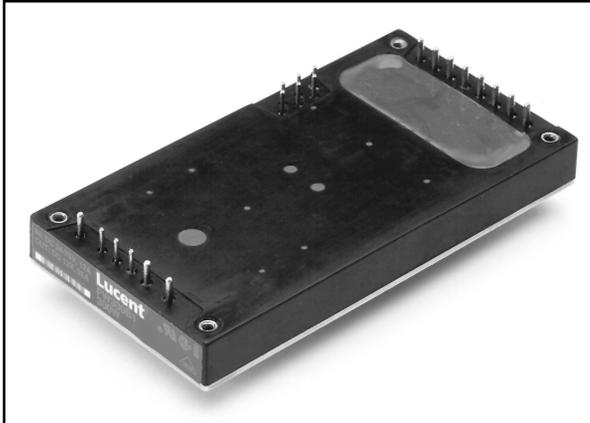




## FC250F1 Power Module: dc-dc Converter; 18 Vdc to 36 Vdc Input, 3.3 Vdc Output; 165 W



The FC250F1 Power Module uses advanced, surface-mount technology and delivers high-quality, compact, dc-dc conversion at an economical price.

### Applications

- Redundant and distributed power architectures
- Computer equipment
- Communications equipment

### Options

- Heat sinks available for extended operation

### Description

The FC250F1 Power Module is a dc-dc converter that operates over an input voltage range of 18 Vdc to 36 Vdc and provides a precisely regulated dc output. The outputs are fully isolated from the inputs, allowing versatile polarity configurations and grounding connections. The module has a maximum power rating of 165 W at a typical full-load efficiency of 78%.

Two or more modules may be paralleled with forced load sharing for redundant or enhanced power applications. The package, which mounts on a printed-circuit board, accommodates a heat sink for high-temperature applications.

### Features

- Size: 61.0 mm x 116.8 mm x 13.5 mm (2.40 in. x 4.60 in. x 0.53 in.)
- Wide input voltage range
- High efficiency: 78% typical
- Parallel operation with load sharing
- Adjustable output voltage
- Overtemperature protection
- Output voltage set-point adjustment (trim)
- Synchronization
- Power good signal
- Output current monitor
- Output overvoltage and overcurrent protection
- Remote sense
- Remote on/off
- Constant frequency
- Case ground pin
- Input-to-output isolation
- ISO\* 9001 Certified manufacturing facilities
- UL†1950 Recognized, CSA‡ C22.2 No. 950-95 Certified, and VDE§ 0805 (EN60950, IEC950) Licensed

\* ISO is a registered trademark of the International Organization of Standardization.

† UL is a registered trademark of Underwriters Laboratories, Inc.

‡ CSA is a registered trademark of Canadian Standards Association.

§ VDE is a trademark of Verband Deutscher Elektrotechniker e.V.

## Absolute Maximum Ratings

Stresses in excess of the absolute maximum ratings can cause permanent damage to the device. These are absolute stress ratings only. Functional operation of the device is not implied at these or any other conditions in excess of those given in the operations sections of the data sheet. Exposure to absolute maximum ratings for extended periods can adversely affect device reliability.

Parameter	Symbol	Min	Max	Unit
Input Voltage (continuous)	$V_I$	—	50	Vdc
I/O Isolation Voltage (for 1 minute)	—	—	1500	Vdc
Operating Case Temperature (See Thermal Considerations section and Figure 18.)	$T_C$	-40	100	°C
Storage Temperature	$T_{stg}$	-55	125	°C

## Electrical Specifications

Unless otherwise indicated, specifications apply over all operating input voltage, resistive load, and temperature conditions.

**Table 1. Input Specifications**

Parameter	Symbol	Min	Typ	Max	Unit
Operating Input Voltage	$V_I$	18	28	36	Vdc
Maximum Input Current ( $V_I = 0$ V to 36 V)	$I_{I, max}$	—	—	15	A
Inrush Transient	$i^2t$	—	—	4.0	A <sup>2</sup> s
Input Reflected-ripple Current, Peak-to-peak (5 Hz to 20 MHz, 12 $\mu$ H source impedance; see Figure 8.)	$I_I$	—	10	—	mAp-p
Input Ripple Rejection (120 Hz)	—	—	60	—	dB

## Fusing Considerations

**CAUTION: This power module is not internally fused. An input line fuse must always be used.**

This encapsulated power module can be used in a wide variety of applications, ranging from simple stand-alone operation to an integrated part of a sophisticated power architecture. To preserve maximum flexibility, internal fusing is not included; however, to achieve maximum safety and system protection, always use an input line fuse. The safety agencies require a normal-blow fuse with a maximum rating of 25 A (see Safety Considerations section). Based on the information provided in this data sheet on inrush energy and maximum dc input current, the same type of fuse with a lower rating can be used. Refer to the fuse manufacturer's data for further information.

## Electrical Specifications (continued)

Table 2. Output Specifications

Parameter	Symbol	Min	Typ	Max	Unit
Output Voltage Set Point ( $V_i = 28\text{ V}$ ; $I_o = I_{o, \text{max}}$ ; $T_c = 25\text{ }^\circ\text{C}$ )	$V_{O, \text{set}}$	3.25	3.3	3.35	Vdc
Output Voltage (Over all operating input voltage, resistive load, and temperature conditions until end of life; see Figure 10 and Feature Descriptions.)	$V_o$	3.20	—	3.40	Vdc
Output Regulation: Line ( $V_i = 18\text{ V}$ to $36\text{ V}$ ) Load ( $I_o = I_{o, \text{min}}$ to $I_{o, \text{max}}$ ) Temperature ( $T_c = -40\text{ }^\circ\text{C}$ to $+100\text{ }^\circ\text{C}$ )	— — —	— — —	0.01 0.05 15	0.1 0.2 50	% $V_o$ % $V_o$ mV
Output Ripple and Noise Voltage (See Figures 4 and 9.): RMS Peak-to-peak (5 Hz to 20 MHz)	— —	— —	— —	40 150	mVrms mVp-p
External Load Capacitance	—	0	—	*	$\mu\text{F}$
Output Current (At $I_o < I_{o, \text{min}}$ , the modules may exceed output ripple specifications.)	$I_o$	0.5	—	50	A
Output Current-limit Inception ( $V_o = 90\%$ of $V_{O, \text{set}}$ ; see Feature Descriptions.)	$I_{o, \text{cli}}$	51.5	57.5	65 <sup>†</sup>	% $I_{o, \text{max}}$
Output Short-circuit Current ( $V_o = 1.0\text{ V}$ ; indefinite duration, no hiccup mode; see Figure 2.)	—	—	—	150	% $I_{o, \text{max}}$
Efficiency ( $V_i = 28\text{ V}$ ; $I_o = I_{o, \text{max}}$ ; $T_c = 25\text{ }^\circ\text{C}$ ; see Figures 3 and 10.)	$\eta$	—	78	—	%
Switching Frequency	—	—	500	—	kHz
Dynamic Response ( $\Delta I_o/\Delta t = 1\text{ A}/10\text{ }\mu\text{s}$ , $V_i = 28\text{ V}$ , $T_c = 25\text{ }^\circ\text{C}$ ; tested with a $10\text{ }\mu\text{F}$ aluminum and a $1.0\text{ }\mu\text{F}$ ceramic capacitor across the load; see Figures 5 and 6.): Load Change from $I_o = 50\%$ to $75\%$ of $I_{o, \text{max}}$ : Peak Deviation Settling Time ( $V_o < 10\%$ of peak deviation) Load Change from $I_o = 50\%$ to $25\%$ of $I_{o, \text{max}}$ : Peak Deviation Settling Time ( $V_o < 10\%$ of peak deviation)	— — — —	— — — —	50 200 50 200	— — — —	mV $\mu\text{s}$ mV $\mu\text{s}$

\* Consult your sales representative or the factory.

