

NCP81239

USB Power Delivery 4-Switch Buck Boost Controller

The NCP81239 USB Power Delivery (PD) Controller is a synchronous buck boost that is optimized for converting battery voltage or adaptor voltage into power supply rails required in notebook, tablet, and desktop systems, as well as many other consumer devices using USB PD standard and C-Type cables. The NCP81239 is fully compliant to the USB Power Delivery Specification when used in conjunction with a USB PD or C-Type Interface Controller. NCP81239 is designed for applications requiring dynamically controlled slew rate limited output voltage that require either voltage higher or lower than the input voltage. The NCP81239 drives 4 NMOSFET switches, allowing it to buck or boost and support the consumer and provider role swap function specified in the USB Power Delivery Specification which is suitable for all USB PD applications. The USB PD Buck Boost Controller operates with a supply and load range of 4.5 V to 28 V.

Features

- Wide Input Voltage Range: from 4.5 V to 28 V
- Dynamically Programmed Frequency from 150 kHz to 1.2 MHz
- I²C Interface
- Real Time Power Good Indication
- Controlled Slew Rate Voltage Transitioning
- Feedback Pin with Internally Programmed Reference
- Support USBPD/QC2.0/QC3.0 Profile
- 2 Independent Current Sensing Inputs
- Over Temperature Protection
- Adaptive Non-Overlap Gate Drivers
- Filter Capacitor Switch Control
- Over-Voltage and Over-Current Protection
- Dead Battery Power Support
- 5 x 5 mm QFN32 Package

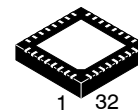
Typical Application

- Notebooks, Tablets, Desktops
- All in Ones
- Monitors, TVs, and Set Top Boxes
- Consumer Electronics



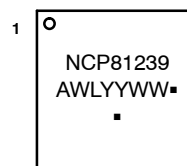
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QFN32 5x5, 0.5P
CASE 485CE

MARKING DIAGRAM



A = Assembly Location
WL = Wafer Lot
YY = Year
WW = Work Week
▪ = Pb-Free Package

(Note: Microdot may be in either location)

ORDERING INFORMATION

Device	Package	Shipping†
NCP81239MNTXG	QFN32 (Pb-Free)	4000 / Tape & Reel

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specification Brochure, BRD8011/D.

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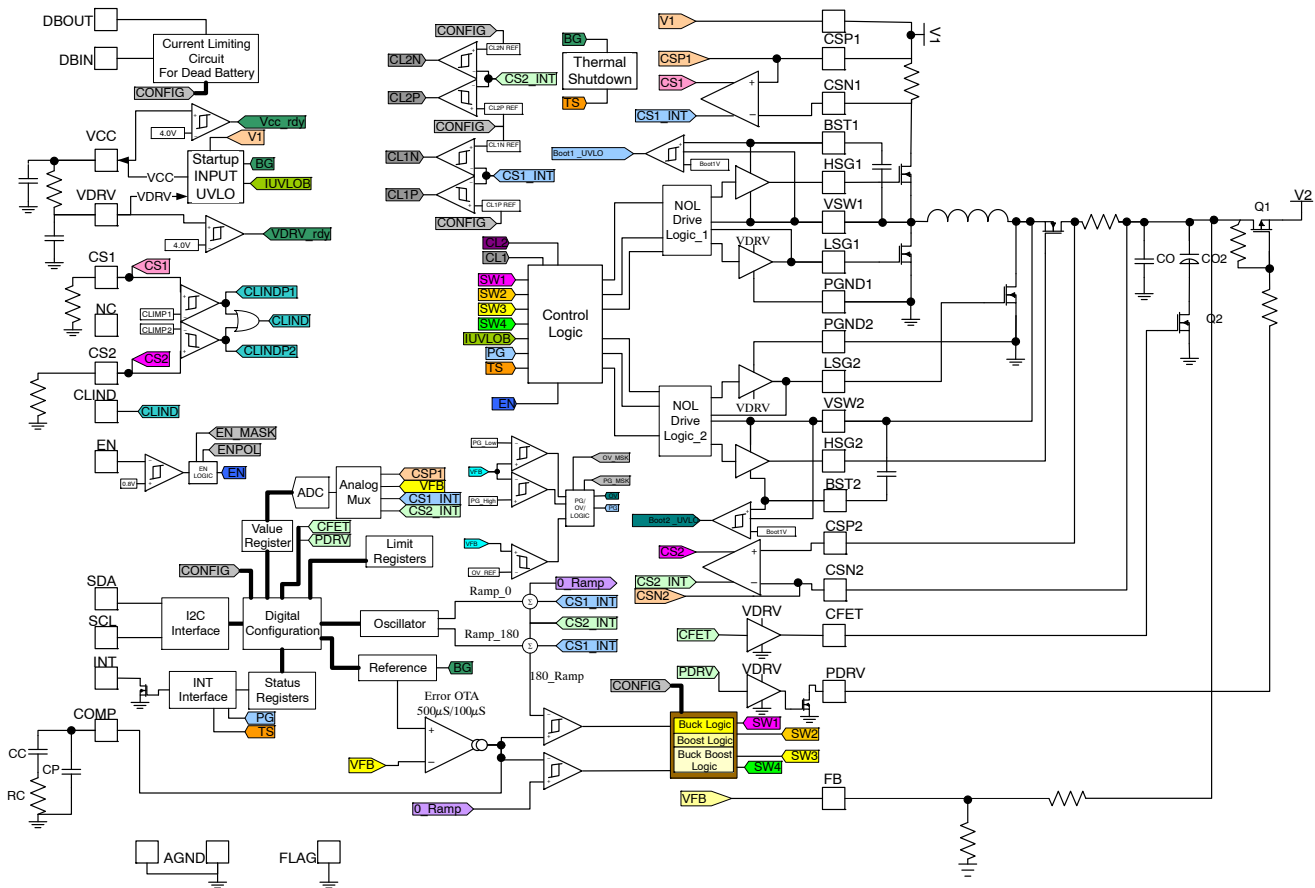


Figure 3. Block Diagram

Table 1. PIN FUNCTION DESCRIPTION

Pin	Pin Name	Description
1	HSG1	S1 gate drive. Drives the S1 N-channel MOSFET with a voltage equal to VDRV superimposed on the switch node voltage VSW1.
2	LSG1	Drives the gate of the S2 N-channel MOSFET between ground and VDRV.
3, 22	PGND	Power ground for the low side MOSFET drivers. Connect these pins closely to the source of the bottom N-channel MOSFETs.
4	CSN1	Negative terminal of the current sense amplifier.
5	CSP1	Positive terminal of the current sense amplifier.
6	V1	Input voltage of the converter
7	CS1	Current sense amplifier output. CS1 will source a current that is proportional to the voltage across RS1 to an external resistor. Ground this pin if not used.
8	CLIND	Open drain output to indicate that the CS1 or CS2 voltage has exceeded the I ² C programmed limit.
9	SDA	I ² C interface data line.
10	SCL	I ² C interface clock line.
11	INT	Interrupt is an open drain output that indicates the state of the output power, the internal thermal trip, and other I ² C programmable functions.
12	CFET	Controlled drive of an external MOSFET that connects a bulk output capacitor to the output of the power converter. Necessary to adhere to low capacitance limits of the standard USB Specifications for power prior to USB PD negotiation.
13-14	AGND	The ground pin for the analog circuitry.
15	COMP	Output of the transconductance amplifier used for stability in closed loop operation.

