

AS1301

Data Sheet

5V/50mA Low Noise Inductorless Boost Converter

1 General Description

The AS1301 is a 50mA inductorless boost converter using a double H-bridge charge-pump topology with two external flying capacitors.

The AS1301 runs on a 1MHz fixed frequency and is utilized with a low noise regulation scheme to allow usage together with sensitive RF circuitry from the same battery supply.

Designed to reside in portable and space limited equipment the 1MHz charge pump converts a 2.7 to 5.25V input to regulated 5V output with 5% accuracy.

The shutdown function reduces the supply current to <5µA and disconnects the load from the output. The integrated soft-start circuitry prevents current spikes being drawn from the battery during start-up.

The AS1301 is available in TDFN (3x3x0.8mm) 10-pin and WL-CSP 8-bumps packages.

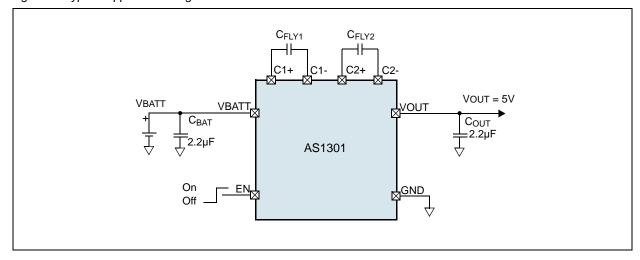
2 Key Features

- Up to 92% Efficiency
- 2.7 to 5.25V Input Voltage
- Regulated 5V Output
- Automatic Mode Up-Switching
- <5µA Shutdown Current
- 5V Tolerant Enable Signal
- Up to 50mA Load Current
- Overload Protection
- Output Disconnected During Shutdown
- Soft-Start
- No Inductor Required
- Small External Components Required (Cout ≤2.2µF, CFLY ≤220nF)
- Low Noise Fixed Frequency 1MHz Charge Pump:
 - 1:1 Battery Feed Through Mode
 - 2:3 Single Phase Mode
 - 1:2 Dual Phase Mode
- Package Options:
 - TDFN (3x3x0.8mm) 10-pin
 - WL-CSP 8-bumps with 0.5mm pitch

3 Applications

The device is ideal for two or three AA cells or a single Li-lon battery cell to 5V conversion, mobile phones, portable instruments, microprocessor based systems and remote data-acquisition systems.

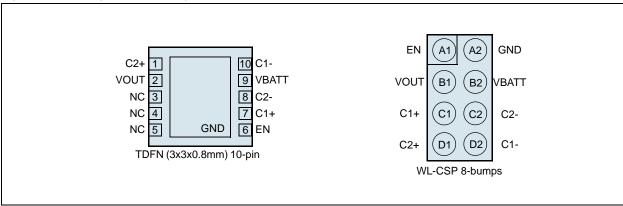
Figure 1. Typical Application Diagram





4 Pin Assignments

Figure 2. Pin Assignments (Through View)



Pin Descriptions

Table 1. Pin Descriptions

Pin Name	TDFN Pinout	WLP Pinout	Description
C2+	1	D1	Connector 2+. Positive terminal of flying cap 2.
VOUT	2	B1	+5V Output Voltage. This pin must be bypassed with a ≥2.2µF low ESR ceramic capacitor.
NC	3	-	Connected to GND or left floating.
NC	4	-	Connected to GND or left floating.
NC	5	-	Connected to GND or left floating.
EN	6	A1	Enable. (operating if EN = 1). Set this digital input to logic high for normal operation. For shutdown, set to logic low.
C1+	7	C1	Connector 1+. Positive terminal of flying cap 1.
C2-	8	C2	Connector 2 Negative terminal of flying cap 2.
VBATT	9	B2	+2.7V to 5.25V Input Voltage . Bypass this pin to GND with a ≥2.2µF low ESR ceramic capacitor.
C1-	10	D2	Connector 1 Negative terminal of flying cap 1.
GND	Exposed Pad	A2	Ground.