† These are manufacturing test limits. In some situations, results may differ.



## Feature Specifications (continued)

Table 4. Feature Specifications (continued)

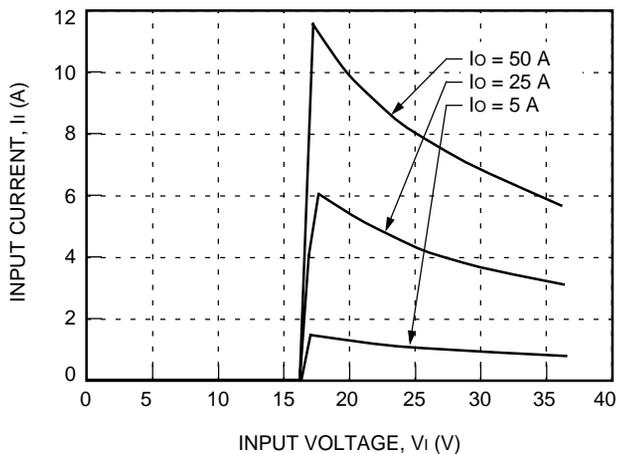
Parameter	Symbol	Min	Typ	Max	Unit
Overtemperature Protection (See Figure 18.)	$T_C$	—	105	—	°C
Forced Load Share Accuracy	—	—	10	—	% $I_{O, rated}$
Power Good Signal Interface (See Feature Descriptions.):					
Low Impedance—Module Operating	$R_{pwr/good}$	—	—	100	$\Omega$
	$I_{pwr/good}$	—	—	1	mA
High Impedance—Module Off	$R_{pwr/good}$	1	—	—	M $\Omega$
	$V_{pwr/good}$	—	—	40	V

## Solder, Cleaning, and Drying Considerations

Post solder cleaning is usually the final circuit-board assembly process prior to electrical testing. The result of inadequate circuit-board cleaning and drying can affect both the reliability of a power module and the testability of the finished circuit-board assembly. For guidance on appropriate soldering, cleaning, and drying procedures, refer to Lucent Technologies *Board-Mounted Power Modules Soldering and Cleaning* Application Note (AP97-021EPS).

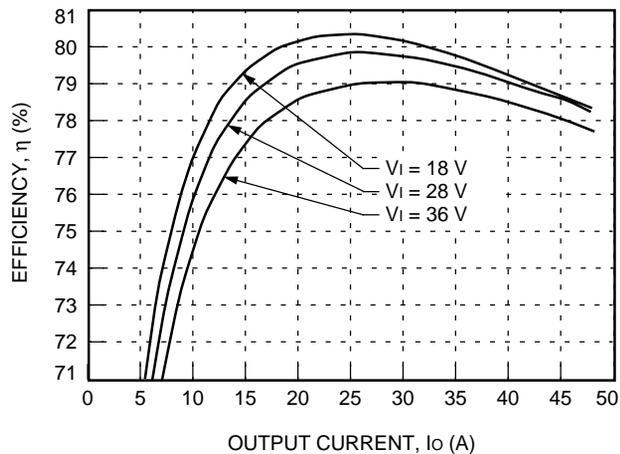
## Characteristic Curves

The following figures provide typical characteristics for the power module.



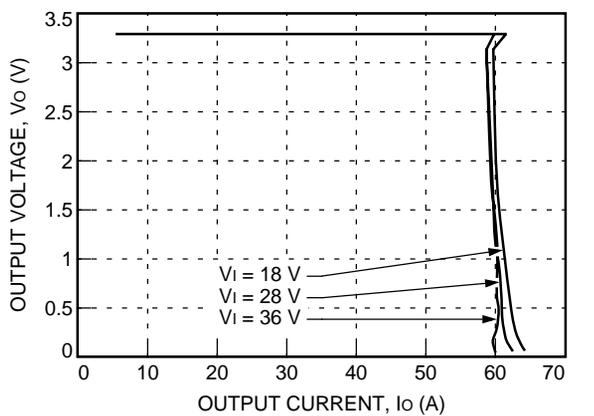
8-2875 (F)

**Figure 1. Typical FC250F1 Input Characteristics at Room Temperature**



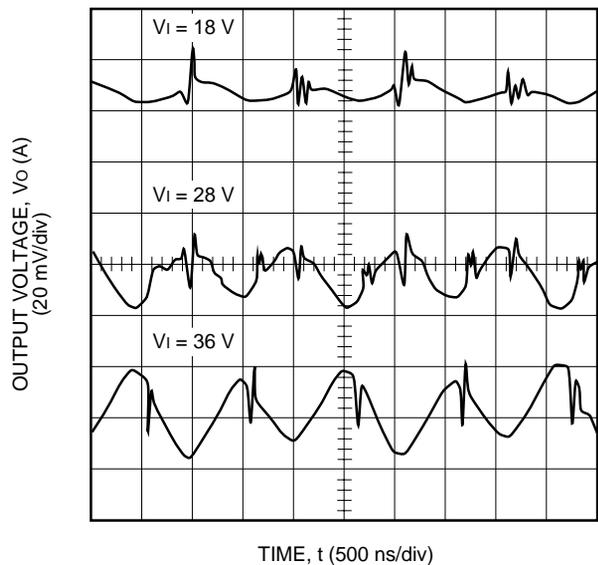
8-2876 (F)

**Figure 3. Typical FC250F1 Efficiency vs. Output Current at Room Temperature**



8-3277 (F)

**Figure 2. Typical FC250F1 Output Characteristics at Room Temperature**

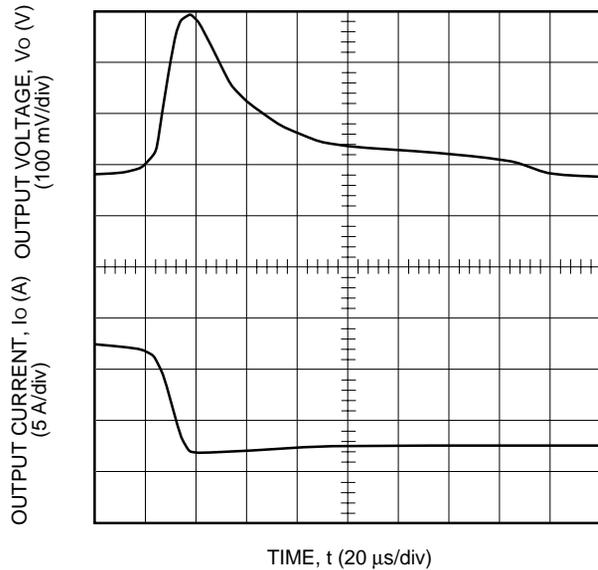


8-2877 (F)

Note: See Figure 9 for test conditions.