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Table 1. PIN FUNCTION DESCRIPTION

Pin	Pin Name	Description
16	EN	Precision enable starts the part and places it into default configuration when toggled.
17	PDRV	The open drain output used to control a PMOSFET.
18	CS2	Current sense amplifier output. CS2 will source a current that is proportional to the voltage across RS2 to an external resistor. Ground this pin if not used.
19	FB	Feedback voltage of the output, negative terminal of the gm amplifier.
20	CSN2	Negative terminal of the current sense amplifier.
21	CSP2	Positive terminal of the current sense amplifier.
23	LSG2	Drives the gate of the S2 N-channel MOSFET between ground and VDRV.
24	HSG2	S4 gate drive. Drives the S4 N-channel MOSFET with a voltage equal to VDRV superimposed on the switch node voltage VSW2.
25	BST2	Bootstrapped Driver Supply. The BST2 pin swings from a diode voltage below VDRV up to a diode voltage below FB + VDRV. Place a 0.1 μ F capacitor from this pin to VSW2.
26	VSW2	Switch Node. VSW2 pin swings from a diode voltage drop below ground up to output voltage.
27	DBOUT	The output of the dead battery circuit which can also be used for the VCONN voltage supply.
28	DBIN	The dead battery input to the converter where 5 V is applied. A 1 μ F capacitor should be placed close to the part to decouple this line.
29	VDRV	Internal voltage supply to the driver circuits. A 1 μ F capacitor should be placed close to the part to decouple this line.
30	VCC	The VCC pin supplies power to the internal circuitry. The VCC is the output of a linear regulator which is powered from V1. Can be used to supply up to a 100 mA load. Pin should be decoupled with a 1 μ F capacitor for stable operation.
31	VSW1	Switch Node. VSW1 pin swings from a diode voltage drop below ground up to V1.
32	BST1	Driver Supply. The BST1 pin swings from a diode voltage below VDRV up to a diode voltage below V1 + VDRV. Place a 0.1 μ F capacitor from this pin to VSW1.
33	THPAD	Center Thermal Pad. Connect to AGND externally.

Table 2. MAXIMUM RATINGS

Over operating free-air temperature range unless otherwise noted

Rating	Symbol	Min	Max	Unit
Input of the Dead Battery Circuit	DBIN	-0.3	5.5	V
Output of the Dead Battery Circuit	DBOUT	-0.3	5.5	V
Driver Input Voltage	VDRV	-0.3	5.5	V
Internal Regulator Output	VCC	-0.3	5.5	V
Output of Current Sense Amplifiers	CS1, CS2	-0.3	3.0	V
Current Limit Indicator	CLIND	-0.3	VCC + 0.3	V
Interrupt Indicator	INT	-0.3	VCC + 0.3	V
Enable Input	EN	-0.3	5.5	V
I ² C Communication Lines	SDA, SCL	-0.3	VCC + 0.3	V
Compensation Output	COMP	-0.3	VCC + 0.3	V
V1 Power Stage Input Voltage	V1	-0.3	40	V
Positive Current Sense	CSP1	-0.3	40	V
Negative Current Sense	CSN1	-0.3	40	V
Positive Current Sense	CSP2	-0.3	40	V
Negative Current Sense	CSN2	-0.3	40	V
Feedback Voltage	FB	-0.3	5.5	V

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Table 2. MAXIMUM RATINGS

Over operating free-air temperature range unless otherwise noted

Rating	Symbol	Min	Max	Unit
CFET Driver	CFET	-0.3	VCC + 0.3	V
Driver 1 and Driver 2 Positive Rails	BST1, BST2	-0.3 V wrt/PGND -0.3 V wrt/VSW	35 V wrt/PGND 5.5 V wrt/VSW	V
High Side Driver 1 and Driver 2	HSG1, HSG2	-0.3 V wrt/PGND -0.3 V wrt/VSW	30 V wrt/GND 5.5 V wrt/VSW	V
Switching Nodes and Return Path of Driver 1 and Driver 2	VSW1, VSW2	-5.0 V	35 V	V
Low Side Driver 1 and Driver 2	LSG1, LSG2	-0.3 V	5.5	V
PMOSFET Driver	PDRV	-0.3	40	V
Voltage Differential	AGND to PGND	-0.3	0.3	V
CSP1-CSN1, CSP2-CSN2 Differential Voltage	CS1DIF, CS2DIF	-0.5	0.5	V
PDRV Maximum Current	PDRVI	0	10	mA
Maximum VCC Current	VCCI	0	80	mA
Operating Junction Temperature Range (Note 1)	TJ	-40	150	°C
Operating Ambient Temperature Range	TA	-40	85	°C
Storage Temperature Range	TSTG	-55	150	°C
Thermal Characteristics (Note 2) QFN 32 5mm x 5mm Maximum Power Dissipation @ TA = 25°C Thermal Resistance Junction-to-Air with Solder	PD RθJA		3.53 35.4	W °C/W
Lead Temperature Soldering (10 sec): Reflow (SMD styles only) Pb-Free (Note 3)	RF		260 Peak	°C

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

1. The maximum package power dissipation limit must not be exceeded.
2. The value of θ_{JA} is measured with the device mounted on a 3in x 3in, 4 layer, 0.062 inch FR-4 board with 1.5 oz. copper on the top and bottom layers and 0.5 ounce copper on the inner layers, in a still air environment with $T_A = 25^\circ\text{C}$.
3. 60–180 seconds minimum above 237°C.

Table 3. ELECTRICAL CHARACTERISTICS

(V1 = 12 V, V_{out} = 1.0 V, T_A = +25°C for typical value; -40°C < T_A < 100°C for min/max values unless noted otherwise)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Units
Power Supply						
V1 Operating Input Voltage	V1		4.5		28	V
VDRV Operating Input Voltage	VDRV		4.5	5	5.5	V
VCC UVLO Rising Threshold	VCC _{START}			4.16		V
UVLO Hysteresis for VCC	VCCV _{HYS}	Falling Hysteresis		200		mV
VDRV UVLO Rising Threshold	VDRV _{START}			4.16		V
UVLO Hysteresis for VDRV	VDRV _{HYS}	Falling Hysteresis		200		mV
VCC Output Voltage	VCC	With no external load	4.90	5		V
VCC Drop Out Voltage	VCCDROOP	30 mA load		150		mV
VCC Output Current Limit	IOU _{VCC}	VCC Loaded to 4.3 V	80	97		mA

4. Ensured by design. Not production tested.

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(V1 = 12 V, V_{out} = 1.0 V, T_A = +25°C for typical value; -40°C < T_A < 100°C for min/max values unless noted otherwise)

V1 Quiescent Current	IV1Q	EN = 5V 4.2V ≤ V1 ≤ 28V LSG1, LSG2, HSG1, HSG2 are open COMP = 0V (Not Switching)		11	18	mA
V1 Shutdown Supply Current	IVCC_SD	EN = 0V 4.2V ≤ V1 ≤ 32V		6.6	7.7	mA
VDRIVE Switching Current Buck	IV1_SW	EN = 5, Cgate = 2.2 nF, VSW = 0 V FSW = 600 kHz, Comp = 1 V		12		mA
VDRIVE Switching Current Boost	IV1_SW	EN = 5, Cgate = 2.2 nF, VSW = 0 V FSW = 600 kHz, Comp = 1 V		12		mA

Voltage Output

Voltage Output Accuracy	FB	DAC_TARGET = 00110010	0.495	0.5	0.505	V
		DAC_TARGET = 01111000	1.188	1.2	1.212	
		DAC_TARGET = 11001000	1.98	2.0	2.02	
Voltage Accuracy Over Temperature	VOUTERT	PWM in CCM mode, -40°C < T _A < 100°C VFB > 0.5 V 0.17 V < VFB < 0.5 V 0.1 V < VFB < 0.17	-1.0 -2.0 -3.3		1.0 1.8 3.0	%
	VOUTER	T _A = 25°C VFB > 0.5 V 0.17 V < VFB < 0.5 V	-0.35 -1.0		0.35 1.2	%