5 Absolute Maximum Ratings

Stresses beyond those listed in Table 2 may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in Section 6 Electrical Characteristics on page 4 is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Table 2. Absolute Maximum Ratings

Parameter	Min	Max	Units	Notes
All pins to GND	-0.3 +7.0		V	
Operating Temperature Range	-40	+85	°C	
Storage Temperature Range	-65	+125	°C	
ESD	2		kV	HBM MIL-Std. 883E 3015.7 methods
Package Body Temperature	+2	260	°C	The reflow peak soldering temperature (body temperature) specified is in accordance with IPC/JEDEC J-STD-020C "Moisture/Reflow Sensitivity Classification for Non-Hermetic Solid State Surface Mount Devices". The lead finish for Pb-free leaded packages is matte tin (100% Sn).



6 Electrical Characteristics

VIN = 2.7 to 5.25V, VOUT = 5V, $COUT = CBAT = 2.2\mu F$, CFLY1 = CFLY2 = 220nF, TAMB = -40 to $+85^{\circ}C$. Typical values are at $TAMB = +25^{\circ}C$, unless otherwise specified.

Table 3. Electrical Characteristics

Symbol	Parameter	Conditions	Min	Тур	Max	Units
Von	Startup Voltage, Rising VBATT			2.8	2.865	V
Voff	Startup Voltage, Falling VBATT		2.505	2.7	2.8	V
VBATT	Battery Supply Voltage		Von/ Voff	3.6	5.25	V
Vout	Settled Average Output Voltage		4.75	5.0	5.25	V
Іоит	Load Current ¹	after startup of 1ms	0		50	mA
V _{ripple}	Output Voltage Ripple	$C_{OUT} = 2.2 \mu F$, 50mA load		15		mV _{PP}
tstart	Startup Time				1	ms
l _{inr}	Inrush Current ²				500	mA
$\Delta V_{O}/\Delta I_{O11}$	Load Regulation in 1:1 Mode	VBATT = 5V, IOUT = 10~50mA		2		
$\Delta V_{O}/\Delta I_{O23}$	Load Regulation in 2:3 Mode	in 2:3 Mode		3		mV/mA
ΔV _O /ΔI _{O12}	Load Regulation in 1:2 Mode	VBATT = 3.1V, IOUT = 10~50mA		3		
η ₁₂	Efficiency in Switching Mode	VBATT = 3.1V, IOUT = 30mA		90		%
η23	Efficiency in Switching Mode	VBATT = 3.5V, IOUT = 30mA		90		%
fosc	Oscillator Frequency	optional selectable		1		MHz
t _{debup}	Up Switching Debounce Time			256		μs
I _{OP12}	Operating Quiescent Current	1:2 mode without load		1.5	3.5	
I _{OP23}	Operating Quiescent Current	2:3 mode without load		1.3	3	mA
I _{OP11}	Operating Current 1:1 Mode	without load		0.1	0.3	
I _{OFF}	Shutdown Current	EN = 0V		0.7	5	μA
T _{OFFL}	Temperature Shutdown	mode off		145		۰C
T _{OFFH}	Temperature Shutdown	mode on		170		۰C
Input Leve	ls					
ViH	Input High Level	pin EN	1.5		5.5	V
VIL	Input Low Level	μιι Ειν	0.0		0.5	V

^{1.} The device is tested in a proprietary test mode.

^{2.} The inrush current is limited by the internal soft-start circuitry.



7 Typical Operating Characteristics

VIN = 2.7 to 5.25V, VOUT = 5V, $COUT = CBAT = 2.2\mu F$, CFLY1 = CFLY2 = 220nF, $TAMB = +25^{\circ}C$, unless otherwise specified.