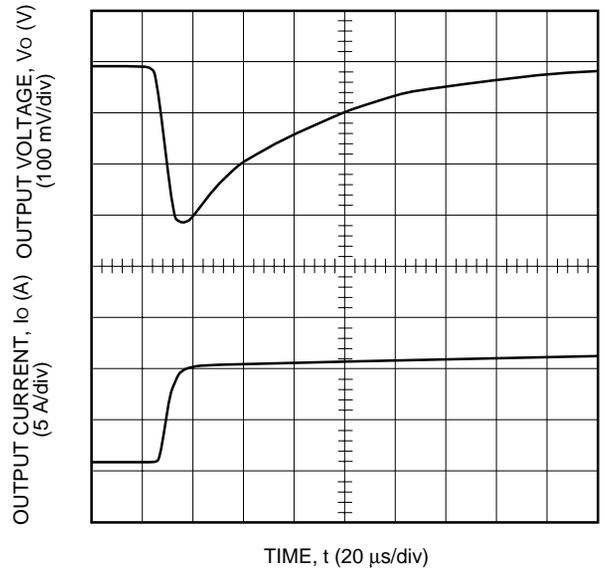
**Figure 4. Typical FC250F1 Output Ripple Voltage at Room Temperature and 50 A Output**

Characteristic Curves (continued)



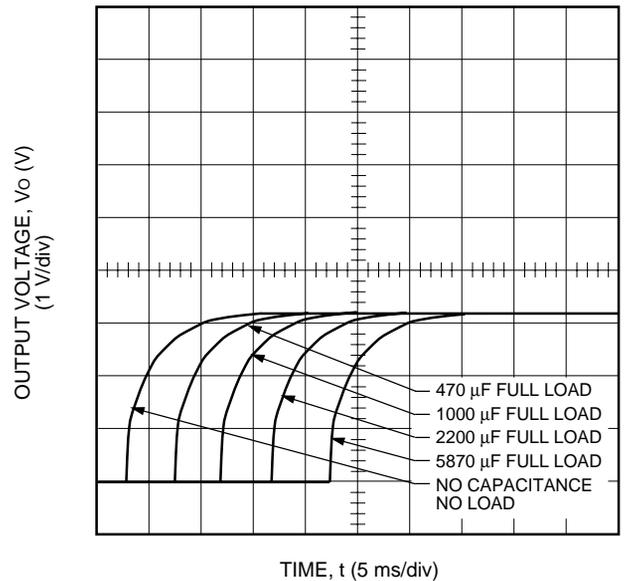
Note: Tested with a 10  $\mu$ F aluminum and a 1.0  $\mu$ F ceramic capacitor across the load. 8-2881 (F)

**Figure 5. Typical FC250F1 Transient Response to Step Decrease in Load from 50% to 25% of Full Load at Room Temperature and 28 V Input (Waveform Averaged to Eliminate Ripple Component.)**



Note: Tested with a 10  $\mu$ F aluminum and a 1.0  $\mu$ F ceramic capacitor across the load. 8-2878 (F)

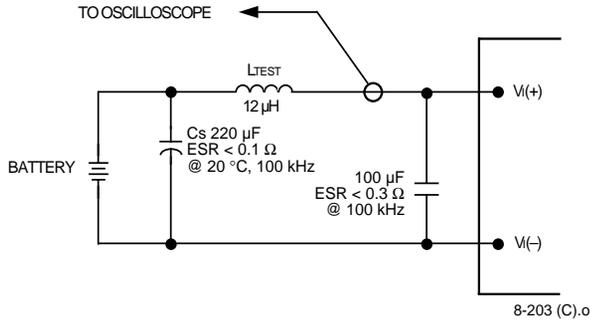
**Figure 6. Typical FC250F1 Transient Response to Step Increase in Load from 50% to 75% of Full Load at Room Temperature and 28 V Input (Waveform Averaged to Eliminate Ripple Component.)**



Note: Tested with a 10  $\mu$ F aluminum and a 1.0  $\mu$ F ceramic capacitor across the load. 8-2882 (F)

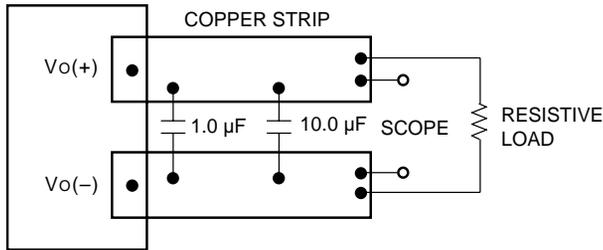
**Figure 7. Typical FC250F1 Start-Up Transient at Room Temperature, 28 V Input, and Full Load**

**Test Configurations**



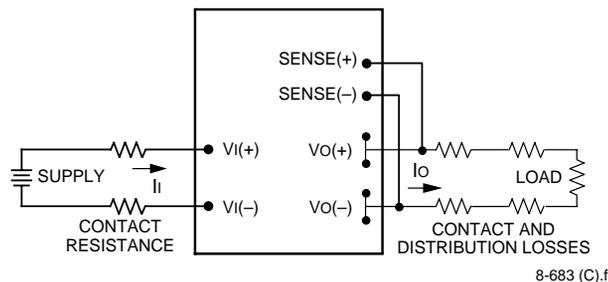
Note: Measure input reflected-ripple current with a simulated source inductance (L<sub>TEST</sub>) of 12 μH. Capacitor Cs offsets possible battery impedance. Measure current as shown above.

**Figure 8. Input Reflected-Ripple Test Setup**



Note: Use a 0.1 μF ceramic capacitor and a 10 μF aluminum or tantalum capacitor. Scope measurement should be made using a BNC socket. Position the load between 50 mm and 76 mm (2 in. and 3 in.) from the module.

**Figure 9. Peak-to-Peak Output Noise Measurement Test Setup**



Note: All measurements are taken at the module terminals. When socketing, place Kelvin connections at module terminals to avoid measurement errors due to socket contact resistance.

$$\eta = \left( \frac{[V_{O(+)} - V_{O(-)}]I_o}{[V_{I(+)} - V_{I(-)}]I_i} \right) \times 100 \quad \%$$

**Figure 10. Output Voltage and Efficiency Measurement Test Setup**

**Design Considerations**

**Input Source Impedance**

The power module should be connected to a low ac-impedance input source. Highly inductive source impedances can affect the stability of the power module. For the test configuration in Figure 8, a 100 μF electrolytic capacitor (ESR < 0.3 Ω at 100 kHz) mounted close to the power module helps ensure stability of the unit. For other highly inductive source impedances, consult the factory for further application guidelines.

**Safety Considerations**

For safety-agency approval of the system in which the power module is used, the power module must be installed in compliance with the spacing and separation requirements of the end-use safety agency standard, i.e., UL-1950, CSA 22.2 No. 95-950, and VDE 0805 (EN60950, IEC950).

For the converter output to be considered meeting the requirements of safety extra-low voltage (SELV), the input must meet SELV requirements.

If the input meets extra-low voltage (ELV) requirements, then the converter's output is considered ELV.

The input to these units is to be provided with a maximum 25 A normal-blow fuse in the ungrounded lead.