Transconductance Amplifier

Gain Bandwidth Product	GBW	3db (Note 4)		5.2		MHz
Transconductance	GM1	Default		500		μS
Max Output Source Current limit	GMSOC		60	80		μA
Max Output Sink Current limit	GMSIC		60	80		μA
Voltage Ramp	Vramp			1.4		V

Internal BST Diode

Forward Voltage Drop	VFBOT	I _F = 10 mA, T _A = 25°C	0.42	0.46	0.51	V
Reverse Bias Leakage Current	DIL	BST-VSW = 5 V V _{SW} = 28 V, T _A = 25°C		0.05	0.16	μA
BST-VSW UVLO	BST1_UVLO	Rising, Note 4		3.5		V
BST-VSW Hysteresis	BST_HYS	Note 4		300		mV

Oscillator

Oscillator Frequency	FSW_0	FSW = 000, default	540	600	660	kHz
	FSW_1	FSW = 001	135	150	166	kHz
	FSW_7	FSW = 110	1058	1200	1320	kHz
Oscillator Frequency Accuracy	FSWE		-12		10	%
Minimum On Time	MOT	Measured at 10% to 90% of VCC, -40°C < T _A < 100°C		50		ns
Minimum Off Time	MOFT	Measured at 90% to 10% of VCC, -40°C < T _A < 100°C		90		ns

INT Thresholds

Interrupt Low Voltage	VINTI	IINT(sink) = 2 mA			0.04	V
Interrupt High Leakage Current	INII	3.3 V		3	11	nA
Interrupt Startup Delay	INTPG	Soft Start end to PG positive edge		2.1		ms

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(V₁ = 12 V, V_{out} = 1.0 V, T_A = +25°C for typical value; -40°C < T_A < 100°C for min/max values unless noted otherwise)

Interrupt Propagation Delay	PGI	Delay for power good in		3.3		ms
	PGO	Delay for power good out		100		ns
Power Good Threshold	PGTH	Power Good in from high VProfile = 0000 Margin = 000		105		%
	PGTH	Power Good in from low Vprofile = 0000 Margin = 000		95		%
	PGTHYS	PG falling hysteresis Vprofile = 0000 Margin = 000		2.5		%
FB Overvoltage Threshold	FB_OV	Vprofile = 0000 Margin = 000		116		%
Overvoltage Propagation Delay	VFB_OVDL			1 Cycle		

External Current Sense (CS1,CS2)

Offset Current Measurement	OSI0	CSP1-CSN1 or CSP2-CSN2 = 0 mV		110		nA
Offset Voltage Measurement	OSVO	CS = 0 μA		40		μV
Positive Current Measurement High	CS10	CSP1-CSN1 or CSP2-CSN2 = 100 mV		500		μA
Transconductance Gain Factor	CSGT	Current Sense Transconductance Vsense = 1 mV to 100 mV		5		mS
Transconductance Deviation	CSGE		-20		20	%
Current Sense Common Mode Range	CSCMMR		3		28	V
-3dB Small Signal Bandwidth	CSBW	VSENSE (AC) = 10 mVPP, RGAIN = 10 kΩ (Note 4)		30		MHz
Input Sense Voltage Full Scale	ISVFS				100	mV
CS Output Voltage Range	CSOR	VSENSE = 100 mV Rset = 6k	0		3	V

External Current Limit (CLIND)

Current Limit Indicator Output Low	CLINDL	Input current = 500 μA		5.6	10	mV
Current Limit Indicator Output High	CLINDH	Input current = 500 μA	4.0	5.0		V

Internal Current Sense

Internal Current Sense Gain for PWM	ICG	CSPx-CSNx = 100 mV	9.30	9.8	10.42	V/V
Positive Peak Current Limit Trip	PPCLT	INT_CL = 00,	34	39	44	mV
Negative Valley Current Limit Trip	NVCLT	INT_CL_NEG = 00	31	40	45	mV

Switching MOSFET Drivers

HSG1 HSG2 Pullup Resistance	HSG_PU	BST-VSW = 4.5 V		2.8		Ω
HSG1 HSG2 Pulldown Resistance	HSG_PD	BST-VSW = 4.5 V		1.2		Ω
LSG1 LSG2 Pullup Resistance	LSG_PU	LSG -PGND = 2.5 V		3.3		Ω
LSG1 LSG2 Pulldown Resistance	LSG_PD	LSG -PGND = 2.5 V		0.9		Ω
HSG Falling to LSG Rising Delay	HSLSD			15		ns
LSG Falling to HSG Rising Delay	LSHSD			15		ns

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(V₁ = 12 V, V_{out} = 1.0 V, T_A = +25°C for typical value; -40°C < T_A < 100°C for min/max values unless noted otherwise)

CFET

CFET Drive Voltage	CFETDV			VCC		V
Source/Sink Current	CFETSS	CFET clamped to 2 V		2		μA
Pull Down Delay	CFETD	Measured at 10% to 90% of VCC, -40°C < T _A < 100°C		1.3		ms
CFET Pull Down Resistance	CFETR	Measured with 1 mA Pull up Current, after 10ms rising edge delay		1.3		kΩ

Slew Rate/Soft Start

Charge Slew Rate	SLEWP	Slew = 00, FB = 0.1 VOUT Slew = 11, FB = 0.1 VOUT		0.6 4.8		mV/μs
Discharge Slew Rate	SLEWN	Slew = 00, FB = 0.1 VOUT Slew = 11, FB = 0.1 VOUT		-0.6 -4.8		mV/μs
Prebias Level	PBLV	FB=0.1VOUT		300		mV

Dead Battery/VCONN

Dead Battery Input Voltage Range	VDB		4.5	5	5.25	V
Dead Battery Output Voltage	VIO	VDB = 5 V, -40°C < T _A < 100°C Output Current 32 mA	4.4	4.7	4.77	V
Dead Battery Current Limit	DB_LIM	VDB = 5 V, V ₁ greater than 2 V	29	57	78	mA

Enable

EN High Threshold Voltage	ENHT	EM_MASK = ENPU = ENPOL = 0		798	808	mV
EN Low Threshold Voltage	ENLT		652	665		mV
EN Pull Up Current	IEN_UP	EN = 0 V		5		μA
EN Pull Down Current	IEN_DN	EN = VCC		5		μA
I ² C Interface						
Voltage Threshold	I2CVTH		0.95	1	1.05	V
Propagation Delay	I2CPD	(Note 4)		25		ns
Communication Speed	I2CSP		0.400		1	MHz

Thermal Shutdown

Thermal Shutdown Threshold	TSD	(Note 4)		151		°C
Thermal Shutdown Hysteresis	TSDHYS	(Note 4)		28		°C

PDRV

PDRV Operating Range			0		28	V
PDRV Leakage Current	PDRV_IDS	FET OFF, VPDRV = 28 V		180		nA
PDRV Saturation Voltage	PDRV_VDS	ISNK = 10 mA		0.20		V

4. Ensured by design. Not production tested.

APPLICATION INFORMATION

Dual Edge Current Mode Control

When dual edge current mode control is used, two voltage ramps are generated that are 180 degrees out of phase. The inductor current signal is added to the ramps to incorporate current mode control. The first ramp, called the Buck_Ramp or 0_Ramp, since it is the leading ramp and has no phase lag with gained current signal imposed on it, will generate the Buck_PWM_COMP signal. The second ramp, called the Boost_Ramp or 180_Ramp, since it has a phase lag of 180 degrees with gained current signal imposed on it, will generate the Boost_PWM_COMP signal. The designer will note that the triangular wave shape of the ramps lend themselves to crossing twice at the midpoint of the Boost_Ramp ascension and Buck_Ramp dissention and vice versa. The point at which they intersect the midpoint of the ramp is the 100% duty cycle level for buck mode and the

0% duty cycle level for boost mode conversion. Further, when the COMP voltage is below the midpoint, the converter is in buck mode and when it is above the midpoint it is in boost mode. The example of the timing diagrams are shown in Figure 4. When in buck mode, if the Buck_PWM_COMP is high and Boost_PWM_COMP is high S1 is on and S2 is off. Likewise, when in buck mode, if the Buck_PWM_COMP is high and Boost_PWM_COMP is low, S1 is off and S2 is on. During buck mode, S3 is always off and S4 is always on. In boost mode if the Buck_PWM_COMP is low and Boost_PWM_COMP is high, S3 is on and S4 is off. Likewise, when the Buck_PWM_COMP is low and Boost_PWM_COMP is low S3 is off and S4 is on. During boost mode S1 is always on and S2 is always off.

