{BR}$  measured at pulse test current  $I_T$  at an ambient temperature of  $25^\circ\text{C}$ .

#  $V_F$  applies to Non-CA suffix devices only.

**FOR BIDIRECTIONAL APPLICATIONS**

— USE CA SUFFIX ON 1.5KE SERIES for 1.5KE6.8CA through 1.5KE250CA.

Electrical characteristics apply in both directions.

**Preferred Bidirectional Devices —**

1.5KE10CA 1.5KE12CA  
1.5KE18CA 1.5KE36CA

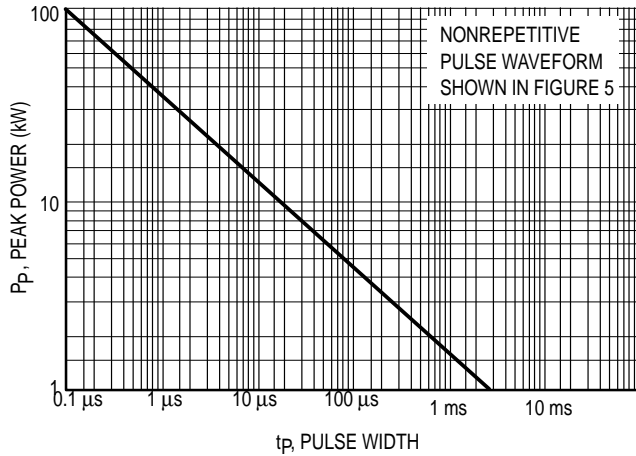


Figure 1. Pulse Rating Curve

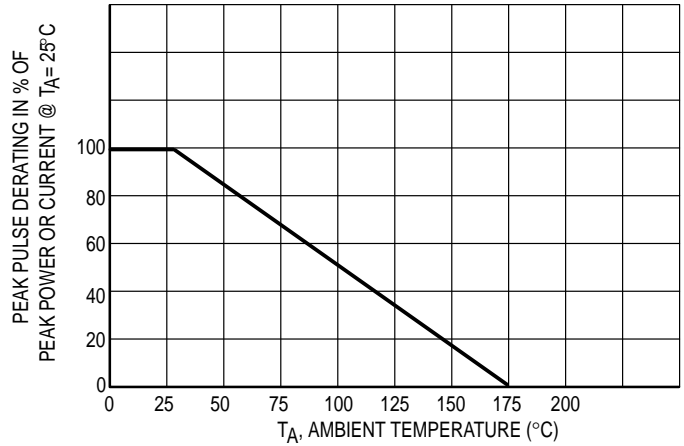
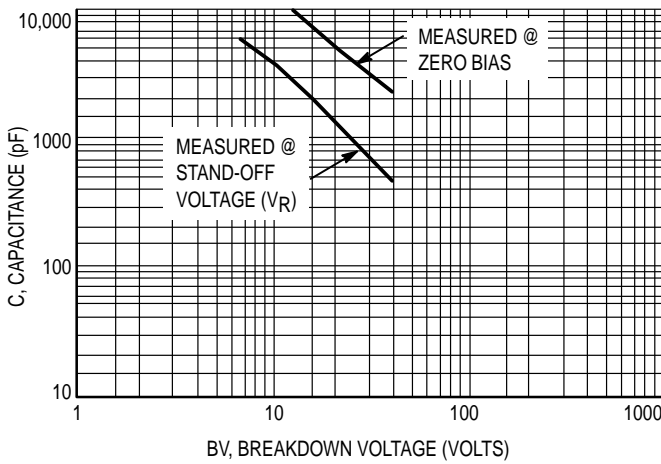


