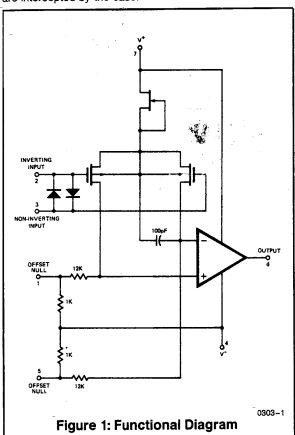
ICH8500/A Ultra Low Input-Bias Operational Amplifier

GENERAL DESCRIPTION

The ICH8500 and ICH8500A are hybrid circuits designed for ultra low input bias current operational amplifier applications. They are ideally suited for analog and electrometer applications where high input resistance and low input current are of prime importance.

Functionally, they are pin for pin identical to the popular 741 monolithic amplifier. These amplifiers are unconditionally stable and the input offset voltage can be adjusted to zero with an external $20k\Omega$ potentiometer. The input bias current for the inverting and noninverting inputs is 0.1pA maximum for the ICH8500, and 0.01pA maximum for the ICH8500A.

Pin 8 is connected to the case. This permits the designer to operate the case at any desired potential. This is the key to achieving the ultra low input currents associated with these two amplifiers. Forcing the case to the same potential as the inputs eliminates current flow between the case and the input pins, and leakage currents that may have otherwise existed between any of the other pins and the inputs are intercepted by the case.





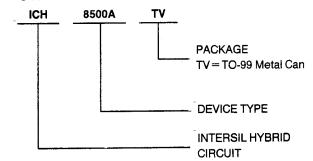
FEATURES

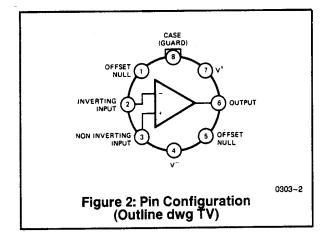
- Input Diode Protection
- Input Bias Current Less Than 0.01pA (8500A)
- No Frequency Compensation Required
- Offset Voltage Null Capability
- Short Circuit Protection
- Low Power Consumption

APPLICATIONS

- Femto Ammeter
- Electrometers
- Long Time Integrators
- Flame Detectors
- pH Meters
- Proximity Detector
- Sample and Hold Circuits

ORDERING INFORMATION





ABSOLUTE MAXIMUM RATINGS

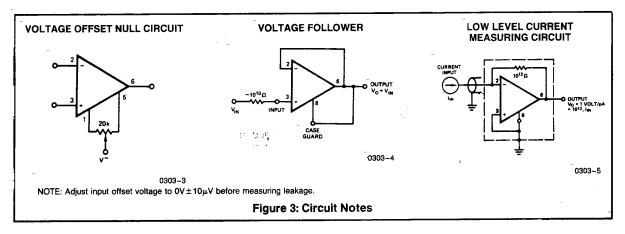
± 18V
500mW
± 0.5V
-65°C to +150°C
25°C to +85°C
300°C
Indefinite

NOTE: Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other conditions above those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Note: 1. Rating applies for ambient temperature to +70°C

ELECTRICAL CHARACTERISTICS (T_A = 25°C unless otherwise specified, V_{SUPPLY} = ±15V)

-	Characteristics Test Conditions	ICH8500			ICH8500A			Units	
Symbol		Conditions	Conditions	Min	Тұр	Max	Min	Тур	Max
I _{BIAS}	Input Bias Current (Inverting and Non-Inverting)	Case at same potential as inputs			±0.1			±0.01	pА
Vos	Input Offset Voltage	·			±75			±50	m∨
Sheet411 co	Offset Voltage Adjustment Range	20k Ω Potentiometer		±50			±50		_mV
ΔV _{OS} /ΔΤ	Change in Input Offset Voltage Over Temperature	+ 25 to + 85°C - 25 to + 25°C	•	± 200			± 100		¯mV
ΔV _{OS} /Δt	Long Term Input Offset Voltage Stability	At 25°C		±3.0	-	-	±3.0		m∨
CMRR	Common Mode Rejection Ratio	±5 volts common mode voltage		75			75		dB
ΔVO	Output Voltage Swing	R _L ≥10kΩ	±11			±11			<u> </u>
CMVR	Common Mode Voltage Range		±10			±10			V
Avol	Large Signal Voltage Gain		20,000	10 ⁵		20,000	10 ⁵		
C _{fb}	Feedback Capacitance	Case guarded		0.1			0.1		pF
SR	Slew Rate	R _L ≥2kΩ		0.5			0.5		V/µs
C _{IN}	Input Capacitance	Case guarded		0.7			0.7		pF
C _{IN}	Input Capacitance	Case grounded		1.5			1.5		pF



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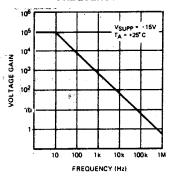
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NOTE: All typical values have been characterized but are not tested.