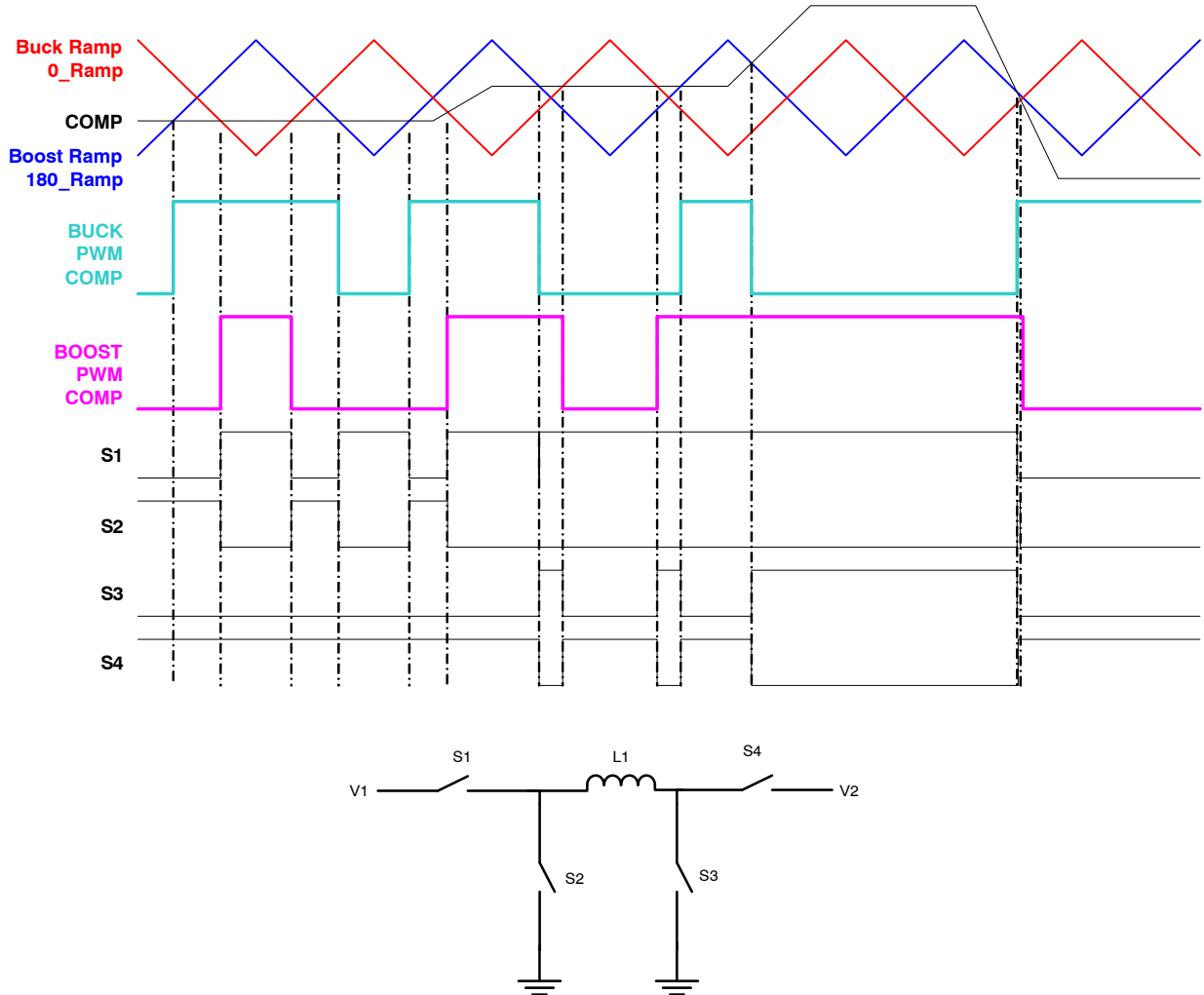


Figure 4. Transitions for Dual Edge 4 Switch Buck Boost

Feedback and Output Voltage Profile

The feedback of the converter output voltage is connected to the FB pin of the device through a resistor divider. Internally FB is connected to the inverting input of the internal transconductance error amplifier. The non-inverting input of the gm amplifier is connected to the internal reference. The internal reference voltage is by default 0.5 V. Therefore a 10:1 resistor divider from the converter output to the FB will set the output voltage to 5V

in default. The reference voltage can be adjusted with 10 mV(default) or 5 mV steps from 0.1 V to 2.55 V through the voltage profile register (01H), which makes the continuous output voltage profile possible through an external resistor divider. For example, by default, if the external resistor divider has a 10:1 ratio, the output voltage profile will be able to vary from 1 V to 25.5 V with 100 mV steps.

Table 4. VOLTAGE PROFILE SETTINGS

VPS_7	VPS_6	VPS_5	VPS_4	VPS_3	VPS_2	VPS_1	VPS_0	Voltage Profile Hex Value	Reference Voltage (mV)
0	0	0	0	0	0	0	0	00H	0
0	0	0	0	0	0	0	1	01H	10
0	0	0	0	0	0	1	0	02H	20
...
0	0	1	1	0	0	1	0	32H	500 (Default)
...
1	1	0	0	0	1	1	1	C7H	1990
1	1	0	0	1	0	0	0	C8H	2000
1	1	1	1	1	1	1	1	FFH	2550

Transconductance Voltage Error Amplifier

To maintain loop stability under a large change in capacitance, the NCP81239 can change the gm of the internal transconductance error amplifier from 87 μS to

1000 μS allowing the DC gain of the system to be increased more than a decade triggered by the adding and removal of the bulk capacitance or in response to another user input. The default transconductance is 500 μS.

Table 5. AVAILABLE TRANSCONDUCTANCE SETTING

AMP_2	AMP_1	AMP_0	Amplifier GM Value (μS)	Max (μS)	Min (μS)
0	0	0	87	95.7	78.3
0	0	1	100	110	90
0	1	0	117	128.7	105.3
0	1	1	333	366.3	299.7
1	0	0	400	440	360
1	0	1	500	550	450
1	1	0	667	733.7	600.3
1	1	1	1000	1100	900

Programmable Slew Rate

The slew rate of the NCP81239 is controlled via the I²C registers with the default slew rate set to 0.6 mV/μs (FB = 0.1 V₂, assume the resistor divider ratio is 10:1) which is the slowest allowable rate change. The slew rate is used when the output voltage starts from 0 V to a user selected profile level, changing from one profile to another, or when the output voltage is dynamically changed. The output voltage is divided by a factor of the external resistor divider and connected to FB pin. The 9 Bit DAC is used to increase the reference voltage in 10 or 5 mV increments.

The slew rate is decreased by using a slower clock that results in a longer time between voltage steps, and conversely increases by using a faster clock. The step monotonicity depends on the bandwidth of the converter where a low bandwidth will result in a slower slew rate than the selected value. The available slew rates are shown in Table 6. The selected slew rate is maintained unless the current limit is tripped; in which case the increased voltage will be governed by the positive current limit until the output voltage falls or the fault is cleared.