Figure 3. Efficiency vs. Input Voltage; ILOAD=10mA

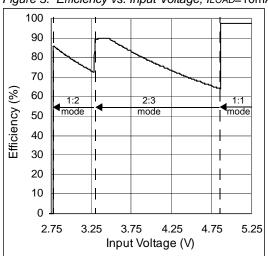


Figure 5. Efficiency vs. Input Voltage; ILOAD=30mA

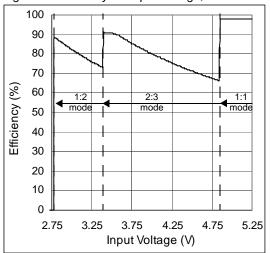


Figure 7. Efficiency vs. Input Voltage; ILOAD=50mA

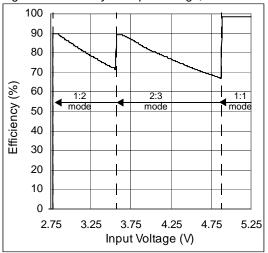


Figure 4. Efficiency vs. Input Voltage; ILOAD=20mA

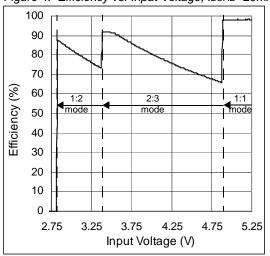


Figure 6. Efficiency vs.Input Voltage; ILOAD=40mA

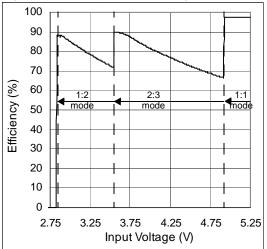


Figure 8. Quiescent Current vs. Input Voltage

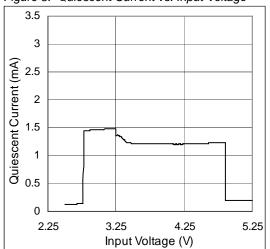


Figure 9. Output Voltage vs. Output Current

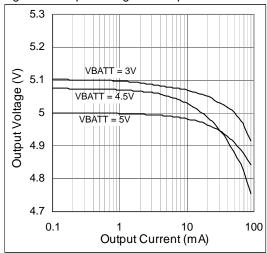


Figure 11. Output Voltage vs. Input Voltage

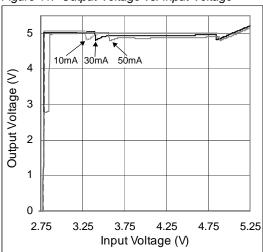


Figure 13. Output Voltage vs. Temp.; IouT = 10mA

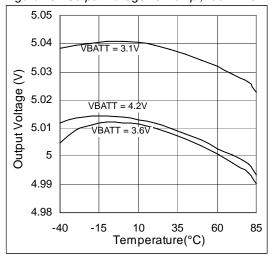


Figure 10. Output Voltage vs. Output Current

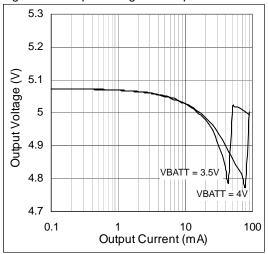


Figure 12. Output Voltage vs. Temp.; IOUT = 0.1mA

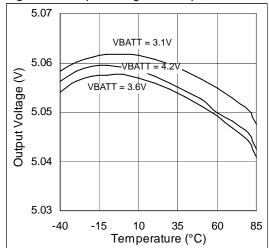