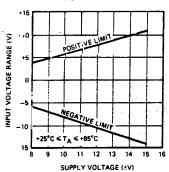
TYPICAL PERFORMANCE CHARACTERISTICS

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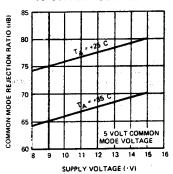
OPEN LOOP VOLTAGE GAIN vs. **FREQUENCY**



INPUT VOLTAGE RANGE vs. SUPPLY **VOLTAGE**



COMMON MODE REJECTION RATIO vs. SUPPLY VOLTAGE



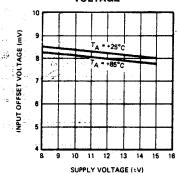
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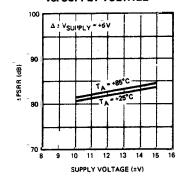
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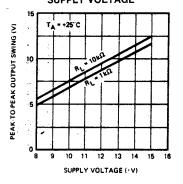
INPUT OFFSET VOLTAGE vs. SUPPLY **VOLTAGE**



± POWER SUPPLY REJECTION RATIO vs. SUPPLY VOLTAGE

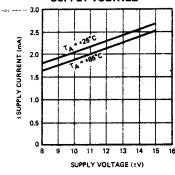


OUTPUT VOLTAGE SWING vs. SUPPLY VOLTAGE

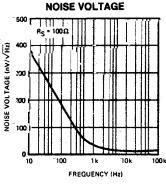


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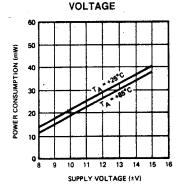
± QUIESCENT SUPPLY CURRENT vs. SUPPLY VOLTAGE



INPUT REFERRED



POWER CONSUMPTION vs. SUPPLY



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ICH8500/A



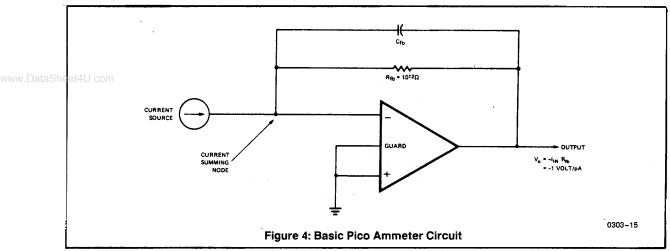
APPLICATIONS The Pico Ammeter

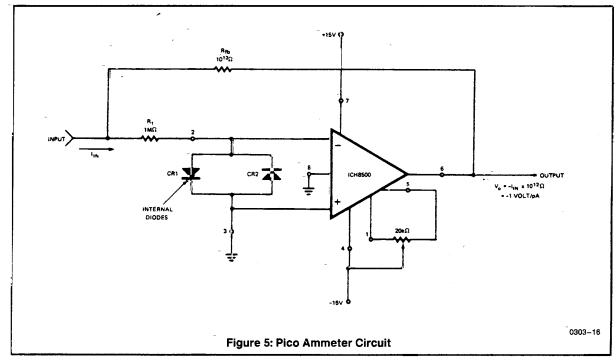
A very sensitive pico ammeter can be constructed with the ICH8500. The basic circuit (illustrated in Figure 4) employs the amplifier in the inverting or current summing

mode.