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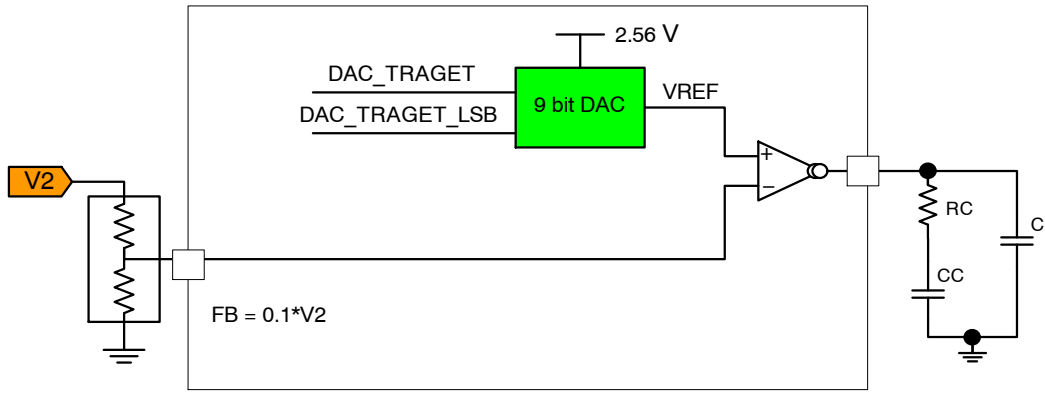


Figure 5. Slew Rate Limiting Block Diagram and Waveforms

Table 6. SLEW RATE SELECTION

Slew Bits	Soft Start or Voltage Transition ($FB = 0.1 * V2$)
Slew_0	0.61 mV/ μ s
Slew_1	1.2 mV/ μ s
Slew_2	2.4 mV/ μ s
Slew_3	4.9 mV/ μ s

The discharge slew rate is accomplished in much the same way as the charging except the reference voltage is decreased rather than increased. The slew rate is maintained unless the negative current limit is reached. If the negative current limit is reached, the output voltage is decreased at the maximum rate allowed by the current limit (see the negative current limit section).

Soft Start

During a 0 V soft start, standard converters can start in synchronous mode and have a monotonic rising of output

Table 7. FREQUENCY PROGRAMMING TABLE

Name	Bit	Definition	Description
Freq1	03H [2:0]	Frequency Setting	3 Bits that Control the Switching Frequency from 150 kHz to 1 MHz. 000: 600 kHz 001: 150 kHz 010: 300 kHz 011: 450 kHz 100: 750 kHz 101: 900 kHz 110: 1.2 MHz 111: Reserved

Current Sense Amplifiers

Internal precision differential amplifiers measure the potential between the terminal CSP1 and CSN1 or CSP2 and CSN2. Current flows from the input V1 to the output in a buck boost design. Current flowing from V1 through the switches to the inductor passes through R_{SENSE} . The external sense resistor, R_{SENSE} , has a significant effect on the function of current sensing and limiting systems and

voltage. If a prebias exists on the output and the converter starts in synchronous mode, the prebias voltage could be discharged. The NCP81239 controller ensures that if a prebias is detected, the soft start is completed in a non-synchronous mode to prevent the output from discharging. During softstart, the output rising slew rate will follow the slew rate register with default value set to 0.6 mV/ μ s ($FB = 0.1 * V2$).

Frequency Programming

The switching frequency of the NCP81239 can be programmed from 150 kHz to 1.2 MHz via the I²C interface. The default switching frequency is set to 600 kHz. Once the part is enabled, the frequency is set and cannot be changed while the part remains enabled. The part must be disabled with no switching prior to writing the frequency bits into the appropriate I²C register.

must be chosen with care. First, the power dissipation in the resistor should be considered. The system load current will cause both heat and voltage loss in R_{SENSE} . The power loss and voltage drop drive the designer to make the sense resistor as small as possible while still providing the input dynamic range required by the measurement. Note that input dynamic range is the difference between the maximum input

signal and the minimum accurately measured signal, and is limited primarily by input DC offset of the internal amplifier. In addition, R_{SENSE} must be small enough that V_{SENSE} does not exceed the maximum input voltage 100 mV, even under peak load conditions.

The potential difference between $CSPx$ and $CSNx$ is level shifted from the high voltage domain to the low voltage VCC domain where the signal is split into two paths.

The first path, or external path, allows the end user to observe the analog or digital output of the high side current

sense. The external path gain is set by the end user allowing the designer to control the observable voltage level. The voltage at $CS1$ or $CS2$ can be converted to 8 bits by the ADC and stored in the internal registers which are accessed through the I^2C interface.

The second path, or internal path, has internally set gain of 10 and allows cycle by cycle precise limiting of positive and negative peak input current limits.

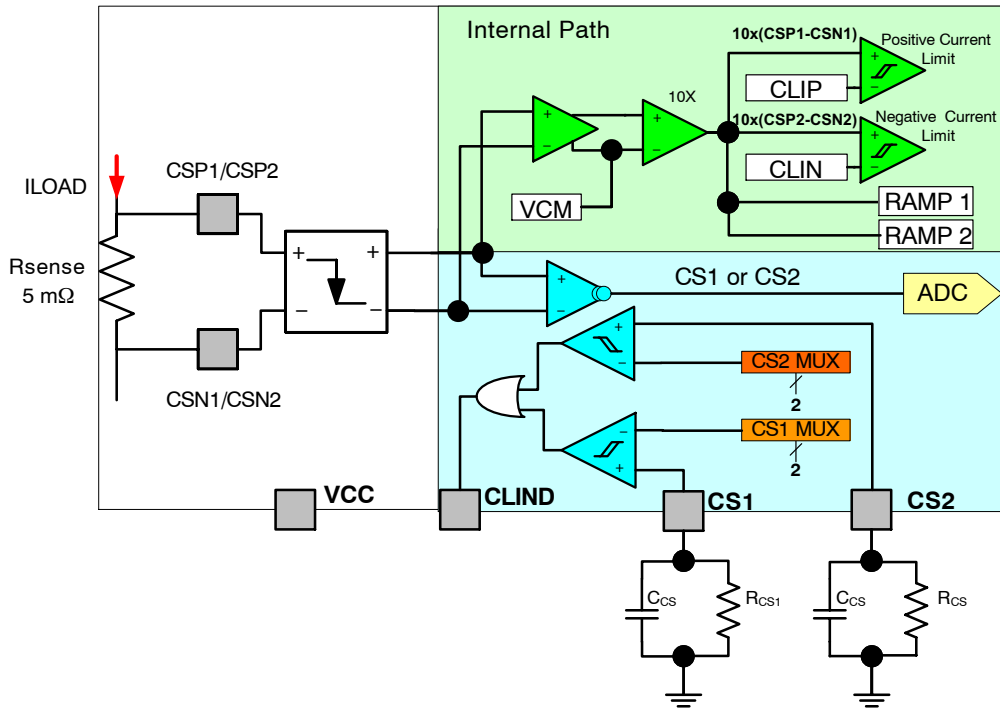


Figure 6. Block Diagram and Typical Connection for Current Sense

Positive Current Limit Internal Path

The NCP81239 has a pulse by pulse current limiting function activated when a positive current limit triggers. $CSP1/CSN1$ will be the positive current limit sense channel.

When a positive current limit is triggered, the current pulse is truncated. In both buck mode and in boost mode the S1 switch is turned off to limit the energy during an over current event. The current limit is reset every switching cycle and waits for the next positive current limit trigger. In this way, current is limited on a pulse by pulse basis. Pulse by pulse current limiting is advantageous for limiting energy into a load in over current situations but are not up to the task of limiting energy into a low impedance short. To address the

low impedance short, the NCP81239 does pulse by pulse current limiting for 2 ms known as I_{lim} timeout or until the output voltage falls below 300 mV, the controller will enter into fast stop. The NCP81239 remains in fast stop state with all switches driven off for 10 ms. Once the 10 ms has expired, the part is allowed to soft start to the previously programmed voltage and current level if the short circuit condition is cleared.