Figure 14. Output Voltage vs. Temp.; IouT = 30mA

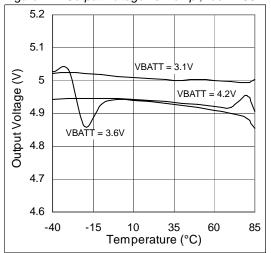


Figure 15. Efficiency vs. Output Current; VIN = 3V

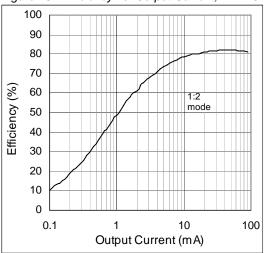


Figure 17. Efficiency vs. Output Current; VIN = 3.5V

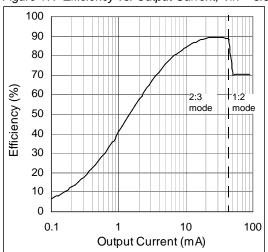


Figure 19. Efficiency vs. Output Current; VIN = 4.3V

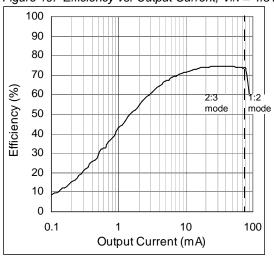


Figure 16. Efficiency vs. Output Current; VIN = 3.3V

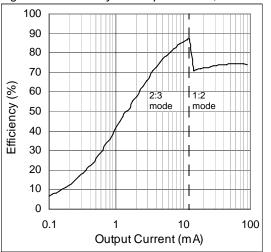


Figure 18. Efficiency vs. Output Current; VIN = 4V

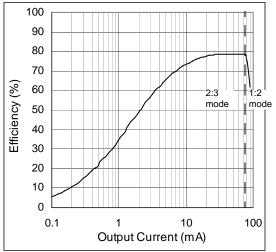


Figure 20. Efficiency vs. Output Current; VIN = 4.7V

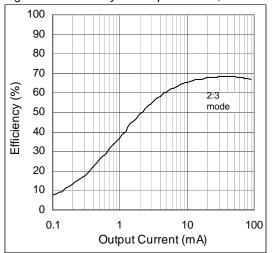




Figure 21. Load Transient; VBATT = 5.2V

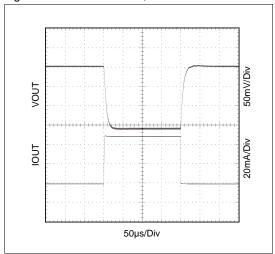


Figure 23. Start-Up Time; VBATT = 3V

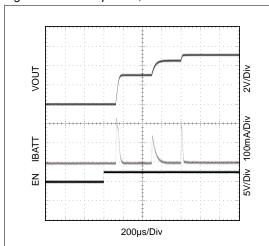


Figure 25. Line Transient; VBATT = 4.5V to 3.5V

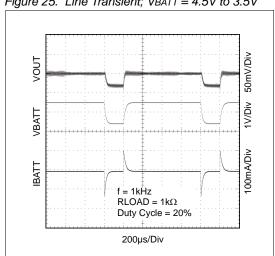


Figure 22. Load Transient; VBATT = 3.6V

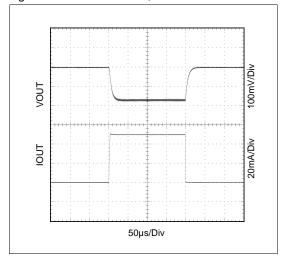
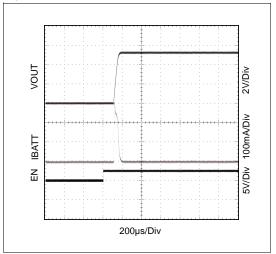