Figure 2. Pulse Derating Curve

**1N6373, ICTE-5, MPTE-5,**  
through  
**1N6389, ICTE-45, C, MPTE-45, C**



**1N6267A/1.5KE6.8A**  
through  
**1N6303A/1.5KE200A**

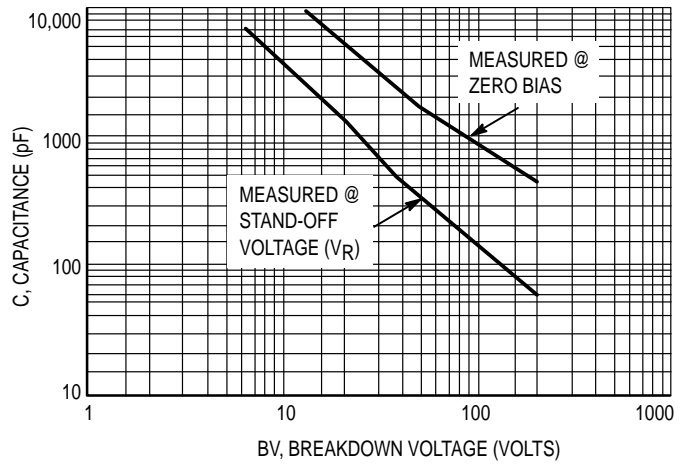


Figure 3. Capacitance versus Breakdown Voltage

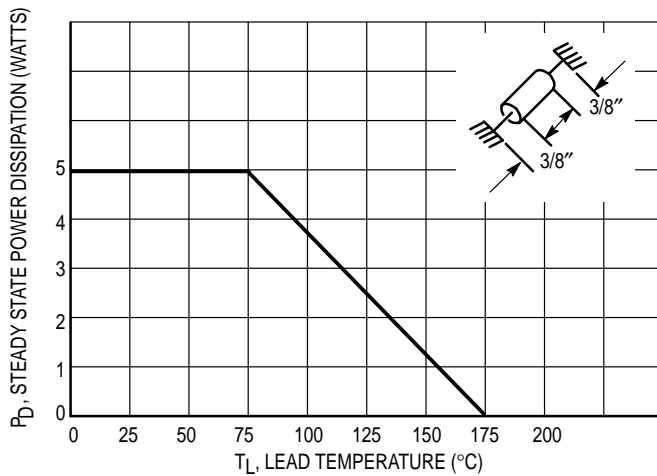


Figure 4. Steady State Power Derating

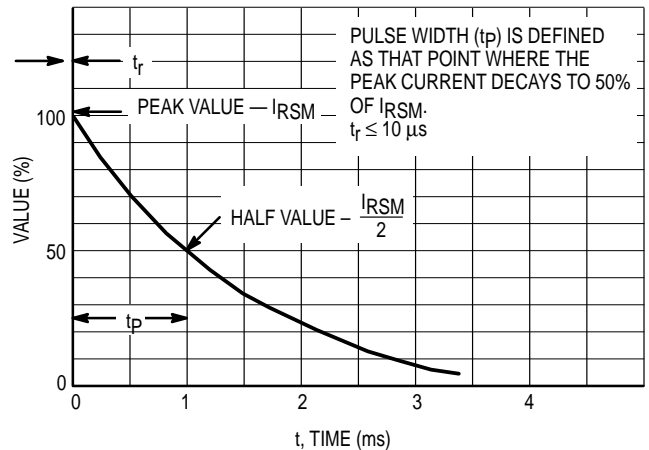
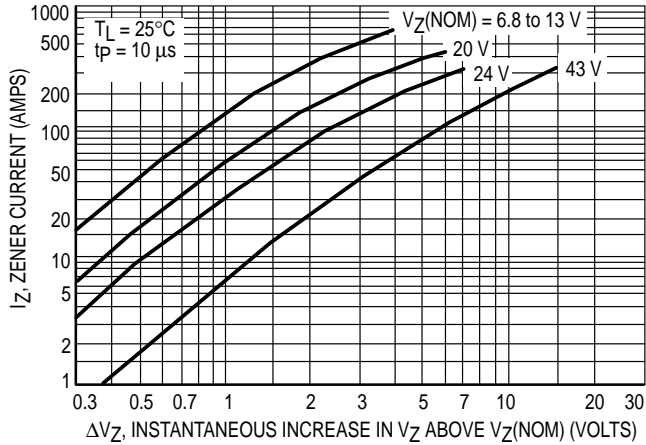