The internal current limits can be controlled via the I^2C interface both in trip level and in function. The internal positive and negative current limit can be masked such that they do not activate when they are exceeded; they will not trigger system protection as shown in Table 8.

Table 8. INTERNAL PEAK CURRENT LIMIT

CLIN_1	CLIN_0	CLIM delta Value (mV)	CSP2-CSN2 (mV)	Current at RSENSE = 5 mΩ (A)
0	0	-400	-40 (Default)	-8
0	1	-250	-25	-5
1	0	-150	-15	-3

Table 8. INTERNAL PEAK CURRENT LIMIT

1	1	0	0	0
CLIP_1	CLIP_0	CLIM delta Value (mV)	CSP1–CSN1 (mV)	Current at RSENSE = 5 mΩ (A)
0	0	380	38 (Default)	7.6
0	1	230	23	4.6
1	0	110	11	2.2
1	1	700	70	14

Table 9. INTERNAL PEAK CURRENT LIMIT

INT_C L1	INT_C L0	Internal Current Limit	
		Positive	Negative
0	0	ON	ON
0	1	ON	OFF
1	0	OFF	ON
1	1	OFF	OFF

Negative Current Limit Internal Path

Negative current limit can be activated in a few instances, including light load synchronous operation, heavy load to light load transition, output overvoltage, and high output voltage to lower output voltage transitions. CSP2/CSN2 will be the negative current limit sense channel.

During light load synchronous operation, or heavy load to light load transitions the negative current limit can be triggered during normal operation. When the sensed current exceeds the negative current limit, the S4 switch is shut off preventing the discharge of the output voltage both in buck mode and in boost mode if the output is in the power good range. Both in boost mode and in buck mode when a negative current is sensed, the S4 switch is turned off for the remainder of either the S4 or S2 switching cycle and is turned on again at the appropriate time. In buck mode, S4 is turned off at the negative current limit transition and turned on again as soon as the S2 on switch cycle ends. In boost mode, the S4 switch is the rectifying switch and upon negative current limit the switch will shut off for the remainder of its switching cycle.

External Path (CS1, CS2, CLIND)

The voltage drop across the sense resistors as a result of the load can be observed on the CS1 and CS2 pins. The

voltage drop is converted into a current by a transconductance amplifier with a typical GM of 5 mS. The final gain of the output is determined by the end users selection of the R_{CS} resistors. The output voltage of the CS pin can be calculated from Equation 1. The user must be careful to keep the dynamic range below 3.0 V when considering the maximum short circuit current.

$$V_{CS} = (I_{LOAD_MAX} * R_{SENSE} * Trans) * R_{CS} \rightarrow$$

$$\rightarrow 2.967 V = (8.5 A * 5 m\Omega * 5 mS) * 13.96 k\Omega$$

$$R_{CS} = \frac{V_{CS}}{I_{LOAD} * R_{SENSE} * Trans} \rightarrow$$

$$\rightarrow 13.96 k\Omega = \frac{2.967 V}{8.5 A * 5 m\Omega * 5 mS} \quad (eq. 1)$$

The speed and accuracy of the dual amplifier stage allows the reconstruction of the input and output current signal, creating the ability to limit the peak current. If the user would like to limit the mean DC current of the switch, a capacitor can be placed in parallel with the R_{CS} resistors.

The external CS voltages are connected to 2 high speed low offset comparators. The comparators output can be used to suspend operation until reset or restart of the part depending on I²C configuration. When one of the comparators trips if not masked, the external CLIND flag is triggered to indicate that the internal comparator has exceeded the preset limit. The default comparator setting is 250 mV which is a limit of 500 mA with a current sense resistor of 5 mΩ and an R_{CS} resistor of 20 kΩ. The block diagram in shows the programmable comparators and the settings are shown in Table 10.

Table 10. REGISTER SETTING FOR THE CLIM COMPARATORS

CLIMx_1	CLIMx_0	CSx_LIM (V)	Current at RSENSE = 5 mΩ RSET = 20 kΩ (A)	Current at RSENSE = 5 mΩ RSET = 10 kΩ (A)
0	0	0.25	.5	1
0	1	0.75	1.5	3
1	0	1.5	3	6
1	1	2.5	5	10

Overvoltage Protection (OVP)

When the divided output voltage is 115% (typical) above the internal reference voltage for greater than one switching cycle, an OV fault is set. During an overvoltage fault, S1 is driven off, S2 is driven on, and S3 and S4 are modulated to discharge the output voltage while preventing the inductor current from going beyond the I²C programmed negative current limit.

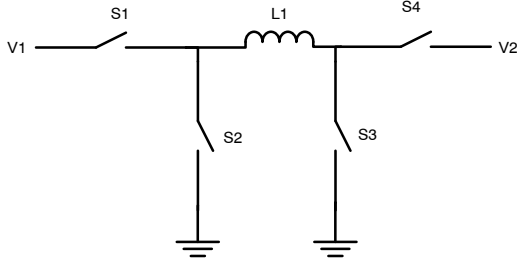


Figure 7. Diagram for OV Protection

During overvoltage fault detection the switching frequency changes from its I²C set value to 50 kHz to reduce the power dissipation in the switches and prevent the inductor from saturating. OOV is disabled during voltage changes to ensure voltage changes and glitches during slewing are not falsely reported as faults. The OOV faults are reengaged 1 ms after completion of the soft start.

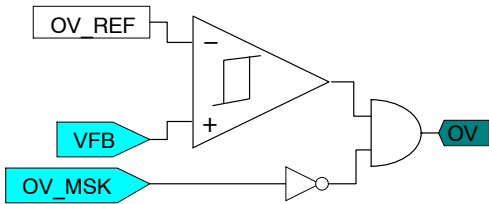


Figure 8. OV Block Diagram

Table 11. OVERVOLTAGE MASKING

OV_MAK	Description
0	OV Action and Indication Unmasked
1	OV Action and Indication Masked

Power Good Monitor (PG)

NCP81239 provides two window comparators to monitor the internal feedback voltage. The target voltage window is $\pm 5\%$ of the reference voltage (typical). Once the feedback voltage is within the power good window, a power good indication is asserted once a 3.3 ms timer has expired. If the feedback voltage falls outside a $\pm 7\%$ window for greater than 1 switching cycle, the power good register is reset. Power good is indicated on the INT pin if the I²C register is set to display the PG state. During startup, INT is set until the feedback voltage is within the specified range for 3.3 ms.

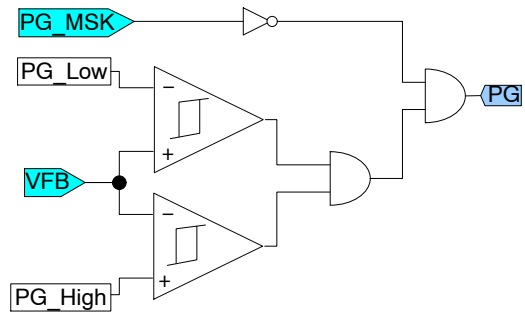


Figure 9. PG Block Diagram

Table 12. POWER GOOD MASKING

PG_MSK	Description
0	PG Action and Indication Unmasked
1	PG Action and Indication Masked

Thermal Shutdown

The NCP81239 protects itself from overheating with an internal thermal shutdown circuit. If the junction temperature exceeds the thermal shutdown threshold (typically 150°C), all MOSFETs will be driven to the off state, and the part will wait until the temperature decreases to an acceptable level. The fault will be reported to the fault register and the INT flag will be set unless it is masked. When the junction temperature drops below 125°C (typical), the part will discharge the output voltage to Vsafe 0 V. If a thermal fault is triggered during the discharge, the part will again be halted until the thermal fault is cleared. The discharging of the output will continue until it is less than 300 mV; at which time it is deemed to be Vsafe 0 V and can be reconfigured to USB 2.0, a benign state of operation.