Figure 24. Start-Up Time; VBATT = 5.25V





8 Detailed Description

Operating Principle

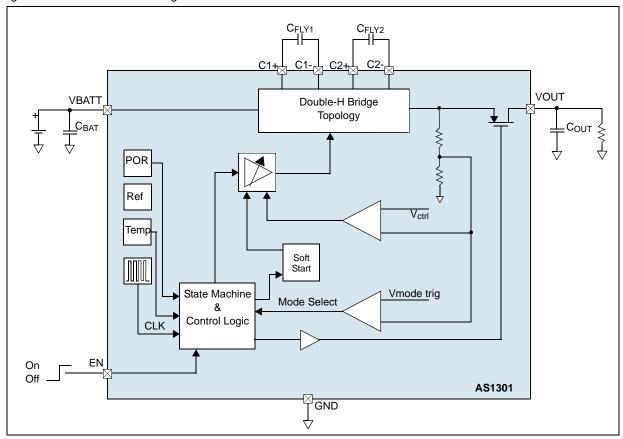
Functional Description

The AS1301 is a high efficiency and low noise switched capacitor DC-DC converter that is capable of boost operation. It is equipped with two built-in coupled H-bridge type switch configurations. Based on the value of the output voltage the system automatically initiates mode-switching to achieve the highest possible efficiency. The regulation of the output voltage is achieved by a regulation loop, which modulates the current drive capability of the power transistors so that the amount of charge transferred from the input to the output at each clock cycle is controlled and is equal to the charge needed by the load.

Regulation Loop

The AS1301 operates at constant frequency at any load. For the regulation loop power transistors, a resistor divider, and an error amplifier is used to keep the output voltage within the allowed limits. The error amplifier takes the feedback and reference signals as inputs and generates the error voltage signal. The error voltage controls a driver that triggers the gate of the power transistor which modulates the current drive capability of the power transistors. The modulated power transistors control the charge transferred from the input to the output and therefore the regulation of the output voltage is realized. Based on adjusting the amount of charge transferred, this regulation concept delivers the smallest voltage ripple possible.

Figure 26. Functional Block Diagram



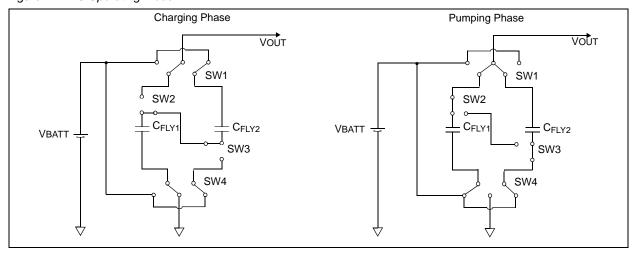


Switch Configuration

The AS1301 has nine built-in power switches in the shape of two coupled H-bridge topologies. The system features 1:2 and 2:3 operation modes as well as a 1:1 operation where the input is directly connected to the output. This feedthrough mode is suitable for input voltages higher than the output voltage.

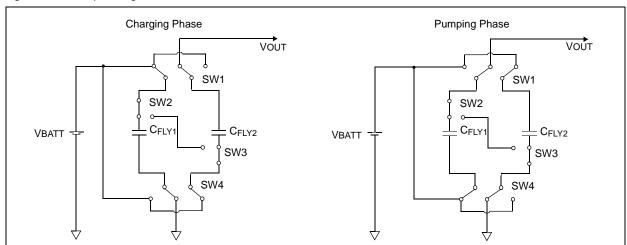
In 2:3 operation mode two flying capacitors are placed in series and each capacitor is charged to a half of the input voltage. In pumping phase the flying capacitors are placed in parallel. The bottom-plates of the parallel flying capacitors CFLY1 and CFLY2 are then connected to the input voltage so that the voltage at the top-plates of the flying capacitors is boosted to a voltage equal to VBATT + VBATT/2. By connecting the top-plates of the capacitors to the output, the output voltage in 2:3 mode can be up to one and a half of VBATT. If the top-plate voltage is higher than 5V, the regulation loop adapts the power transistor's current drive capability to drop some voltage. The 2:3 operation mode runs in single-phase operation only.

Figure 27. 2:3 Operating Mode



In 1:2 operation mode just one of both flying capacitors is placed in series to the input voltage, and therefore charged to the input voltage. During pumping phase the input voltage is connected to the bottom-plate of the discharged flying capacitor CFLY. The voltage at the top-plate of the capacitor is now boosted to 2VBATT. By connecting the top-plate of the capacitor to the output, the output can be charged to twice the voltage of VBATT. If the top-plate voltage is higher than 5V the regulation loop limits the charge transfer to the output. In collaboration with the second flying capacitor this mode features dual-phase operation.