Care must be taken to eliminate any stray currents from flowing into the current summing node. This can be accomplished by forcing all points surrounding the input to the same potential as the input. In this case the potential of the input is at virtual ground, or 0V. Therefore, the case of the device is grounded to intercept any stray leakage currents

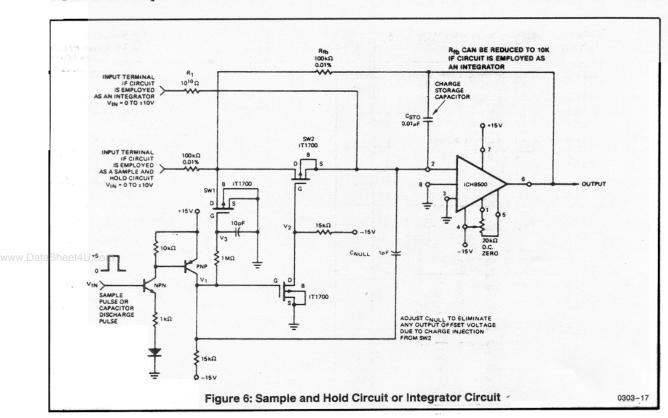
that may otherwise exist between the \pm 15V input terminals and the inverting input summing junctions. Feedback capacitance* should be kept to a minimum in order to maximize the response time of the circuit to step function input currents. The time constant of the circuit is approximately the product of the feedback capacitance C_{fb} times the feedback resistor R_{fb} . For instance, the time constant of the circuit in Figure 4 is 1 sec if C_{fb} =1pF. Thus, it takes approximately 5 sec (5 time constants) for the circuit to stabilize to within 1% of its final output voltage after a step function of input current has been applied. C_{fb} of less than 0.2 to 0.3pF can be achieved with proper circuit layout. A practical pico ammeter circuit is illustrated in Figure 5.





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The internal diodes CR1 and CR2 together with external resistor R1 protect the input stage of the amplifier from voltage transients. The two diodes contribute no error currents, since under normal operating conditions there is no voltage across them.

*Feedback capacitance is the capacitance between the output and the inverting input terminal of the amplifier.

Sample and Hold Circuit

The basic principle of this circuit (Figure 6) is to rapidly charge a capacitor CSTO to a voltage equal to an input signal. The input signal is then electrically disconnected from the capacitor with the charge still remaining on CSTO. Since CSTO is in the negative feedback loop of the operational amplifier, the output voltage of the amplifier is equal to the voltage across the capacitor. Ideally, the voltage across CSTO should remain constant, causing the output of the amplifier to remain constant as well. However, the voltage across CSTO will decay at a rate proportional to the current being injected or taken out of the current summing node of the amplifier. This current can come from four sources: leakage resistance of CSTO, leakage current due to the solid state switch SW2, currents due to high resistance paths on the circuit fixture, and most important, bias current of the operational amplifier. If the ICH8500A operational amplifier is employed, this bias current is almost non-existant (<0.01pA). Note that the voltages on the source, drain and

gate of switch SW2 are zero or near zero when the circuit is in the hold mode. Careful construction will eliminate stray resistance paths and capacitor resistance can be eliminated if a quality capacitor is selected. The net result is a low drift sample and hold circuit.

As an example, suppose the leakage current due to all sources flowing into the current summing node of the sample and hold circuit is 100pA. The rate of change of the voltage across the $0.01\mu F$ storage capacitor is then 10mV/ sec. In contrast, if an operational amplifier which exhibited an input bias current of 1nA were employed, the rate of change of the voltage across C_{STO} would be 0.1V/sec. An error build up such as this could not be tolerated in most applications.

Waveforms illustrating the operation of the sample and hold circuit are shown in Figure 7.

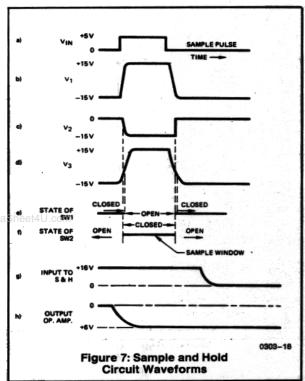
The Gated Integrator

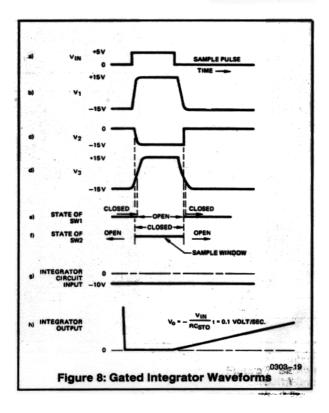
The circuit in Figure 6 can double as an integrator. In this application the input voltage is applied to the integrator input terminal. The time constant of the circuit is the product of R1 and C_{STO} . Because of the low leakage current associated with the ICH8500 and ICH8500A, very large values of R1 (Up to 10^{12} ohms) can be employed. This permits the use of small values of integrating capacitor (C_{STO}) in applications that require long time delays. Waveforms for the integrator circuit are illustrated in Figure 8.

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