Table 13. THERMAL TRIP NOT AVAILABLE FOR CUSTOMERS

ThermTrip	Definition
0	Thermal Trip Performs as Designed
1	Thermal Trip is Masked and will not shut the part off

CFET Turn On

The CFET is used to engage the output bulk capacitance after successful negotiations between a consumer and a provider. The USB Power Delivery Specification requires that no more than 30 μ F of capacitance be present on the VBUS rail when sinking power. Once the consumer and provider have completed a power role swap, a larger capacitance can be added to the output rail to accommodate a higher power level. The bulk capacitance must be added in such a way as to minimize current draw and reduce the

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voltage perturbation of the bus voltage. The NCP81239 incorporates a right drive circuit that regulates current into the gate of the MOSFET such that the MOSFET turns on slowly reducing the drain to source resistance gradually. Once the transition from high to low has occurred in a controlled way, a strong pulldown driver is used to ensure

normal operation does not turn on the power N–MOSFET engaging the bulk capacitance. The CFET must be activated through the I²C interface where it can be engaged and disengaged. The default state is to have the CFET disengaged.

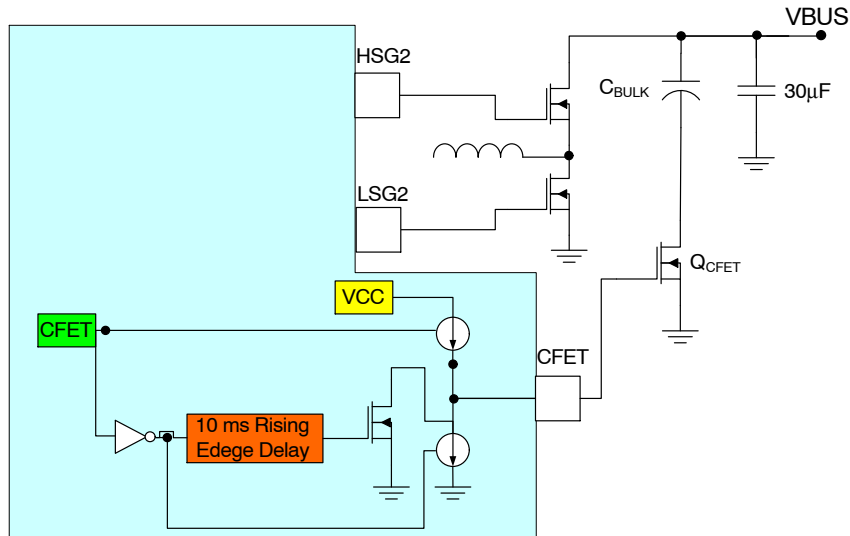


Figure 10. CFET Drive

Table 14. CFET ACTIVATION TABLE

CFET_0	Description
0	CFET Drive Pulldown
1	CFET Drive Pull Up

PFET Drive

The PMOS drive is an open drain output used to control the turn on and turn off of PMOSFET switches at a floating potential. The external PMOS can be used as a cutoff switch, enable for an auxiliary power supply, or a bypass switch for a power supply. The R_{DSon} of the pulldown NMOSFET is typically 20 Ω allowing the user to quickly turn on large PMOSFET power channels.

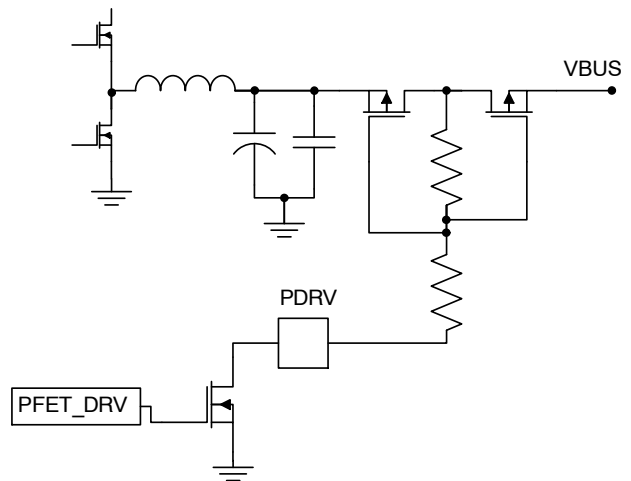


Figure 11. PFET Drive

Table 15. PFET ACTIVATION TABLE

PFET_DRV	Description
0	NFET OFF (Default)
1	NFET ON

Analog to Digital Converter

The analog to digital converter is a 7-bit A/D which can be used as an event recorder, an input voltage sampler, output voltage sampler, input current sampler, or output current sampler. The converter digitizes real time data during the sample period. The internal precision reference is used to provide the full range voltage; in the case of CSP1(input voltage), or FB (with 10:1 external resistor divider) the full range is 0 V to 25.6 V. The CSP1 is internally divided down by 10 before it is digitized by the ADC, thus

the range of the measurement is 0 V–2.56 V, same as FB. The resolution of the CSP1 and FB voltage is 20 mV at the analog mux, but since the voltage is divided by 10 output voltage resolution will be 200 mV. When CS1 and CS2 are sampled, the range is 0 V–2.56 V. The resolution will be 20 mV in the CS monitoring case. The actual current can be calculated by dividing the CS1 or CS2 values with the factor of $R_{sense} * 5mS * RCSx$, the total gain from the current input to the external current monitoring outputs.

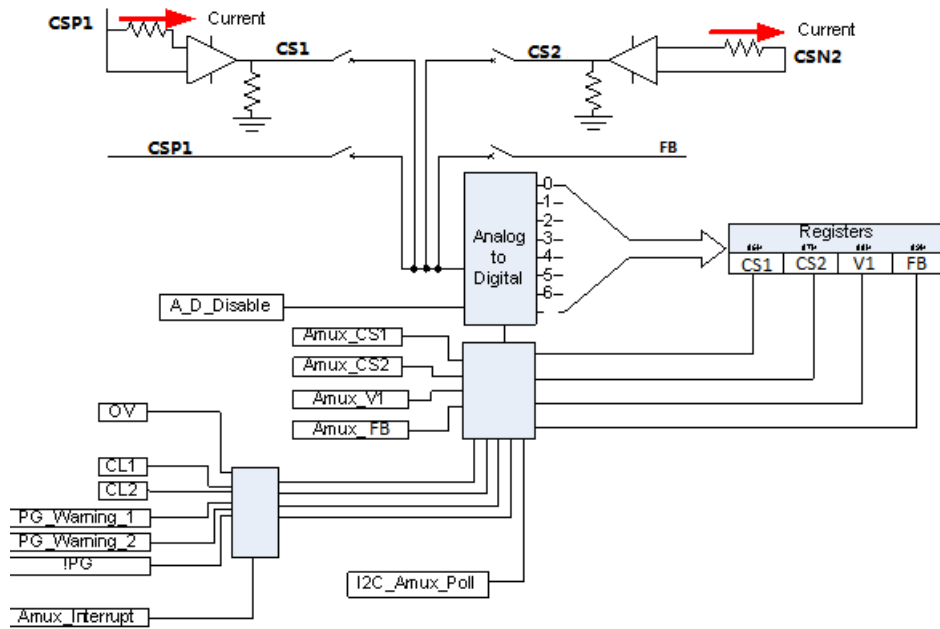


Figure 12. Analog to Digital Converter

Table 16. ADC BYTE

	MSB	5	4	3	2	1	LSB
DATA	D6	D5	D4	D3	D2	D1	D0

Table 17. REGISTER SETTING FOR ENABLING DESIRED ADC BEHAVIOUR

ADC_2	ADC_1	ADC_0	Description
0	0	0	Poll Amux Inputs on Interrupt Fault State Control, A/D Enabled, Data Convert all Settings in Interrupt
0	0	1	Sets Amux to CS1, Reads Once
0	1	0	Sets Amux to CS2, Reads Once
0	1	1	Sets Amux to V1, Reads Once
1	0	0	Sets Amux to FB (FB Voltage), Reads Once
1	0	1	Disable A/D Conversion Low Power
1	1	0	Poll Amux Inputs One at a Time Continuously
1	1	1	Spare

Table 18. REGISTER SETTING FOR ADC FLAG CLEAR BEHAVIOUR

ADC_Flag	Description
0	Flag cleared, indicating that the required polling has not yet completed.
1	Flag set, indicating that the required polling has been completed; this is not set when continuous polling is used. Once a read is completed, the flag is reset.