Figure 28. 1:2 Operating Mode





Overload Protection

When the output voltage drops significantly below battery voltage due to a very high load the AS1301 enters into an overload protection condition. In this condition the output is connected to the input via a current limiting connection. Once the overload is removed, the device enters soft-start period and ramps up to the nominal output voltage.

Undervoltage Lockout, UVLO

The AS1301 is equipped with undervoltage lockout functionality. If the battery voltage drops below 2.7V (typ) the device enters the undervoltage lockout condition. The device remains in this condition until the battery voltage is high enough to enter the soft-start period. An internal hysteresis of 100mV will prevent ringing during startup. If the input voltage climbs back to 2.8V (typ) after such a condition, the device turns-on automatically.

Shutdown Mode

The AS1301 enters low-power shutdown mode when EN is set to logic low. In shutdown the charge-pump action is halted, the output is completely disconnected from the input and VouT will drop to 0V. During shutdown the output is set to a high-Z condition. So it can be forced higher voltage then the input, because the permanent monitoring of the input- and output voltage will prevent an erroneous current form the output back to the input during shutdown.

Thermal Shutdown

The AS1301 offers thermal shutdown, which prevents eventual damage due to an over-temperature condition. Thermal shutdown will be initiated if the junction temperature exceeds 145°C. If the temperature drops below this value, the thermal shutdown will be released automatically and the device will resume operation.



9 Application Information

External Component Selection

The high internal oscillator frequency of 1MHz permits the use of small capacitors for both, the flying capacitors and the output capacitors. For any given load value of the flying- and output capacitors as well as their ESR are affecting the output voltage performance.

In general, the capacitor's ESR is inversely proportional to its physical size. Larger capacitances and higher voltage ratings tend to reduce ESR. The ESR is a function of the frequency too, so it must be rated at the devices operating frequency. Another factor affecting capacitor ESR is temperature.

Note: Many capacitors have a huge capacity variation over temperature. This can be compensated by choosing a capacitor with a better thermal coefficient or by choosing a larger nominal value to ensure proper operation over temperature.

Input and Output Capacitor Selection

It is not critical which type of input bypass capacitor CBAT and output filter capacitor COUT is used, but it will affect the performance of the charge pump. Low ESR capacitors should be used to minimize VouT ripple. Multi-layer ceramic capacitors are recommended since they have extremely low ESR and are available in small footprints.

Input Capacitor

An 2.2µF input bypass low ESR capacitor such as tantalum or ceramic is recommended to reduce noise and supply transients. During startup and mode change it supplies part of the peak input current drawn by the device.

Output Capacitor

The output capacitor is charged to the Vout voltage during pumping phase. The ESR of the output capacitor introduces steps in the output voltage waveform whenever the charge pump charges Cout. These steps contribute to the ripple voltage of Vout. Therefore, ceramic or tantalum low ESR capacitors are recommended for Cout to minimize the output voltage ripple.

Table 4. Recommended Input and Output Capacitor

Part Number	С	TC Code	Rated Voltage	Dimensions (L/W/T)	Manufacturer
GRM21BR71A225KA01	2.2µF	X7R	10V	2x1.2x1.35mm	Murata www.murata.com

Flying Capacitor Selection

To ensure the required output current and avoid high peak currents the values of the flying capacitors CFLY1 and CFLY2 are very critical. A 220nF capacitor is sufficient for most applications. Dependent on the operation mode the AS1301 alternately charges and discharges CFLY1/2. Since the flying capacitors lead a higher current than the output capacitor the ESR of CFLY1/2 has a greater impact on the performance of the whole system. The voltage drop caused by the ESR of the flying capacitors directly adds to the output source resistance of the charge pump.