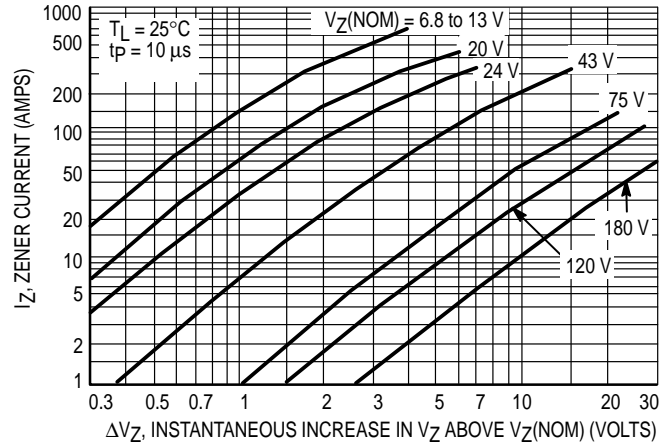
Figure 5. Pulse Waveform

Devices listed in bold, italic are Motorola preferred devices.

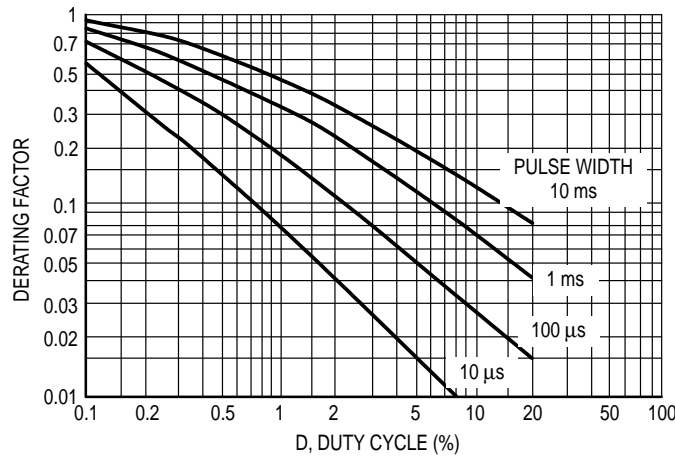
**1N6373, ICTE-5, MPTE-5,  
through  
1N6389, ICTE-45, C, MPTE-45, C**



**1N6267A/1.5KE6.8A  
through  
1N6303A/1.5KE200A**



**Figure 6. Dynamic Impedance**



**Figure 7. Typical Derating Factor for Duty Cycle**

**APPLICATION NOTES**

**RESPONSE TIME**

In most applications, the transient suppressor device is placed in parallel with the equipment or component to be protected. In this situation, there is a time delay associated with the capacitance of the device and an overshoot condition associated with the inductance of the device and the inductance of the connection method. The capacitance effect is of minor importance in the parallel protection scheme because it only produces a time delay in the transition from the operating voltage to the clamp voltage as shown in Figure A.

The inductive effects in the device are due to actual turn-on time (time required for the device to go from zero current to full current) and lead inductance. This inductive effect produces an overshoot in the voltage across the equipment or component being protected as shown in Figure B. Minimizing this overshoot is very important in the application, since the main purpose for adding a transient suppressor is to clamp voltage spikes. These devices have excellent response time, typically in the picosecond range and negligible inductance. However, external inductive effects could produce unacceptable overshoot. Proper circuit layout, minimum lead lengths

and placing the suppressor device as close as possible to the equipment or components to be protected will minimize this overshoot.

Some input impedance represented by  $Z_{in}$  is essential to prevent overstress of the protection device. This impedance should be as high as possible, without restricting the circuit operation.

**DUTY CYCLE DERATING**

The data of Figure 1 applies for non-repetitive conditions and at a lead temperature of 25°C. If the duty cycle increases, the peak power must be reduced as indicated by the curves of Figure 7. Average power must be derated as the lead or ambient temperature rises above 25°C. The average power derating curve normally given on data sheets may be normalized and used for this purpose.

At first glance the derating curves of Figure 7 appear to be in error as the 10 ms pulse has a higher derating factor than the 10 μs pulse. However, when the derating factor for a given pulse of Figure 7 is multiplied by the peak power value of Figure 1 for the same pulse, the results follow the expected trend.