Interrupt Control

The interrupt controller continuously monitors internal interrupt sources, generating an interrupt signal when a system status change is detected. Individual bits generating interrupts will be set to 1 in the INTACK register (I²C read only registers), indicating the interrupt source. INTACK register is automatically reset by an I²C read. All interrupt sources can be masked by writing 1 in register INTMSK.

Masked sources will never generate an interrupt request on the INT pin. The INT pin is an open drain output. A non-masked interrupt request will result in the INT pin being driven high. When the host reads the INTACK registers, the INT pin will be driven low and the interrupt register INTACK is cleared. Figure 13 illustrates the interrupt process.

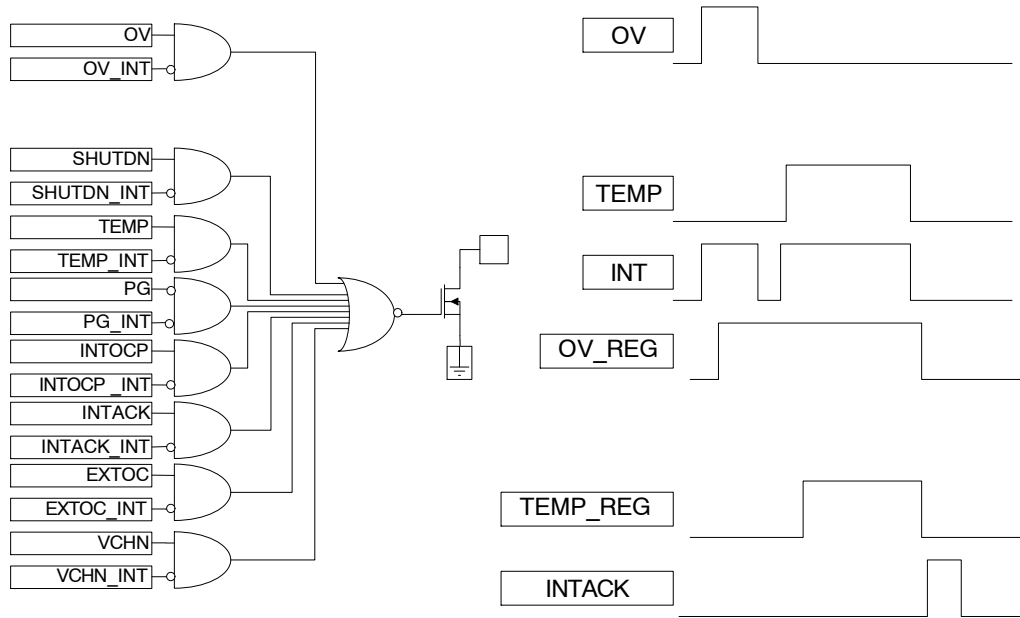


Figure 13. Interrupt Logic

Table 19. INTERPRETATION TABLE

Interrupt Name	Description
OV	Output Over Voltage
Shutdown	Shutdown Detection (EN=low)
TEMP	IC Thermal Trip
PG	Power Good Trip Thresholds Exceeded
INTOCP	Internal Current Limit Trip
EXTOC	External Current Trip from CLIND
VCHN	Output Negative Voltage Change
INTACK	I ² C ACK signal to the host

I²C Address

NCP81239 has four address selectable factory settings (ADD0 to ADD3). Different address settings can be generated upon request to ON Semiconductor. The default address is set to E8h /E9h.

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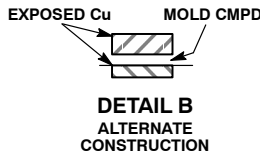
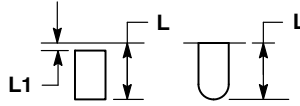
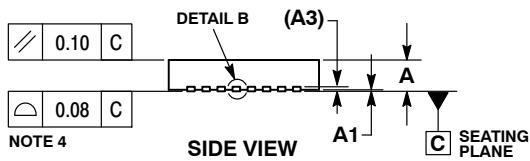
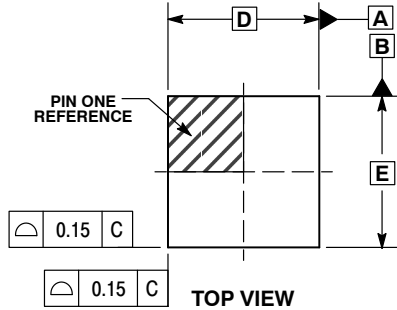
Table 20. I²C ADDRESS

I ² C Address	Hex	A7	A6	A5	A4	A3	A2	A1	A0
ADD0 (default)	W 0xE8 R 0xE9	1	1	1	0	1	0	0	R/W
ADD1	W 0xEA R 0xEB	1	1	1	0	1	0	1	R/W
ADD2	W 0xEC R 0xED	1	1	1	0	1	1	0	R/W
ADD3	W 0xEE R 0xEF	1	1	1	0	1	1	1	R/W

NCP81239

PACKAGE OUTLINE

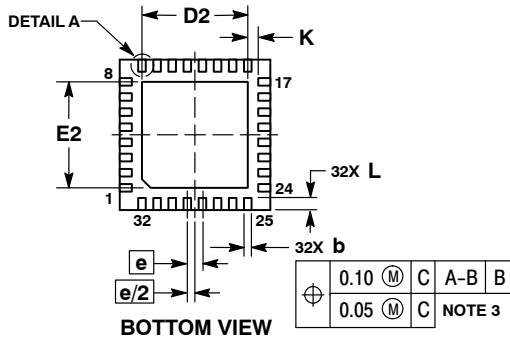
QFN32 5x5, 0.5P
CASE 485CE
ISSUE O



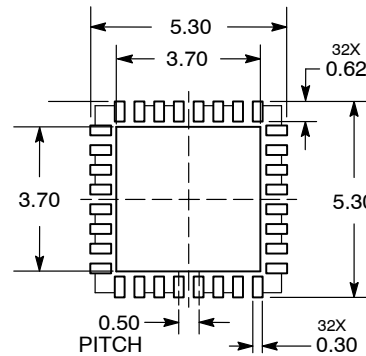
NOTES:

1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.
2. CONTROLLING DIMENSION: MILLIMETERS.
3. DIMENSION b APPLIES TO PLATED TERMINAL AND IS MEASURED BETWEEN 0.15 AND 0.30 MM FROM THE TERMINAL TIP.
4. COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS THE TERMINALS.

MILLIMETERS		
DIM	MIN	MAX
A	0.80	1.00
A1	---	0.05
A3	0.20	REF
b	0.20	0.30
D	5.00	BSC
D2	3.40	3.60
E	5.00	BSC
E2	3.40	3.60
e	0.50	BSC
K	0.20	---
L	0.30	0.50
L1	---	0.15



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