Therefore low ESR capacitors, e.g. tantalum or ceramic, are recommended for the flying capacitors as well.

Table 5. Recommended Flying Capacitor

Part Number	С	TC Code	Rated Voltage	Dimensions (L/W/T)	Manufacturer
GRM188R71E224KA88	220nF	X7R	25V	1.6x0.8x0.87mm	Murata www.murata.com



10 Package Drawings and Markings

The device is available in a TDFN (3x3x0.8mm) 10-pin and WL-CSP 8-bumps package.

Figure 29. TDFN (3x3x0.8mm) 10-pin package Diagram

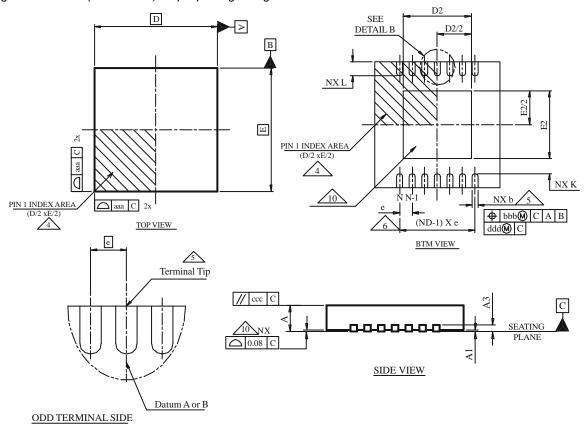


Table 6. TDFN (3x3x0.8mm) 10-pin package Dimensions

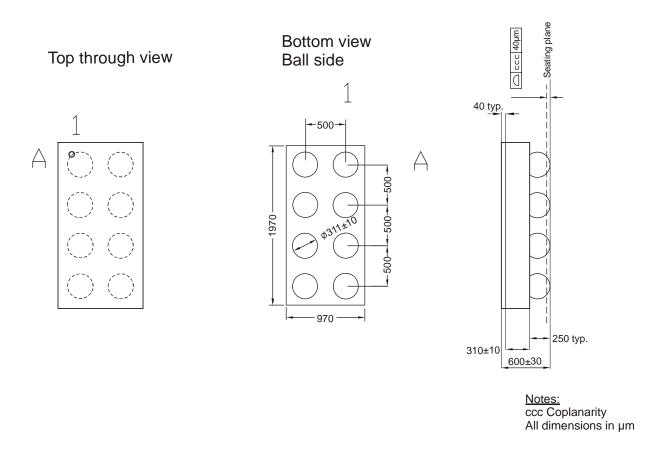
Symbol	Min	Тур	Max	Symbol	Min	Тур	Max
Α	0.70	0.75	0.80	D BSC		3.00	
A1	0.00	0.02	0.05	E BSC		3.00	
A3		0.20 REF		D2	2.20		2.70
L1	0.03		0.15	E2	1.40		1.75
L2			0.13	L	0.30	0.40	0.50
aaa		0.15		θ	00		
bbb		0.10		k	0.20		
ccc		0.10		b	0.18	0.25	0.30
ddd		0.05		е		0.50	
eee		0.08		N		10	
ggg		0.10		ND		5	

Note:

- 1. Dimensioning and tolerancing conform to ASME Y14.5M-1994.
- 2. All dimensions are in millimeters, angle is in degrees.
- 3. N is the total number of terminals.



Figure 30. WL-CSP 8-bumps Package Diagram





11 Ordering Information

Table 7. Ordering Information

Part	Marking	Description	Delivery Form	Package
AS1301A-BWLT	ASO4	5V/50mA Low Noise Inductorless Boost Converter	T&R	WL-CSP 8-bumps
AS1301A-BTDT	ASO4	5V/50mA Low Noise Inductorless Boost Converter	T&R	TDFN (3x3x0.8mm) 10-pin



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