## TYPICAL PROTECTION CIRCUIT

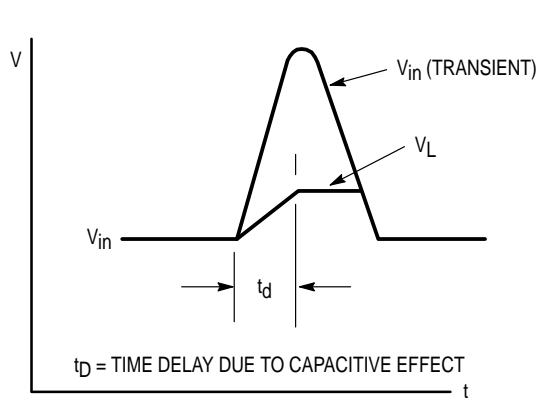
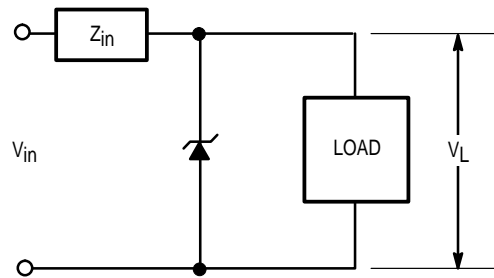


Figure 8.

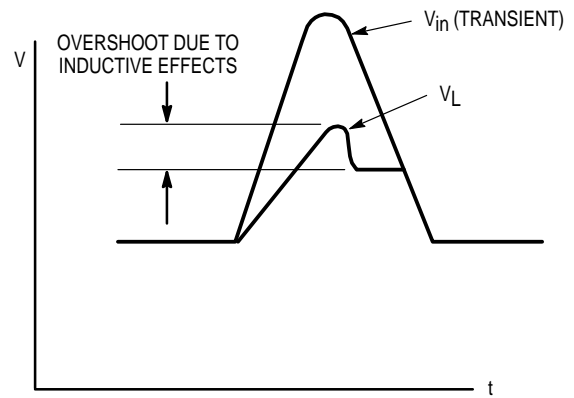


Figure 9.

## UL RECOGNITION\*

The entire series has *Underwriters Laboratory Recognition* for the classification of protectors (QVGV2) under the UL standard for safety 497B and File #116110. Many competitors only have one or two devices recognized or have recognition in a non-protective category. Some competitors have no recognition at all. With the UL497B recognition, our parts successfully passed several tests including Strike Voltage Breakdown test, Endurance Conditioning, Temperature test,

Dielectric Voltage-Withstand test, Discharge test and several more.

Whereas, some competitors have only passed a flammability test for the package material, we have been recognized for much more to be included in their Protector category.

\*Applies to 1.5KE6.8A, CA thru 1.5KE250A, CA

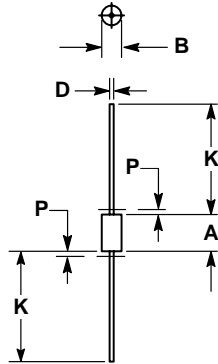
## CLIPPER BIDIRECTIONAL DEVICES

1. Clipper-bidirectional devices are available in the 1.5KEXXA series and are designated with a "CA" suffix; for example, 1.5KE18CA. Contact your nearest Motorola representative.
2. Clipper-bidirectional part numbers are tested in both directions to electrical parameters in preceding table (except for  $V_F$  which does not apply).
3. The 1N6267A through 1N6303A series are JEDEC registered devices and the registration does not include a "CA" suffix. To order clipper-bidirectional devices one must add CA to the 1.5KE device title.

Devices listed in bold, italic are Motorola preferred devices.

# Transient Voltage Suppressors — Axial Leaded

## 1500 Watt Peak Power



- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
  2. CONTROLLING DIMENSION: INCH.
  3. LEAD FINISH AND DIAMETER UNCONTROLLED IN DIM P.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.360	0.375	9.14	9.52
B	0.190	0.205	4.83	5.21
D	0.038	0.042	0.97	1.07
K	1.000	—	25.40	—
P	—	0.050	—	1.27

**CASE 41A-02  
PLASTIC**

(Refer to Section 10 for Surface Mount, Thermal Data and Footprint Information.)

### MULTIPLE PACKAGE QUANTITY (MPQ) REQUIREMENTS

Package Option	Type No. Suffix	MPQ (Units)
Tape and Reel	RL4	1.5K

(Refer to Section 10 for more information on Packaging Specifications.)