**Feature Descriptions**

**Overcurrent Protection**

To provide protection in a fault (output overload) condition, the unit is equipped with internal current-limiting circuitry and can endure current limiting for an unlimited duration. At the point of current-limit inception, the unit shifts from voltage control to current control. If the output voltage is pulled very low during a severe fault, the current-limit circuit can exhibit either foldback or tailout characteristics (output-current decrease or increase). The unit operates normally once the output current is brought back into its specified range.

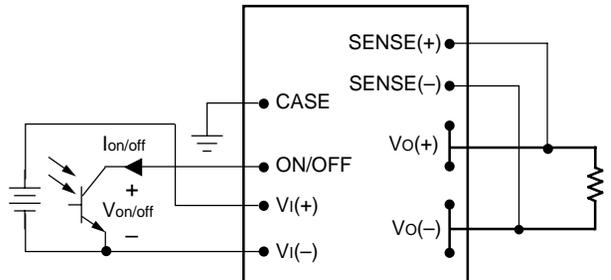
## Feature Descriptions (continued)

### Remote On/Off

To turn the power module on and off, the user must supply a switch to control the voltage between the on/off terminal and the VI(-) terminal (V<sub>on/off</sub>). The switch can be an open collector or equivalent (see Figure 11). A logic low is V<sub>on/off</sub> = 0 V to 1.2 V, during which the module is on. The maximum I<sub>on/off</sub> during a logic low is 1 mA. The switch should maintain a logic-low voltage while sinking 1 mA.

During a logic high, the maximum V<sub>on/off</sub> generated by the power module is 15 V. The maximum allowable leakage current of the switch at V<sub>on/off</sub> = 15 V is 50 μA.

If not using the remote on/off feature, short the ON/OFF pin to VI(-).



8-580 (C).d

Figure 11. Remote On/Off Implementation

### Remote Sense

Remote sense minimizes the effects of distribution losses by regulating the voltage at the remote-sense connections. The voltage between the remote-sense pins and the output terminals must not exceed the output voltage sense range given in the Feature Specifications table, i.e.:

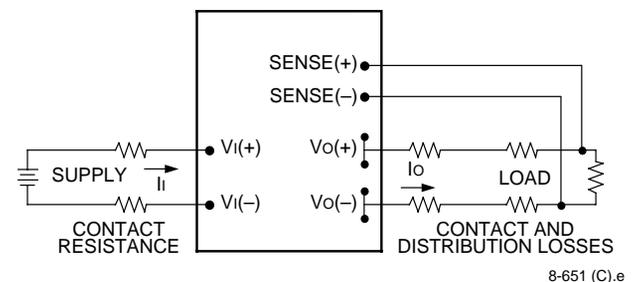
$$[V_o(+)-V_o(-)]-[SENSE(+)-SENSE(-)] \leq 1.2 \text{ V}$$

The voltage between the Vo(+) and Vo(-) terminals must not exceed the minimum value indicated in the output overvoltage protection section of the Feature Specifications table. This limit includes any increase in voltage due to remote-sense compensation and output voltage set-point adjustment (trim), see Figure 12.

If not using the remote-sense feature to regulate the output at the point of load, connect SENSE(+) to Vo(+) and SENSE(-) to Vo(-) at the module.

Although the output voltage can be increased by both the remote sense and by the trim, the maximum increase for the output voltage is not the sum of both. The maximum increase is the larger of either the remote sense or the trim. Consult the factory if you need to increase the output voltage more than the above limitation.

The amount of power delivered by the module is defined as the voltage at the output terminals multiplied by the output current. When using remote sense and trim, the output voltage of the module can be increased, which at the same output current would increase the power output of the module. Care should be taken to ensure that the maximum output power of the module remains at or below the maximum rated power.



8-651 (C).e

Figure 12. Effective Circuit Configuration for Single-Module Remote-Sense Operation

### Output Voltage Set-Point Adjustment (Trim)

Output voltage trim allows the user to increase or decrease the output voltage set point of a module. This is accomplished by connecting an external resistor between the TRIM pin and either the SENSE(+) or SENSE(-) pins. The trim resistor should be positioned close to the module.

If not using the trim feature, leave the TRIM pin open.

With an external resistor between the TRIM and SENSE(-) pins (R<sub>adj-down</sub>), the output voltage set point (V<sub>O, adj</sub>) decreases (see Figure 13). The following equation determines the required external-resistor value to obtain a percentage output voltage change of Δ%.

$$R_{\text{adj-down}} = \left( \frac{205}{\Delta\%} - 2.255 \right) \text{ k}\Omega$$

The test results for this configuration are displayed in Figure 14. This figure applies to all output voltages.

**Feature Descriptions** (continued)

**Output Voltage Set-Point Adjustment (Trim)**  
 (continued)

With an external resistor connected between the TRIM and SENSE(+) pins ( $R_{adj-up}$ ), the output voltage set point ( $V_{O, adj}$ ) increases (see Figure 15).

The following equation determines the required external-resistor value to obtain a percentage output voltage change of  $\Delta\%$ .

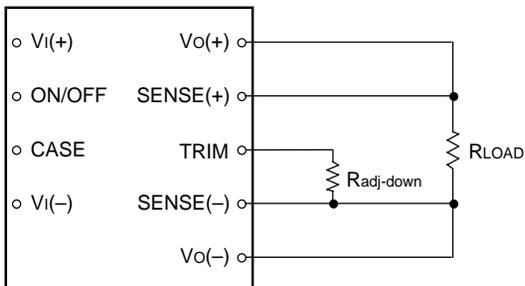
$$R_{adj-up} = \left( \frac{(V_{O, nom}(1 + \frac{\Delta\%}{100}) - 1.225)}{1.225\Delta\%} - 205 - 2.255 \right) k\Omega$$

The test results for this configuration are displayed in Figure 14.

The voltage between the  $V_{O}(+)$  and  $V_{O}(-)$  terminals must not exceed the minimum value of the output over-voltage protection as indicated in the Feature Specifications table. This limit includes any increase in voltage due to remote-sense compensation and output voltage set-point adjustment (trim). See Figure 12.

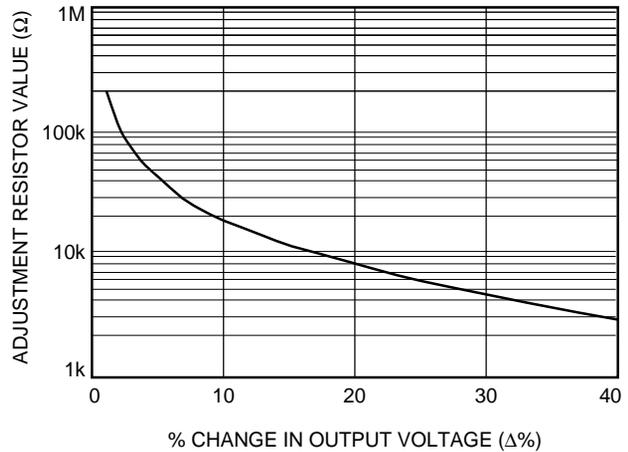
Although the output voltage can be increased by both the remote sense and by the trim, the maximum increase for the output voltage is not the sum of both. The maximum increase is the larger of either the remote sense or the trim. Consult the factory if you need to increase the output voltage more than the above limitation.

The amount of power delivered by the module is defined as the voltage at the output terminals multiplied by the output current. When using remote sense and trim, the output voltage of the module can be increased, which at the same output current would increase the power output of the module. Care should be taken to ensure that the maximum output power of the module remains at or below the maximum rated power.



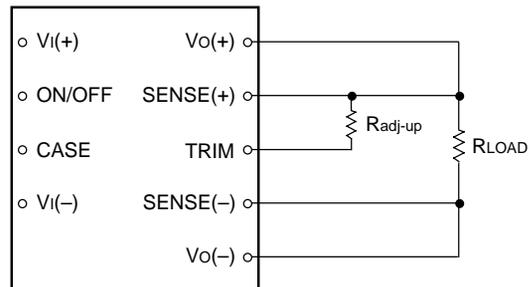
8-748 (C).b

**Figure 13. Circuit Configuration to Decrease Output Voltage**



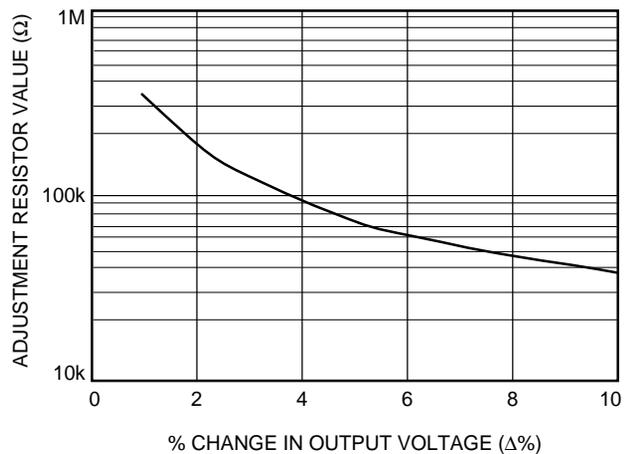
8-2883 (F)

**Figure 14. Resistor Selection for Decreased Output Voltage**



8-715 (C).b

**Figure 15. Circuit Configuration to Increase Output Voltage**



8-2884 (F)

**Figure 16. Resistor Selection for Increased Output Voltage**

## Feature Descriptions (continued)

### Output Overvoltage Protection

The output voltage is monitored at the  $V_o(+)$  and  $V_o(-)$  pins of the module. If the voltage at these pins exceeds the value indicated in the Feature Specifications table, the module will shut down and latch off. Recovery from latched shutdown is accomplished by cycling the dc input power off for at least 1.0 second or toggling the primary referenced on/off signal for at least 1.0 second.

### Output Current Monitor

The CURRENT MON pin provides a dc voltage proportional to the dc output current of the module given in the Feature Specifications table. For example, on the FC250F1, the V/A ratio is set at  $67 \text{ mV/A} \pm 10\%$  @  $70^\circ\text{C}$  case. At a full load current of 50 A, the voltage on the CURRENT MON pin is 3.685 V. The current monitor signal is referenced to the SENSE(-) pin on the secondary and is supplied from a source impedance of approximately 2 k $\Omega$ . It is recommended that the CURRENT MON pin be left open when not in use, although no damage will result if the CURRENT MON pin is shorted to secondary ground. Directly driving the CURRENT MON pin with an external source will detrimentally affect operation of the module and should be avoided.

### Synchronization

Any module can be synchronized to any other module or to an external clock using the SYNC IN or SYNC OUT pins. The modules are not designed to operate in a master/slave configuration; that is, if one module fails, the other modules will continue to operate.

#### SYNC IN Pin

This pin can be connected either to an external clock or directly to the SYNC OUT pin of another FC250x module.

If an external clock signal is applied to the SYNC IN pin, the signal must be a 500 kHz ( $\pm 50$  kHz) square wave with a 4 Vp-p amplitude. Operation outside this frequency band will detrimentally affect the performance of the module and must be avoided.

If the SYNC IN pin is connected to the SYNC OUT pin of another module, the connection should be as direct as possible, and the  $V_i(-)$  pins of the modules must be shorted together.

Unused SYNC IN pins should be tied to  $V_i(-)$ . If the SYNC IN pin is unused, the module will operate from its own internal clock.

#### SYNC OUT Pin

This pin contains a clock signal referenced to the  $V_i(-)$  pin. The frequency of this signal will equal either the module's internal clock frequency or the frequency established by an external clock applied to the SYNC IN pin.

When synchronizing several modules together, the modules can be connected in a daisy-chain fashion where the SYNC OUT pin of one module is connected to the SYNC IN pin of another module. Each module in the chain will synchronize to the frequency of the first module in the chain.

To avoid loading effects, ensure that the SYNC OUT pin of any one module is connected to the SYNC IN pin of only one module. Any number of modules can be synchronized in this daisy-chain fashion.

### Overtemperature Protection

To provide protection in a fault condition, the unit is equipped with an overtemperature shutdown circuit. The shutdown circuit will not engage unless the unit is operated above the maximum case temperature. Recovery from overtemperature shutdown is accomplished by cycling the dc input power off for at least 1.0 second or toggling the primary referenced on/off signal for at least 1.0 second.

### Forced Load Sharing (Parallel Operation)

For either redundant operation or additional power requirements, the power modules can be configured for parallel operation with forced load sharing (see Figure 17). For a typical redundant configuration, Schottky diodes or an equivalent should be used to protect against short-circuit conditions. Because of the remote sense, the forward-voltage drops across the Schottky diodes do not affect the set point of the voltage applied to the load. For additional power requirements, where multiple units are used to develop combined power in excess of the rated maximum, the Schottky diodes are not needed.

**Feature Descriptions** (continued)

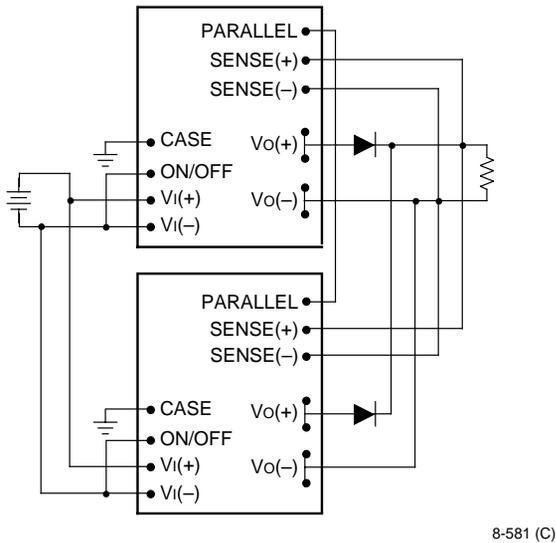
**Forced Load Sharing (Parallel Operation)**

(continued)

Good layout techniques should be observed for noise immunity. To implement forced load sharing, the following connections must be made:

- The parallel pins of all units must be connected together. The paths of these connections should be as direct as possible.
- All remote-sense pins should be connected to the power bus at the same point, i.e., connect all SENSE(+) pins to the (+) side of the power bus at the same point and all SENSE(-) pins to the (-) side of the power bus at the same point. Close proximity and directness are necessary for good noise immunity.

When not using the parallel feature, leave the PARALLEL pin open.



**Figure 17. Wiring Configuration for Redundant Parallel Operation**

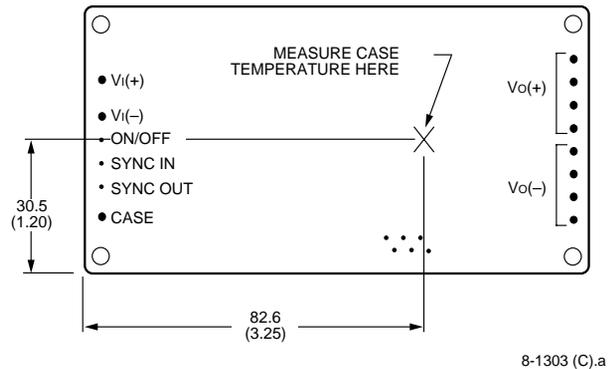
**Power Good Signal**

The PWR GOOD pin provides an open-drain signal (referenced to the SENSE(-) pin) that indicates the operating state of the module. A low impedance (<100 Ω) between PWR GOOD and SENSE(-) indicates that the module is operating. A high impedance (>1 MΩ) between PWR GOOD and SENSE(-) indicates that the module is off or has failed. The PWR GOOD pin can be pulled up through a resistor to an external voltage to facilitate sensing. This external voltage level must not exceed 40 V, and the current into the PWR GOOD pin during the low-impedance state should be limited to 1 mA maximum.

**Thermal Considerations**

**Introduction**

The power modules operate in a variety of thermal environments; however, sufficient cooling should be provided to help ensure reliable operation of the unit. Heat-dissipating components inside the unit are thermally coupled to the case. Heat is removed by conduction, convection, and radiation to the surrounding environment. Proper cooling can be verified by measuring the case temperature. Peak temperature occurs at the position indicated in Figure 18.



Note: Top view, measurements shown in millimeters and (inches). Pin locations are for reference only.

**Figure 18. Case Temperature Measurement Location**

## Thermal Considerations (continued)

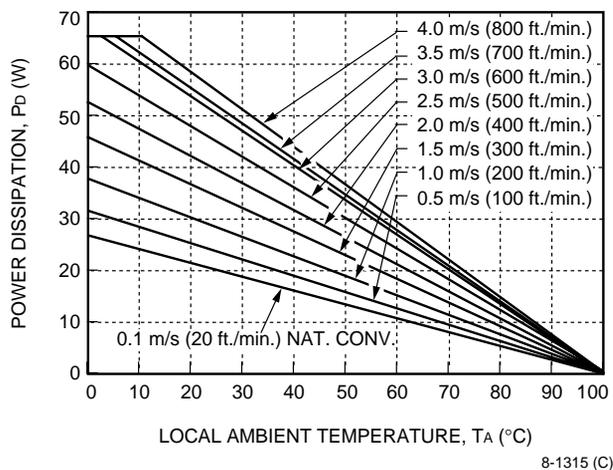
### Introduction (continued)

The temperature at this location should not exceed 100 °C. The maximum case temperature can be limited to a lower value for extremely high reliability. The output power of the module should not exceed the rated power for the module as listed in the Ordering Information table.

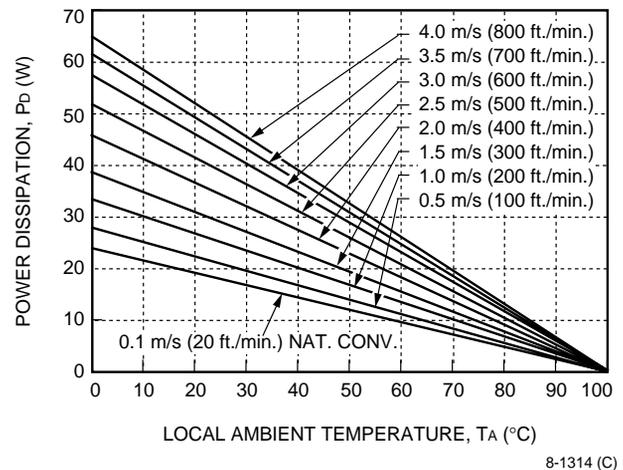
For additional information about these modules, refer to the Lucent Technologies *Thermal Management for FC- and FW-Series 250 W—300 W Board-Mounted Power Modules* Technical Note (TN96-009EPS).

### Heat Transfer Without Heat Sinks

Derating curves for forced-air cooling without a heat sink are shown in Figures 19 and 20. These curves can be used to determine the appropriate airflow for a given set of operating conditions. For example, if the unit with airflow along its length dissipates 20 W of heat, the correct airflow in a 40 °C environment is 1.0 m/s (200 ft./min.).



**Figure 19. Convection Power Derating with No Heat Sink; Airflow Along Width; Transverse Orientation**



**Figure 20. Convection Power Derating with No Heat Sink; Airflow Along Length; Longitudinal Orientation**

### Heat Transfer with Heat Sinks

The power modules have through-threaded, M3 x 0.5 mounting holes, which enable heat sinks or cold plates to be attached to the module. The mounting torque must not exceed 0.56 N-m (5 in.-lb.). For a screw attachment from the pin side, the recommended hole size on the customer's PWB around the mounting holes is 0.130 ± 0.005 inches. If a larger hole is used, the mounting torque from the pin side must not exceed 0.25 N-m (2.2 in.-lb.).

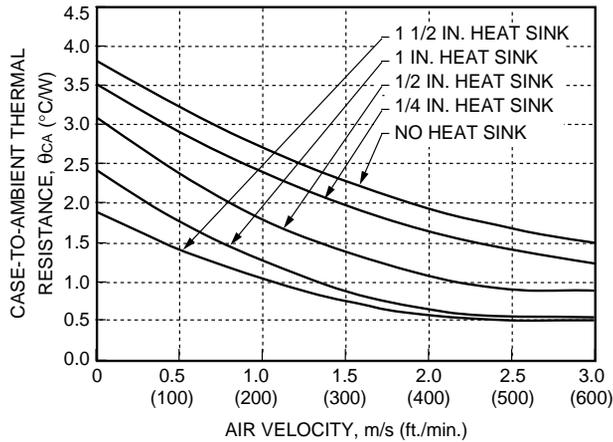
Thermal derating with heat sinks is expressed by using the overall thermal resistance of the module. Total module thermal resistance ( $\theta_{ca}$ ) is defined as the maximum case temperature rise ( $\Delta T_{C, max}$ ) divided by the module power dissipation ( $P_D$ ):

$$\theta_{ca} = \left[ \frac{\Delta T_{C, max}}{P_D} \right] = \left[ \frac{(T_C - T_A)}{P_D} \right]$$

The location to measure case temperature ( $T_C$ ) is shown in Figure 18. Case-to-ambient thermal resistance vs. airflow for various heat sink configurations is shown in Figures 21 and 22. These curves were obtained by experimental testing of heat sinks, which are offered in the product catalog.

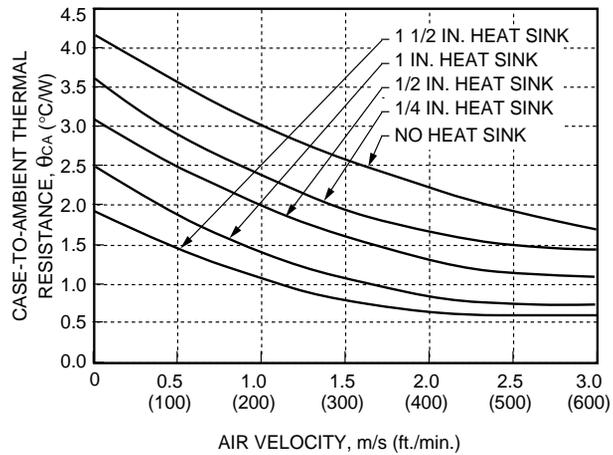
**Thermal Considerations** (continued)

**Heat Transfer with Heat Sinks** (continued)



8-1321 (C)

**Figure 21. Case-to-Ambient Thermal Resistance Curves; Transverse Orientation**

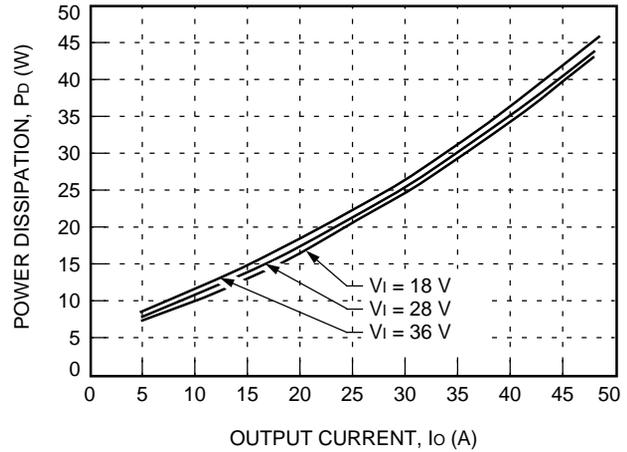


8-1320 (C)

**Figure 22. Case-to-Ambient Thermal Resistance Curves; Longitudinal Orientation**

These measured resistances are from heat transfer from the sides and bottom of the module as well as the top side with the attached heat sink; therefore, the case-to-ambient thermal resistances shown are generally lower than the resistance of the heat sink by itself. The module used to collect the data in Figures 21 and 22 had a thermal-conductive dry pad between the case and the heat sink to minimize contact resistance.

To choose a heat sink, determine the power dissipated as heat by the unit for the particular application. Figure 23 shows typical heat dissipation for a range of output currents and three voltages for the FC250F1.



8-2885 (F)

**Figure 23. FC250F1 Power Dissipation vs. Output Current at 25 °C**

**Example**

If an 85 °C case temperature is desired, what is the minimum airflow necessary? Assume the FC250F1 module is operating at  $V_i = 28\text{ V}$  and an output current of 40 A, maximum ambient air temperature of 40 °C, and the heat sink is 1.0 inch.

**Solution**

- Given:  $V_i = 28\text{ V}$
- $I_o = 40\text{ A}$
- $T_A = 40\text{ °C}$
- $T_C = 85\text{ °C}$
- Heat sink = 1.0 inch

Determine  $P_D$  by using Figure 23:

$$P_D = 35\text{ W}$$

Then solve the following equation:

$$\theta_{ca} = \left[ \frac{(T_C - T_A)}{P_D} \right]$$

$$\theta_{ca} = \left[ \frac{(85 - 40)}{35} \right]$$

$$\theta_{ca} = 1.3\text{ °C/W}$$

## Thermal Considerations (continued)

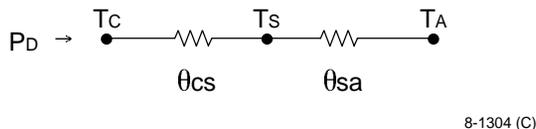
### Heat Transfer with Heat Sinks (continued)

Use Figures 21 and 22 to determine air velocity for the 1.0 inch heat sink. The minimum airflow necessary for this module depends on heat sink fin orientation and is shown below:

- 1.0 m/s (200 ft./min.) (oriented along width)
- 1.15 m/s (230 ft./min.) (oriented along length)

### Custom Heat Sinks

A more detailed model can be used to determine the required thermal resistance of a heat sink to provide necessary cooling. The total module resistance can be separated into a resistance from case-to-sink ( $\theta_{cs}$ ) and sink-to-ambient ( $\theta_{sa}$ ) as shown in Figure 24.



**Figure 24. Resistance from Case-to-Sink and Sink-to-Ambient**

For a managed interface using thermal grease or foils, a value of  $\theta_{cs} = 0.1 \text{ }^\circ\text{C/W}$  to  $0.3 \text{ }^\circ\text{C/W}$  is typical. The solution for heat sink resistance is:

$$\theta_{sa} = \left[ \frac{(T_C - T_A)}{P_D} \right] - \theta_{cs}$$

This equation assumes that all dissipated power must be shed by the heat sink. Depending on the user-defined application environment, a more accurate model, including heat transfer from the sides and bottom of the module, can be used. This equation provides a conservative estimate for such instances.

### EMC Considerations

For assistance with designing for EMC compliance, please refer to the FLTR100V10 data sheet (DS99-294EPS).

### Layout Considerations

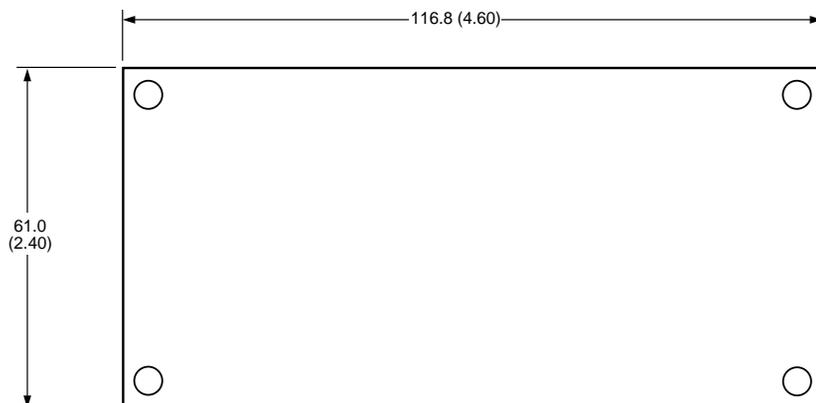
Copper paths must not be routed beneath the power module mounting inserts. For additional layout guidelines, refer to the FLTR100V10 data sheet (DS99-294EPS).

## Outline Diagram

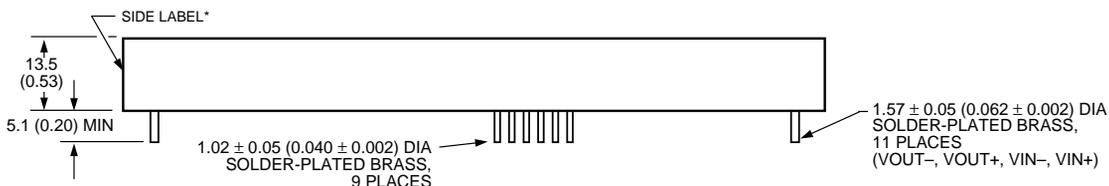
Dimensions are in millimeters and (inches).

Tolerances: x.x mm  $\pm$  0.5 mm (x.xx in.  $\pm$  0.02 in.),  
 x.xx mm  $\pm$  0.25 mm (x.xxx in.  $\pm$  0.010 in.)

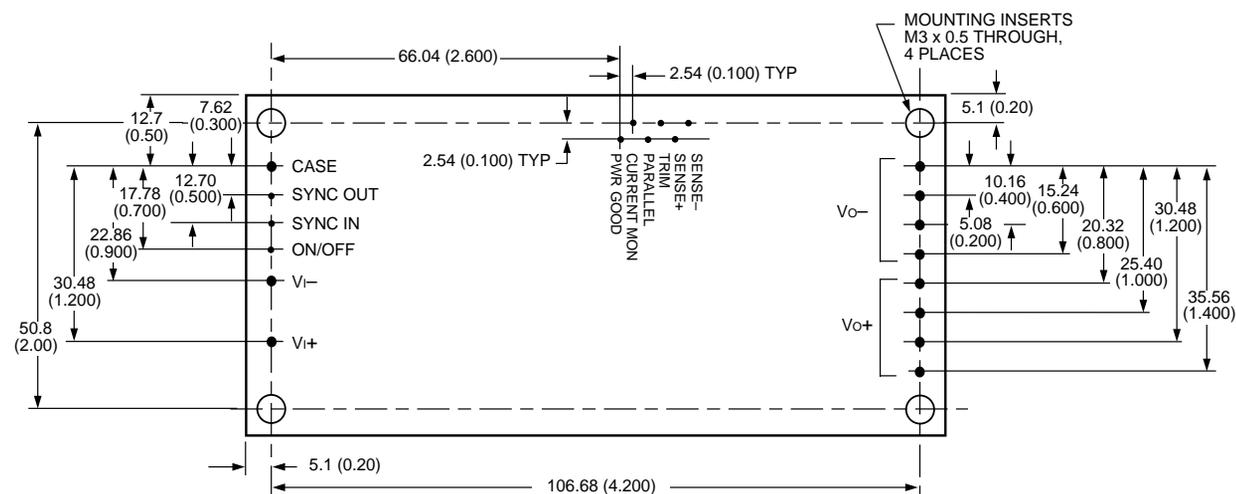
### Top View



### Side View



### Bottom View



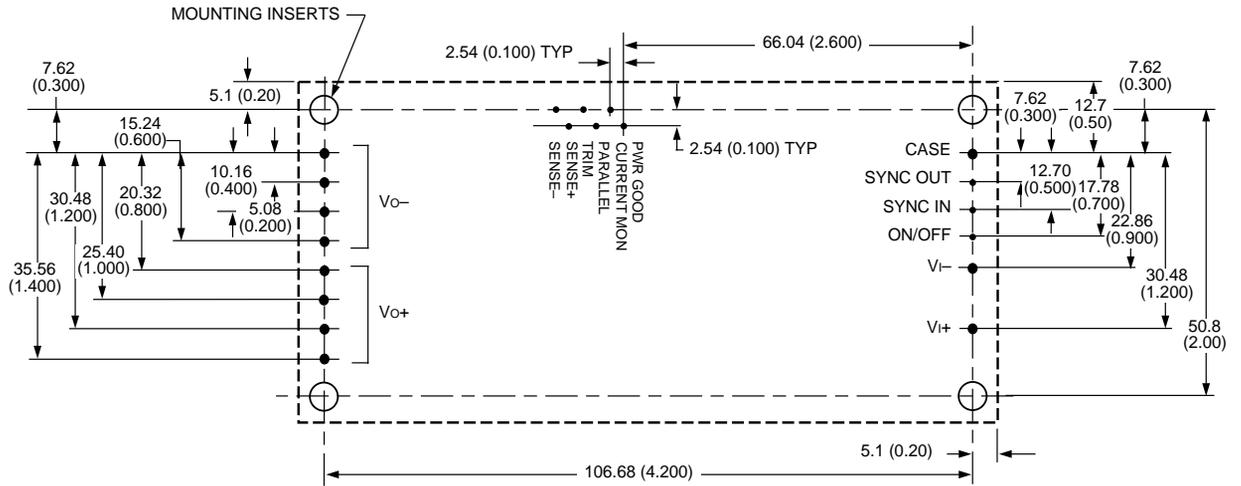
8-1650 (C).a

\* Side label includes Lucent logo, product designation, safety agency markings, input/output voltage and current ratings, and bar code.

## Recommended Hole Pattern

Component-side footprint.

Dimensions are in millimeters and (inches).



8-1650 (C).a

## Ordering Information

Table 5. Device Codes

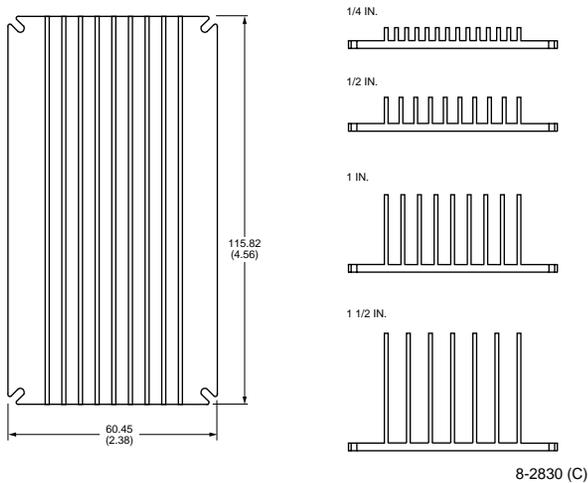
Input Voltage	Output Voltage	Output Power	Device Code	Comcode
28 V	3.3 V	165 W	FC250F1	108178740

**Ordering Information** (continued)

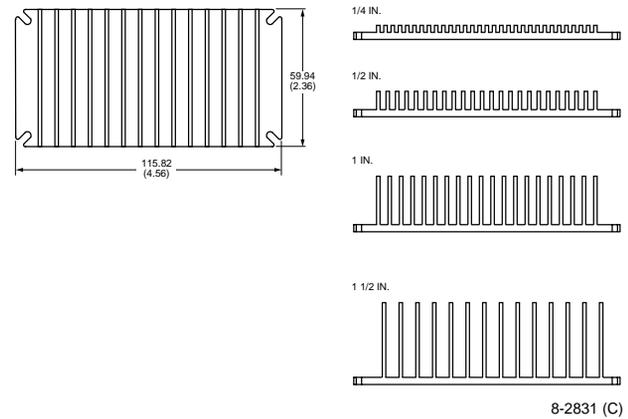
**Table 6. Device Accessories**

Accessory	Comcode
1/4 in. transverse kit (heat sink, thermal pad, and screws)	847308335
1/4 in. longitudinal kit (heat sink, thermal pad, and screws)	847308327
1/2 in. transverse kit (heat sink, thermal pad, and screws)	847308350
1/2 in. longitudinal kit (heat sink, thermal pad, and screws)	847308343
1 in. transverse kit (heat sink, thermal pad, and screws)	847308376
1 in. longitudinal kit (heat sink, thermal pad, and screws)	847308368
1 1/2 in. transverse kit (heat sink, thermal pad, and screws)	847308392
1 1/2 in. longitudinal kit (heat sink, thermal pad, and screws)	847308384

Dimension are in millimeters and (inches).



**Figure 25. Longitudinal Heat Sink**



**Figure 26. Transverse Heat Sink**

**Notes**

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